



## Ballscrews / Linear Guideway / Mono Stage General Catalog

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## COMPANY INTRODUCTION

**PMI GROUP** was established in 1990. It's highly involved in manufacturing of ballscrews, linear guideway and mono stage, which is the critical component of precision machinery and mainly applied to Machine Tool, Electric Discharging Machine, Cutting Wire Machine, Plastics Injection Machine, Semi-conductor Equipment, Precision Orientation Equipment and other equipments and machines.

Recent years, **PMI** Group places great emphasis in upgrading not only the manufacturing and quality of products but also the manpower. In addition to comply with requirement of quality management system, **PMI** Group has been actively carried out 『RoHS Green Environmental System』 and environmentally friendly management system to conform to the regulation in order to reach a pollution-free workplace.



## Environment Policy

**PMI** devotes in research & developing and manufacturing of Precision Linear Motion Components. To provide world class levels of service, quality and learning through our innovative business philosophy, that is integral to all **PMI's** transmission components and services. To protect the environment and personal safety by more actively promoting and implementing the ROHS green system, ESH and energy management systems. To meet or exceed regulatory levels for emission and waste control, within a labor-friendly work environment that utilizes the latest energy reduction technology to make **PMI** a leader in environmental protection. Through the guidance of safety and environmental management systems, energy awareness advocacy and setting up the related regulations, we promise to prevent any pollution, conserve resources, safety as priority, enhance health and energy-saving, with every staff's involvement. In accordance with the spirits of innovations and developments, **PMI** can provide the best mechanical efficiency and quality service to our customers, ensure the personal safety, reduce any harmful factors to every staff in the working place, increase the knowledge of safety and environment, prevent any pollutions, injuries, diseases happened, and effective energy control. Moreover, to be a sustainable development GREEN INDUSTRY, **PMI** will continue to improve the safety, environment activities and energy usage management in order to take the corporation social responsibility to the utmost and reduce any harmful factors and energy consumption during the manufacturing.

We promise and are devoted to implement the following environmental and energy policies:

1. By reducing pollution and continually improving our energy usage performance, **PMI** can simultaneously minimize accidents and sickness whilst achieving regulatory compliance.
2. **PMI** develops GREEN products, strengthen risk and energy management.
3. Purchase energy-saving products, improve the design of the energy performance.
4. Every department participates preserving our environment, energy awareness, and the prevention of injuries, diseases and the reduction of energy consumption.

Based on the above descriptions, **PMI** will continue holding every kind of safety, environment and energy activities, increase our international environmental protection image and industry competition, and let the related organizations understand our ambitions and responsibilities to the environment and energy management that people live in.

## Quality Policy

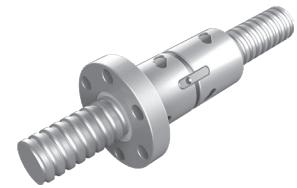
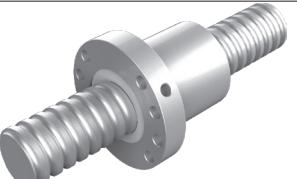
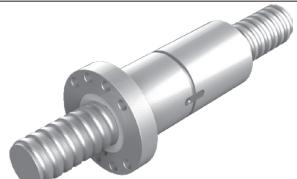
The followings are what the employees expect for the quality policy:

Prompt delivery, sustained improvement, satisfying customer's needs and expectations.

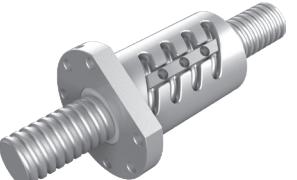


# PRODUCT INFORMATION

## Precision Ground Series

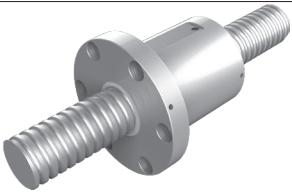
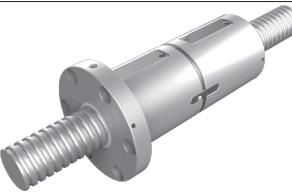
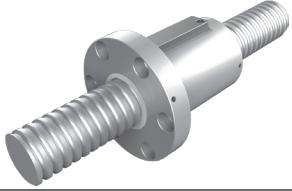
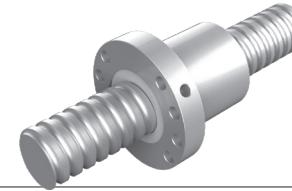
Internal Ball Circulation Series	
FSIC	A-131
	
FDIC	A-135
	
FOIC	
FOIC	A-139
	
RSIC	A-141
	
RDIC	
RDIC	A-143
	
End Deflector Series	
FSDC	A-146
	
FDDC	A-150
	

## Precision Ground Series

External Ball Circulation Series	
FSWC	A-155
	
FDWC	A-160
	
FSVC	
FSVC	A-165
	
FDVC	A-169
	
FOWC	
FOWC	A-173
	

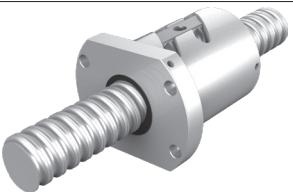
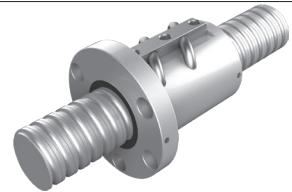
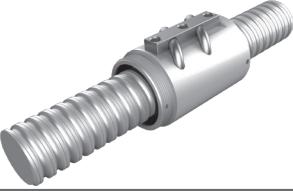
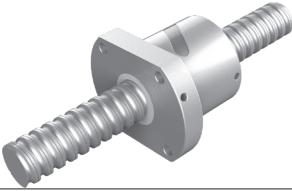
## Precision Ground Series

### High Lead Series

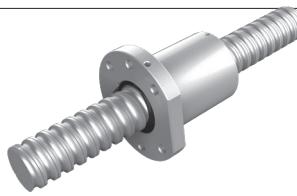
<b>FSWE</b>	A-176	<b>FDWE</b>	A-180
			
<b>FSVE</b>	A-184	<b>FDVE</b>	A-188
			
<b>End Cap Series</b>			
<b>FSKC</b>	A-192		
			
<b>Heavy Load Series</b>			
<b>FSVH</b>	A-197	<b>FSDH</b>	A-199
			

## Rolled Series

### External Ball Circulation Series

<b>FSWW</b>	A-252	<b>FSVW</b>	A-255
			
<b>RSVW</b>	A-258	<b>FSBW</b>	A-259
			
<b>SSVW</b>	A-260		
			
<b>End Cap Series</b>			
<b>FSKW</b>	A-261		
			

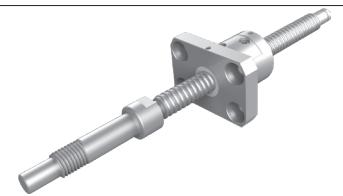
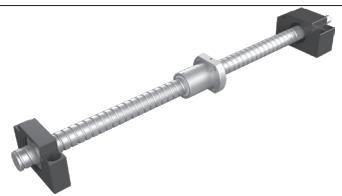
## Rolled Series

internal Ball Circulation Series			
<b>FSIW</b>	A-262	<b>FSDW</b>	A-264
			

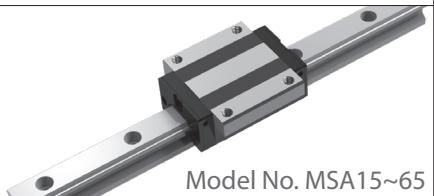
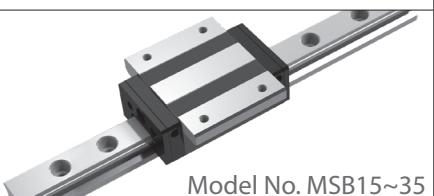
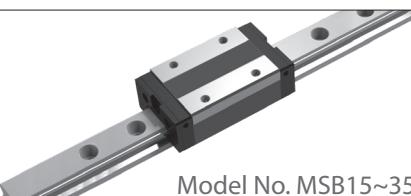
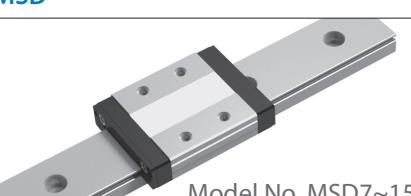
Blank Shaft End Series			
<b>FSIN</b>	A-266	<b>FSDN</b>	A-267

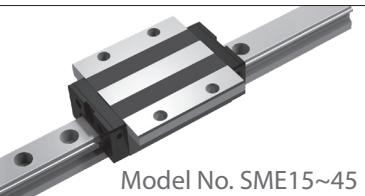
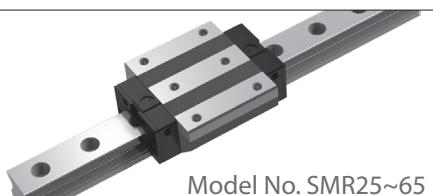
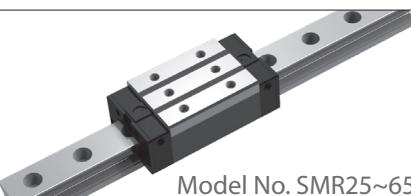
## Standard type series

Miniaature Series	FA Series
<b>FSMC</b>	A-200
	

PPR	PTR
	

Heavy Load Type		B-39
MSA-A / MSA-LA	MSA-E / MSA-LE	MSA-S / MSA-LS
		
Model No. MSA15~65	Model No. MSA15~65	
Compact Type		B-62
MSB-E	MSB-S	
		
Model No. MSB15~35	Model No. MSB15~35	
Full Roller Type		B-82
MSR-E	MSR-S	
		
Model No. MSR25E~65E	Model No. MSR25S~65S	
Miniature Type		B-102
MSC	MSD	
		
Model No. MSC7~15	Model No. MSD7~15	

Ball Chain Type		B-120
SME-E	SME-S	
		
Model No. SME15~45	Model No. SME15~45	
Roller Chain Type		B-146
SMR-E	SMR-S	
		
Model No. SMR25~65	Model No. SMR25~65	
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KM		
		
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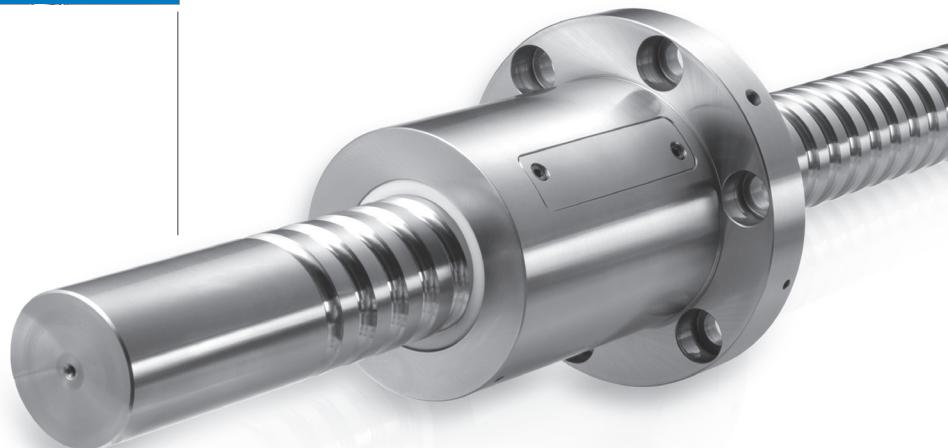
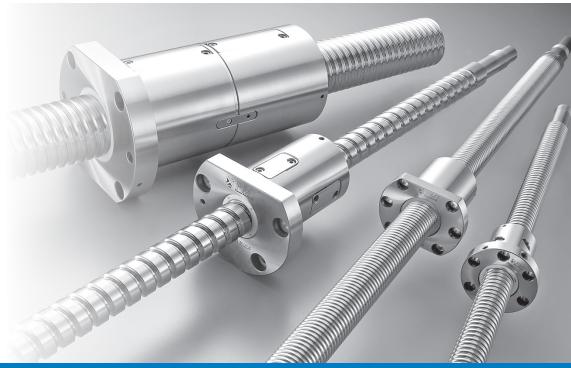
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## Ballscrews



**(1) High reliability**

**PMI** has accumulated many years experience in production managing. It covers the whole production sequence, from receiving the order, designing, material preparation, machining, heat treating, grinding, assembling, inspection, packaging and delivery. The systemized managing ensures high reliability of **PMI** Ballscrews.

**(2) High accuracy**

**PMI** Ballscrews are machined, ground, assembled and Q.C. inspected under the constant temperature control (20°C) to ensure high precision of Ballscrews. Fig.1.1 accuracy inspection certificate.

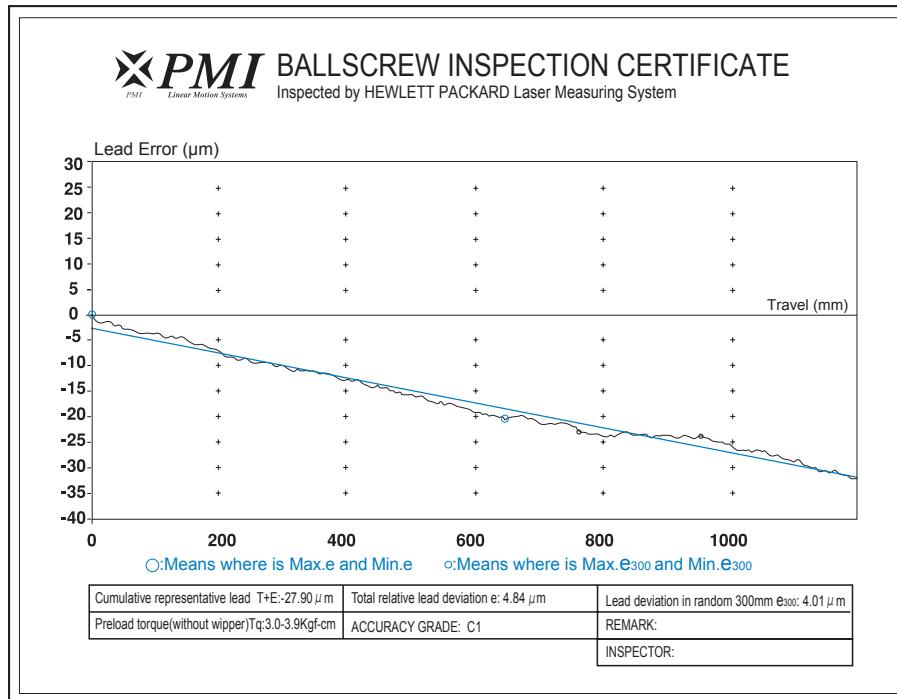


Fig.1.1 Accuracy inspection certificate.

**(3) Long durability**

**PMI** Ballscrews are Alloy steels, which are well quenching and tempering treated for good rigidity, along with suitable surface hardening to ensure long durability.

**(4) High working efficiency**

Balls are rotating inside the Ballscrew nut to offer high working efficiency. Comparing with the traditional ACME screws, which work by friction sliding between the nut and screw, the Ballscrews needs only 1/3 of driving torque. It is easy to transmit linear motion into rotation motion.

**(5) No backlash and with high rigidity**

The Gothic profile is applied by **PMI** Ballscrews. It offers best contact between balls and the grooves. If suitable preload is exerted on Ballscrew hence to eliminate clearance between the ball nut and screw and to reduce elastic deformation, the ballscrew shall get much better rigidity and accuracy.

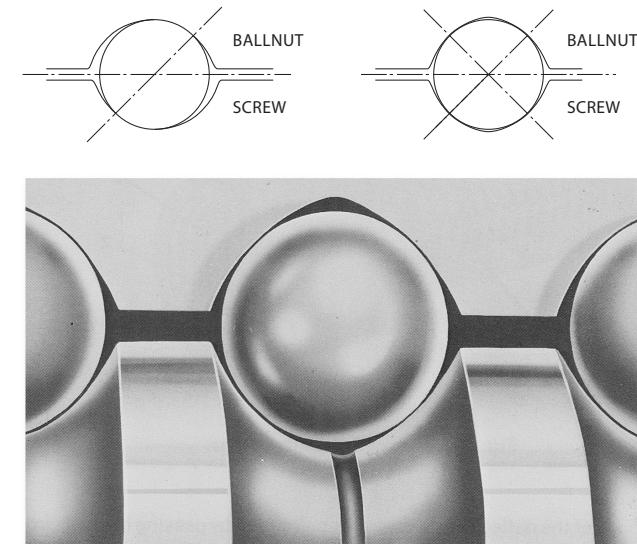


Fig.1.2 Gothic arch thread

## 2.1 Lead Accuracy

PMI's precision ground Ballscrews are controlled in accordance with JIS B 1192.

The permissible values and each part of definitions are shown below.

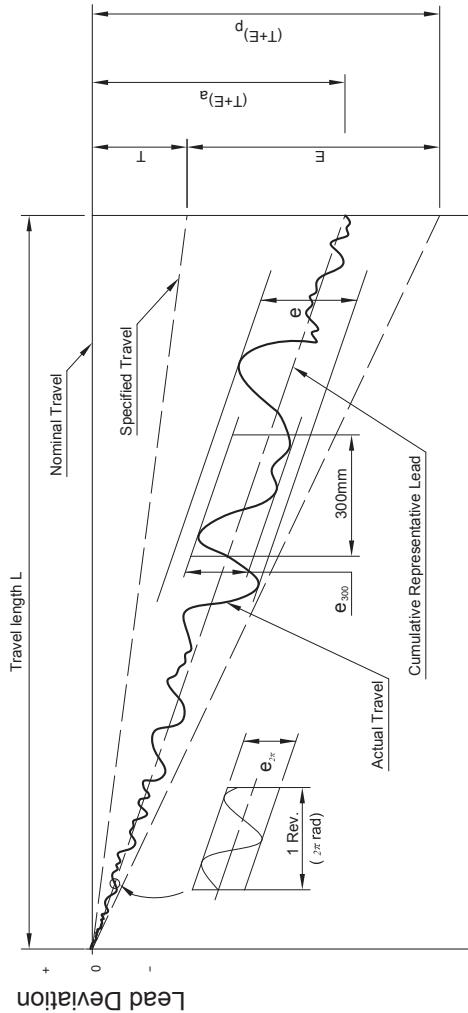


Fig.2.1 Technical Terms Concerning the Lead

Table 2.1 Terms

<b>T+E</b>	Cumulative representative lead. A straight line representing the tendency of the cumulative actual lead. This is obtained by least square method and measured by laser system.
<b>P</b>	Permissible value.
<b>a</b>	Actual value.
<b>T</b>	Specified travel. This value is determined by customer and maker as it depends on different application requirements.
<b>E</b>	Accumulated reference lead deviation. This is allowable deviation of specified travel. It is decided by both of the accuracy grade and effective thread length.
<b>e</b>	Total relative lead variation Maximum width of variation over the travel length.
<b>e<sub>300</sub></b>	Lead deviation in random 300 mm.
<b>e<sub>2π</sub></b>	Lead deviation in random 1 revolution $2\pi$ rad.

Table 2.2 Accumulated reference lead deviation ( $\pm E$ ) and total relative variation (e)

		Unit: $\mu m$													
		GRADE		C0		C1		C2		C3		C4		C5	
OVER	UP TO	E	e	E	e	E	e	E	e	E	e	E	e	E	e
-	315	4	3.5	6	5	8	7	12	8	12	12	23	18		
315	400	5	3.5	7	5	9	7	13	10	14	12	25	20		
400	500	6	4	8	5	10	7	15	10	16	12	27	20		
500	630	6	4	9	6	11	8	16	12	18	14	30	23		
630	800	7	5	10	7	13	9	18	13	20	14	35	25		
800	1000	8	6	11	8	15	10	21	15	22	16	40	27		
1000	1250	9	6	13	9	18	11	24	16	25	18	46	30		
1250	1600	11	7	15	10	21	13	29	18	29	20	54	35		
1600	2000	-	-	18	11	25	15	35	21	35	22	65	40		
2000	2500	-	-	22	13	30	18	41	24	41	25	77	46		
2500	3150	-	-	26	15	36	21	50	29	50	29	93	54		
3150	4000	-	-	32	18	44	25	60	35	62	35	115	65		
4000	5000	-	-	-	-	52	30	72	41	76	41	140	77		
5000	6300	-	-	-	-	65	36	90	50	95	50	170	93		
6300	8000	-	-	-	-	-	-	110	62	120	62	210	115		
8000	10000	-	-	-	-	-	-	137	75	157	75	260	140		

Table 2.3 Accuracy grade

Variation in random 300mm ( $e_{300}$ ) and wobble ( $e_{2\pi}$ )

$e_{300}$	Unit: $\mu m$									
GRADE	C0	C1	C2	C3	C4	C5	C6	C7	C10	
JIS	3.5	5	-	8	-	18	-	50	210	
ISO	3.5	6	-	12	-	23	-	52	210	
DIN	-	6	-	12	-	23	-	52	210	
PMI	3.5	5	7	8	12	18	25	50	210	

$e_{2\pi}$	Unit: $\mu m$					
GRADE	C0	C1	C2	C3	C4	C5
JIS	3	4	-	6	-	8
ISO	3	4	-	6	-	8
DIN	-	4	-	6	-	8
PMI	3	4	4	6	8	8

Table 2.4 Accuracy grades of ball screw and their application

Application	Name of axis	Accuracy grade								
		C0	C1	C2	C3	C4	C5	C6	C7	C10
Lathe	X	●	●	●	●	●	●			
	Z				●	●	●			
Machining center	X,Y		●	●	●	●	●			
	Z			●	●	●	●			
Drilling machine	X,Y				●	●	●			
	Z							●	●	●
Milling machine Boring machine	X,Y		●	●	●	●	●			
	Z			●	●	●	●			
Jig boring machine	X,Y	●	●							
	Z	●	●							
Grinder	X,Y	●	●	●						
	Z		●	●	●	●				
Electric discharge machine	X,Y		●	●	●					
	Z			●	●	●	●	●		
Wire cutting Electric discharge machine	X,Y		●	●	●					
	Z		●	●	●	●				
Punch press	X,Y				●	●	●			
Laser cutting machine	X,Y				●	●	●			
	Z				●	●	●			
Woodworking machine							●	●	●	●
General industrial machines Machines for specific use				●	●	●	●	●	●	●

Application	Name of axis	Accuracy grade								
		C0	C1	C2	C3	C4	C5	C6	C7	C10
Industrial robots	Assembly				●	●	●	●	●	
	Cartesian type other purposes									●
Articulate type	Assembly					●	●	●	●	
	other purposes						●	●	●	
SCARA type					●	●	●	●	●	
	Lithographic machine	●	●							
Semiconductor/ associated industrial	Chemical processing equipment				●	●	●	●	●	●
	Wire bonder			●	●					
Three-dimensional coordinate measuring machine	Prober	●	●	●						
	Printed circuit board drilling machine		●	●	●	●	●			
Nuclear power	Electric component mounted device			●	●	●	●	●		
	Fuel rod control				●	●	●	●	●	
Aircraft	Mechanical snubber								●	●
					●	●	●			

## 2.2 Preloading Torque

The preloading torque of the Ballscrew is controlled in accordance with JIS B 1192.

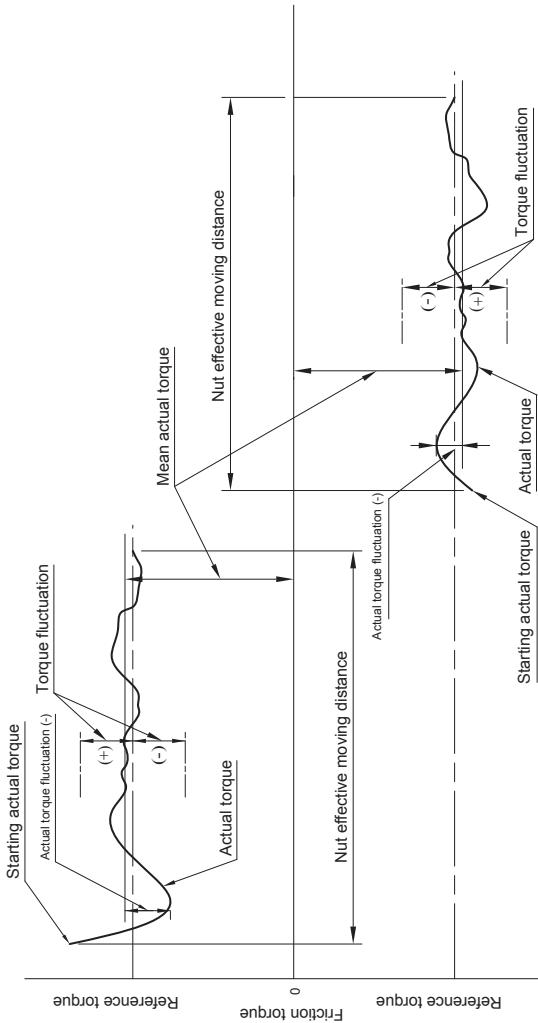


Fig.2.2 Technical terms concerning preload

<b>Preload</b>	The goal in preload is to clear axial play and increase rigidity of Ballscrew. Reference to 5.1.3
<b>Preload torque</b>	Torque needed to continuously turn a Ballscrew with preload with no other load applied to it.
<b>Reference torque</b>	Preload torque set as a goal.
<b>Torque fluctuation</b>	Fluctuation from a goal value of the preload torque. Defined as positive or negative in respect to the reference torque.
<b>Rating of torque fluctuation</b>	Rating on reference torque and torque fluctuation.
<b>Actual torque</b>	Preloaded dynamic torque measured by using an actual value of Ballscrew.
<b>Mean actual torque</b>	In the effective thread length, the net reciprocal to measure the maximum actual torque and minimum actual torque are doing count mean.
<b>Actual torque fluctuation</b>	In the effective thread length, the net reciprocal to measure the maximum fluctuant value.
<b>Rating of Actual torque fluctuation</b>	Rating on mean actual torque and actual torque fluctuation.

Table 2.5 Allowable range of preload torque

Reference torque (kgf.cm)		Effective Thread Length (mm)										
		up to and incl. 4000					over 4000 up to and incl. 10000.					
		Slenderness ratio: up to and incl. 40			Slenderness ratio: over 40 up to and incl. 60			Accuracy grade				
OVER	OR LESS	C0	C1	C3	C5	C0	C1	C3	C5	C1	C3	C5
2	4	±30%	±35%	±40%	±50%	±40%	±40%	±50%	±60%	-	-	-
4	6	±25%	±30%	±35%	±40%	±35%	±35%	±40%	±45%	-	-	-
6	10	±20%	±25%	±30%	±35%	±30%	±30%	±35%	±40%	-	±40%	±45%
10	25	±15%	±20%	±25%	±30%	±25%	±25%	±30%	±35%	-	±35%	±40%
25	63	±10%	±15%	±20%	±25%	±20%	±20%	±25%	±30%	-	±30%	±35%
63	100	-	±15%	±15%	±20%	-	-	±20%	±25%	-	±25%	±30%

### Reference torque

$$T_p = 0.05 (\tan \beta)^{-0.5} \times \frac{Fao \times l}{2\pi} \quad \dots \dots \dots \quad (2.1)$$

Here

$$\begin{array}{ll} T_p & \text{Reference torque (kgf.cm)} \\ Fao & \text{Preload (kgf)} \\ l & \text{Lead(cm)} \\ \beta & \text{Lead angle} \end{array}$$

### 2.3 Tolerances on Various Areas of PMI Ballscrew

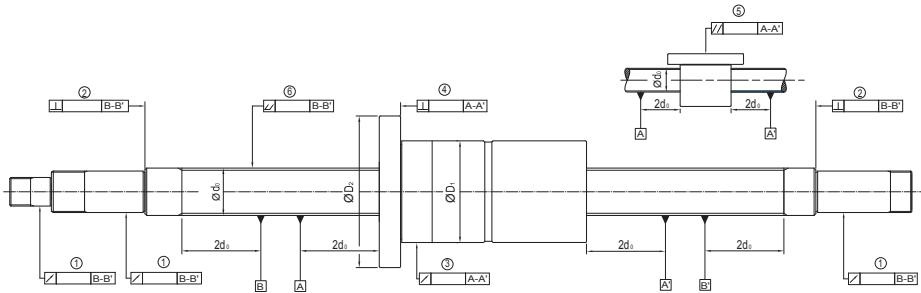


Fig.2.3

Those on above are samples of accuracy of tolerance on various areas of PMI Ballscrew.

⊥ : Perpendicularity      ↗ : Radial runout      // : Parallel      A : Reference

Accuracy on various areas of PMI Ballscrew has to measure items:

1. Radial run-out of the circumference of the screw shaft supported portion in respect to the B-B' line.
2. Perpendicularity of the screw shaft supported portion end face to the B-B' line.
3. Radial run-out of the nut circumference in respect to the A-A' line.
4. Perpendicularity of the flange mounting surface to the A-A' line.
5. Parallelism between the nut circumference to the A-A' line.
6. Overall radial run-out to the A-A' line.

Note: 1.The mounting surface of the Ballscrew is finished to the accuracy specified in JIS B 1192:1997

2.Standard tolerance of accuracy measuring from Jan. 1st 2012 on.

## 2.4 Standard tolerance of accuracy measuring of ballscrew

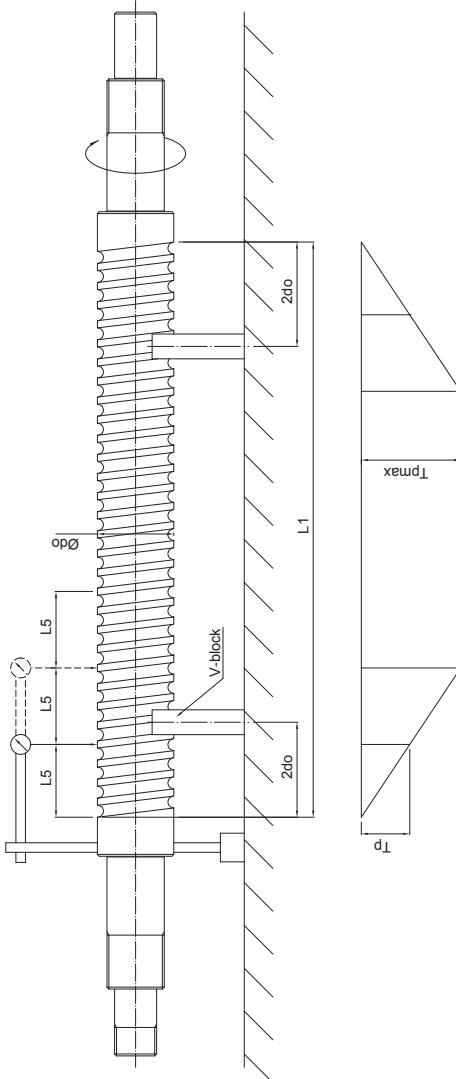


Table 2.6 Total runout in radial direction of outside diameter of screw shaft threaded part in respect to measuring basic length (measuring basic length is according to DIN 69051 and JIS B1192)

Normal diameter <i>d</i> (mm)	Measuring basic length <i>Lr</i>	PMI's Grade <i>Tpmax</i>						
		C0	C1	C2	C3	C4	C5	C7
6	12	-	80					
12	25	160						
25	50	315	20	20	23	25	28	
50	100	630						
100	200	1250						

Slenderness ratio <i>L/d</i> (mm)	Measuring basic length <i>Lr</i>	PMI's Grade <i>Tpmax</i>						
		C0	C1	C2	C3	C4	C5	C7
above up to and incl.	-							
6	40	40	40	45	50	60	64	C10
12	60	60	60	70	75	85	96	160
25	80	100	100	115	125	140	160	240
50	100	160	160	180	200	220	256	400
80								640

Unit:  $\mu\text{m}$

PMI's Grade (*L < Lr*)

Normal diameter <i>d</i> (mm)	Measuring basic length <i>Lr</i>	PMI's Grade ( <i>L &lt; Lr</i> )						
		C0	C1	C2	C3	C4	C5	C7
above up to and incl.	-							
6	20	80	6	8	10	11	12	16
20	50	125	8	10	12	14	16	20
50	125	200	10	12	16	18	20	26
125	200	315	-	-	20	25	32	40

Unit:  $\mu\text{m}$

PMI's Grade (*L < Lr*)

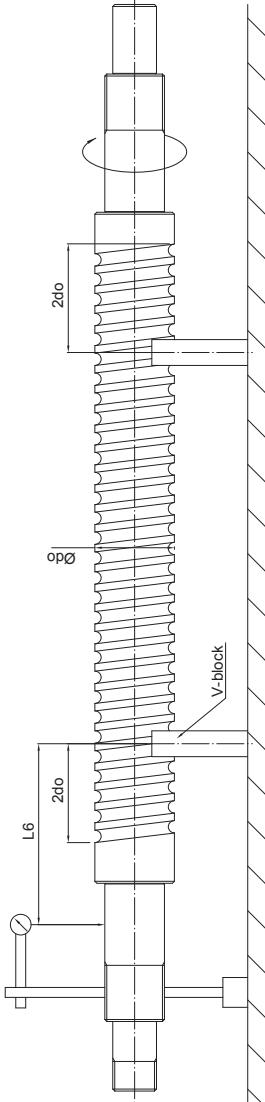


Table 2.7 Circumferential runout in radial direction of outside diameter of mounting part of parts in respect to threaded part axial line of screw shaft (measuring basic length is according to DIN 69051 and JIS B1192)

Normal diameter <i>d</i> (mm)	Measuring basic length <i>Lr</i>	PMI's Grade ( <i>L &lt; Lr</i> )						
		C0	C1	C2	C3	C4	C5	C7
above up to and incl.	-							
6	20	80	6	8	10	11	12	16
20	50	125	8	10	12	14	16	20
50	125	200	10	12	16	18	20	26
125	200	315	-	-	20	25	32	40

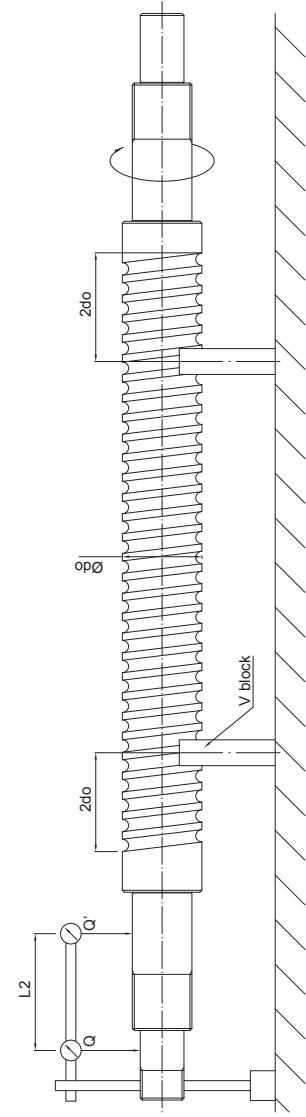


Table 2.8 Perpendicularity on supporting-part end face in respect to the threaded part axial line of screw shaft  
(measuring basic length is according to DIN 69051 and JIS B1192)(Difference of maximum value within Q and Q')  
Unit:  $\mu\text{m}$

Normal diameter $d(\text{mm})$	Measuring basic length $L_b$	PMI's Grade ( $L_2 \leq L_p$ )								
		C0	C1	C2	C3	C4	C5	C6	C7	C10
6	20	80	4	5	5	6	7	8	12	16
20	50	125	5	6	7	8	9	10	16	20
50	125	200	6	7	8	9	10	11	20	25
125	200	315	-	-	10	12	14	16	25	32

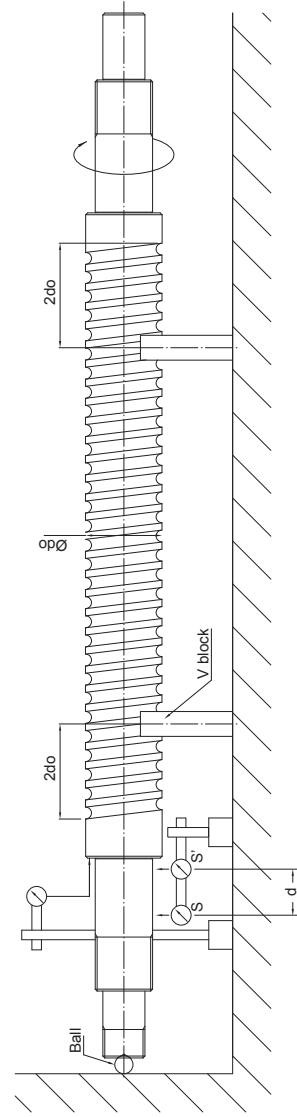


Table 2.9 Perpendicularity on supporting-part end face in respect to the threaded part axial line of screw shaft  
(measuring basic length is according to DIN 69051 and JIS B1192)(the value of deflection supports two ends'  
deflection of difference between S and S')  
Unit:  $\mu\text{m}$

Normal diameter $d(\text{mm})$	Measuring basic length $L_b$	PMI's Grade								
		C0	C1	C2	C3	C4	C5	C6	C7	C10
6	63	3	3	3	4	4	5	5	6	10
63	125	3	4	4	5	5	6	6	8	12
125	200	-	-	6	6	8	8	10	16	

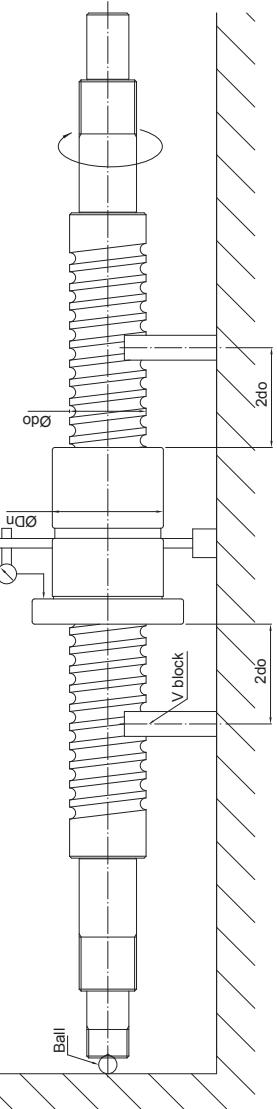


Table 2.10 Perpendicularity on mounting face of flange of nut  
(measuring basic length is according to DIN 69051 and JIS B1192)

Outside diameter of nut $D_n$	PMI's Grade									
	up to and incl. above	C0	C1	C2	C3	C4	C5	C6	C7	C10
-	20	5	6	7	8	9	10	12	14	-
20	32	5	6	7	8	9	10	12	14	-
32	50	6	7	8	9	10	11	15	18	-
50	80	7	8	9	10	12	13	16	18	-
80	125	7	9	10	12	14	15	18	20	-
125	160	8	10	11	13	15	17	19	20	-
160	200	-	11	12	14	16	18	22	25	-
200	250	-	12	14	15	18	20	25	30	-

Unit:  $\mu\text{m}$

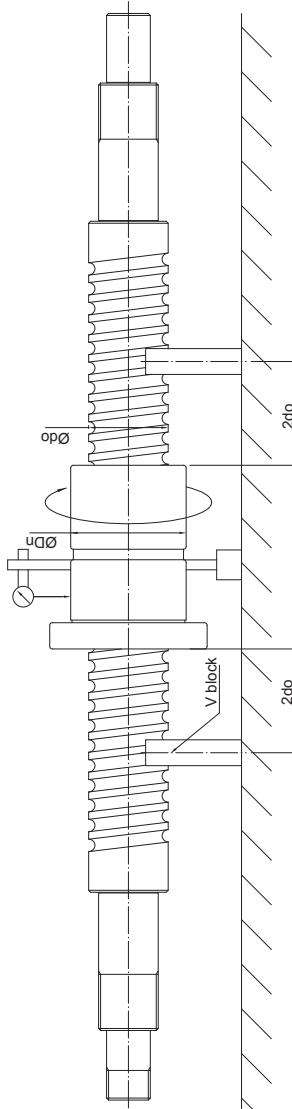


Table 2.11 Circumferential runout in radial direction on outer peripheral face of nut  
(measuring basic length is according to DIN 69051 and JIS B1192)

Outside diameter of nut $D_n$	PMI's Grade									
	up to and incl. above	C0	C1	C2	C3	C4	C5	C6	C7	C10
-	20	5	6	7	8	10	11	12	16	20
20	32	6	7	8	10	12	14	15	20	25
32	50	7	8	10	12	14	15	20	25	-
50	80	8	10	12	15	17	19	25	30	-
80	125	9	12	16	20	21	22	25	40	-
125	160	10	13	17	22	25	28	32	40	-
160	200	-	16	20	22	25	28	32	40	-
200	250	-	17	20	22	25	28	32	40	-

Unit:  $\mu\text{m}$

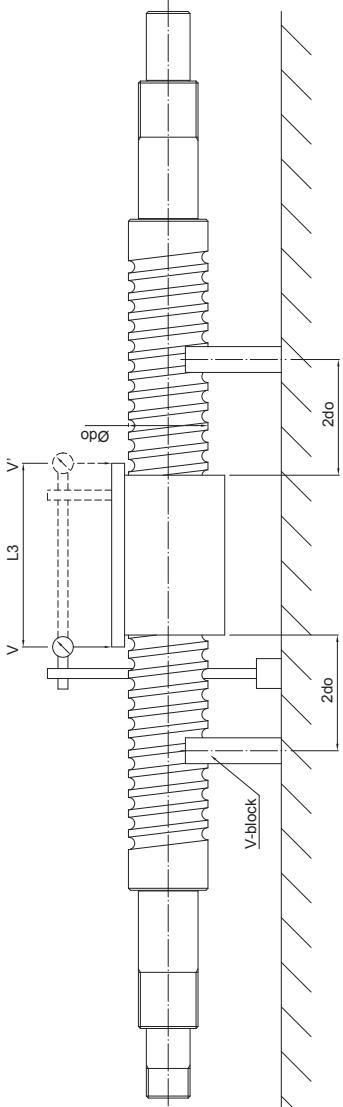


Table 212 Parallelism on outer peripheral face of nut  
( $V-V$ )(measuring basic length is according to DIN 69051 and JIS B1192)

Measuring basic length $L_3$		PMI's Grade								
above	up to and incl	C0	C1	C2	C3	C4	C5	C6	C7	C10
-	50	5	6	7	8	9	10	14	17	-
50	100	6	7	8	10	11	12	15	17	-
100	200	-	10	11	13	15	17	24	30	-

Unit:  $\mu m$

### 3.1 Production Limit Length of Screw Shaft

**Production limit length of precision ground Ballscrew:**

When screw shaft O.D. is 4 mm, Limit length of Ballscrew is 150 mm.

When screw shaft O.D. is 120 mm, Limit length of Ballscrew is 10000 mm.

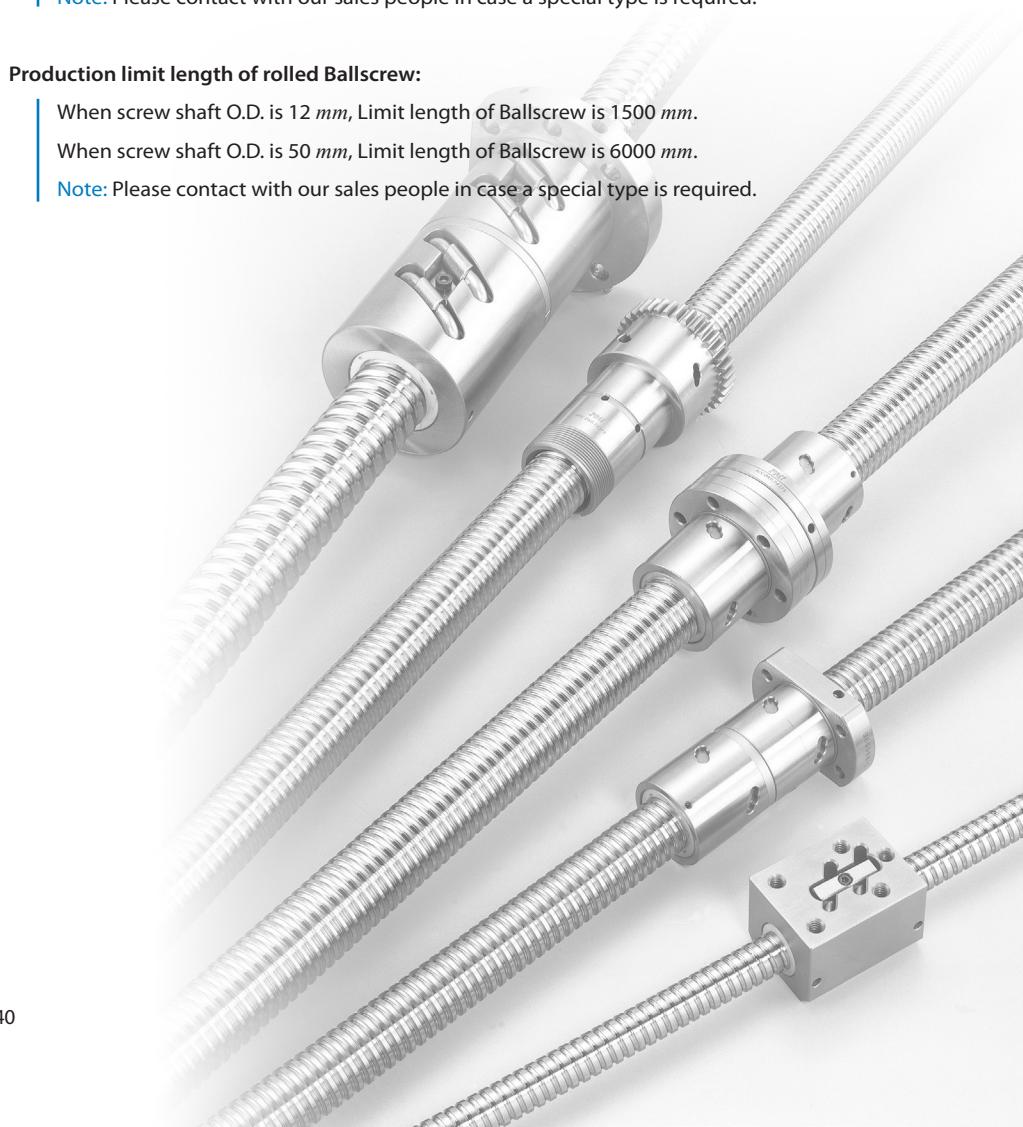
**Note:** Please contact with our sales people in case a special type is required.

**Production limit length of rolled Ballscrew:**

When screw shaft O.D. is 12 mm, Limit length of Ballscrew is 1500 mm.

When screw shaft O.D. is 50 mm, Limit length of Ballscrew is 6000 mm.

**Note:** Please contact with our sales people in case a special type is required.



### 3.2 Method for Mounting

The permissible axial load and permissible rotational speed vary with the screw-shaft mounting method used, so the mounting method should be determined in accordance with the operating conditions.

Diagrams 3.1~3.3 illustrate a typical method for mounting a screw shaft.

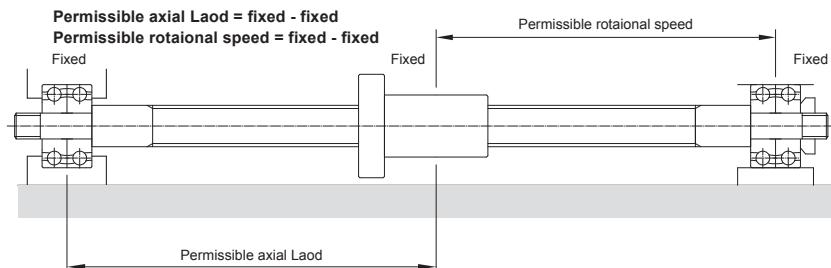


Fig.3.1 Mount method : fixed-fixed

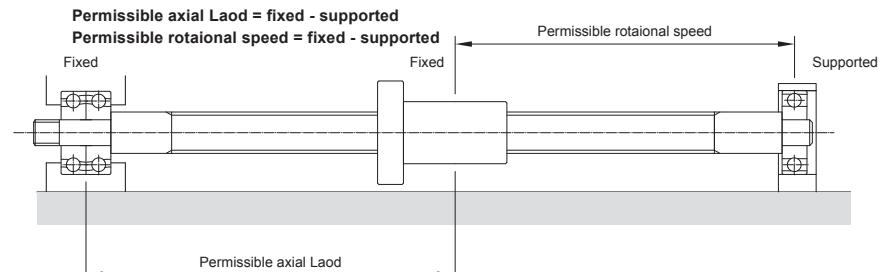


Fig.3.2 Mount method : fixed-supported

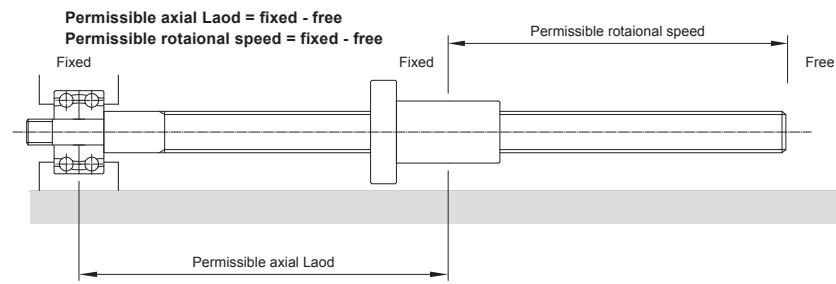


Fig.3.3 Mount method : fixed-free

### 3.3 Permissible Axial Load

#### (1) Buckling load :

The Ballscrew to be used should not buckle under the maximum compressive load applied in its axial direction. The buckling load can be calculated by using equation (3.1):

$$P = \alpha \frac{\pi^2 N EI}{L^2} = m \frac{dr^4}{L^2} \times 10^3 \quad (\text{kgf}) \quad \dots \dots \dots \quad (3.1)$$

Here:

- $\alpha$  Safety factor ( $\alpha=0.5$ )
- $E$  Young's modulus ( $E=2.1 \times 10^4 \text{ kgf/mm}^2$ )
- $I$  Minimum geometrical moment of inertia of the screw shaft cross section ( $I=\pi dr^4/64 \text{ mm}^4$ )
- $dr$  Screw shaft thread minor diameter (mm)
- $L$  Distance between mounting positions (mm)
- $m \cdot N$  Coefficient depending on the mounting method
  - supported-supported  $m=5.1$  ( $N=1$ )
  - fixed-supported  $m=10.2$  ( $N=2$ )
  - fixed-fixed  $m=20.3$  ( $N=4$ )
  - fixed-free  $m=1.3$  ( $N=1/4$ )

#### (2) Permissible tensile-compressive load of the screw shaft :

Where the axial load is exerted on the Ballscrew, the screw shaft to be used should be determined in consideration of the permissible tensile-compressive load that can exert yielding stress on the screw shaft.

The permissible tensile-compressive load can be calculated using equation (3.2).

a. Permissible tensile-compressive load of yield stress of screw shaft

$$P = \sigma \cdot A = \sigma \cdot \pi \cdot dr^2/4 \quad \dots \dots \dots \quad (3.2)$$

Here:

- $\sigma$  Permissible tensile-compressive stress ( $\text{kgf/mm}^2$ )
- $A$  Cross section area of root diameter of screw shaft ( $\text{mm}^2$ )
- $dr$  Screw-shaft thread minor diameter (mm)

#### b. Permissible Load of contact point of ball groove

The maximal axial load must be less than the basic static rate load of the ball screw shaft. For more details please see section 6.3, the permissible load of ball groove.

Fig. Value shown(outer diameter of screw shaft-lead)

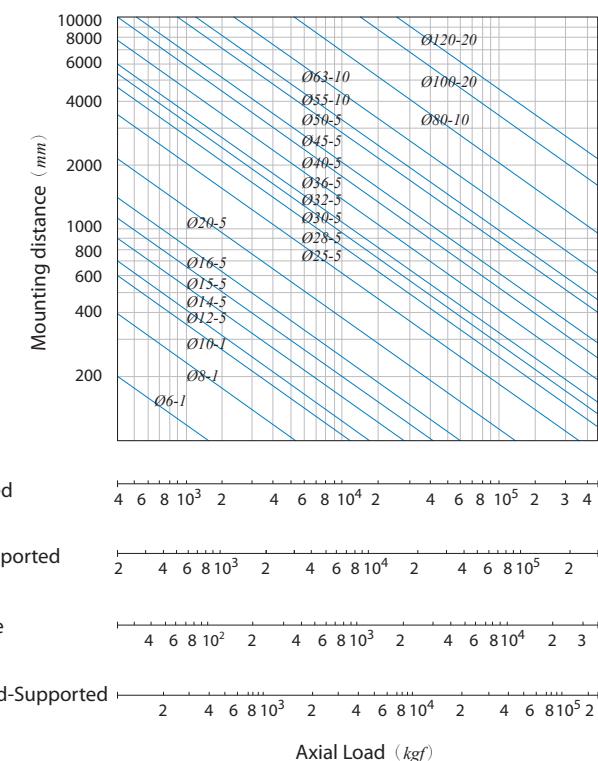


Fig. 3.4 Permissible Axial Load



Fig. Value shown(outer diameter of screw shaft-lead)

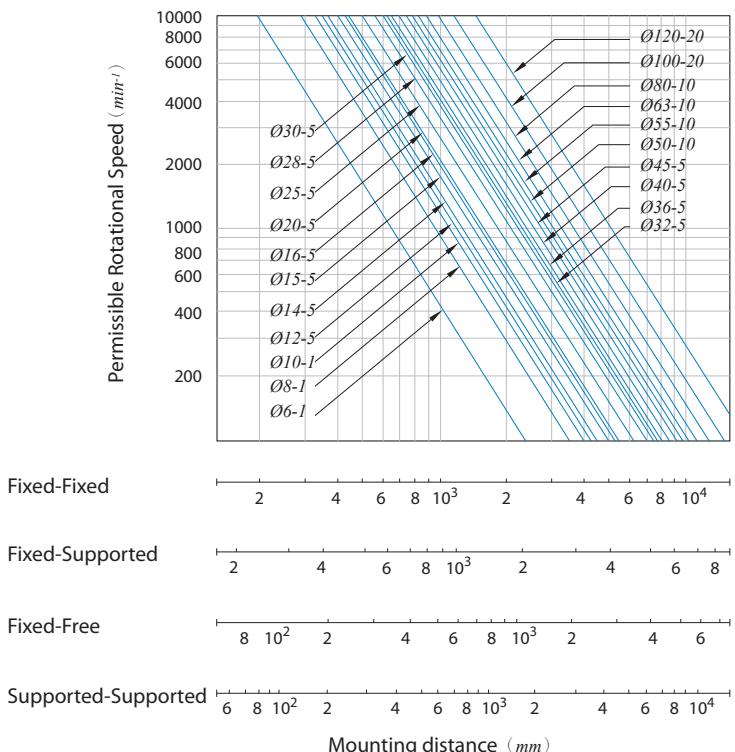


Fig.3.5 Permissible Rotational Speed

### 3.5 Notes on Screw shaft design

#### (1) Through end thread:

For the Ballscrews with internal ball circulation Ballnut, it is required to have at least one end with complete thread to the end of Ballscrew for Ballnut assembly to screw shaft. If it is impossible for through end thread, it is required to have at least one end with complete thread and the journal area is with diameter to be 0.2mm smaller than the diameter of thread root area.

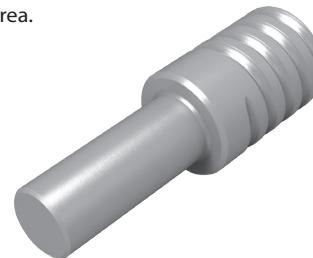


Fig. 3.6.1 Incomplete thread

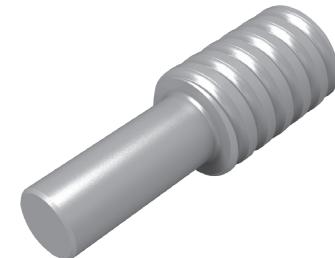


Fig. 3.6.2 Through end thread

#### (2) Machine design for the area of Ballnut and ends area of Ballscrew:

It is very important to check if there is enough space for assembly of Ballscrew onto the machine during machine design. In some cases, there is not enough space for assembly and the Ballnut has to be disassembled from the screw shaft for easier work. It may cause problems, such as the balls falling out from Ballnut, worse accuracy of squareness and roundout of Ballnut, change of preload and damage to external ball circulating tubes. In some more serious cases, the ballscrew may be damaged and not to be used. Please contact with our people if said above disassembling is required.

#### (3) Not effective hardened area:

The threads on screw shaft are hardened by induction hardening. It shall cause about 15mm at both ends of thread area are not hard enough. It is required to pay attention during machine design for the effective thread length of travel.

#### (4) Extra support unit for long ballscrew:

For a long ballscrew, the bending due to self weight might happen. It may cause radial direction load to ballscrew. The radial direction vibration during rotation might also be more serious. To prevent these problems from happening, it may be required to have extra supports for ballscrew in between the existing supports at both ends. There are two types of supports; one is movable to move along the Ballnut. The other one is fixed type; it is located in a fixed position. The Table must be designed not to hit with this support during moving.

Fixed-Fixed

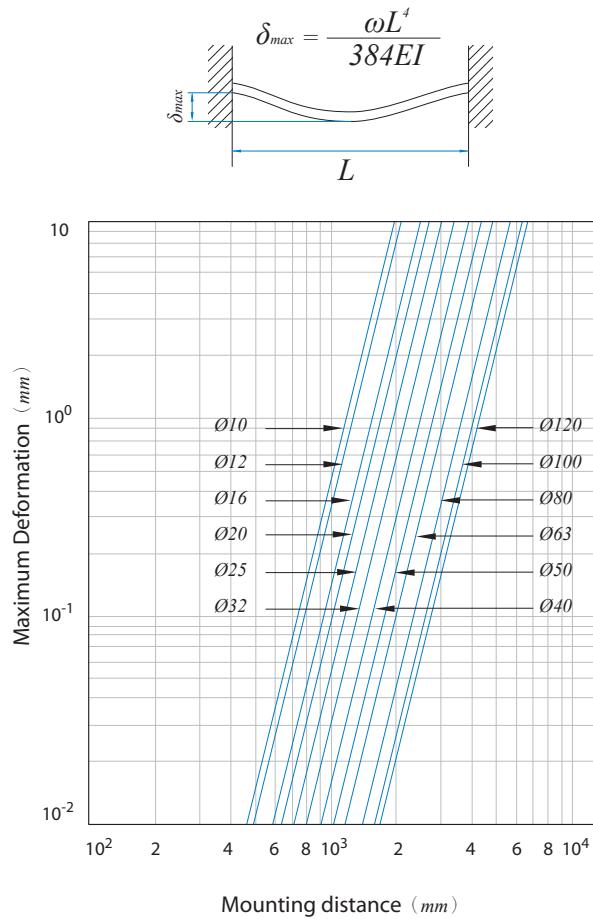


Fig. 3.7.1 Maximum deformation for fixed-fixed

Fixed-Supported

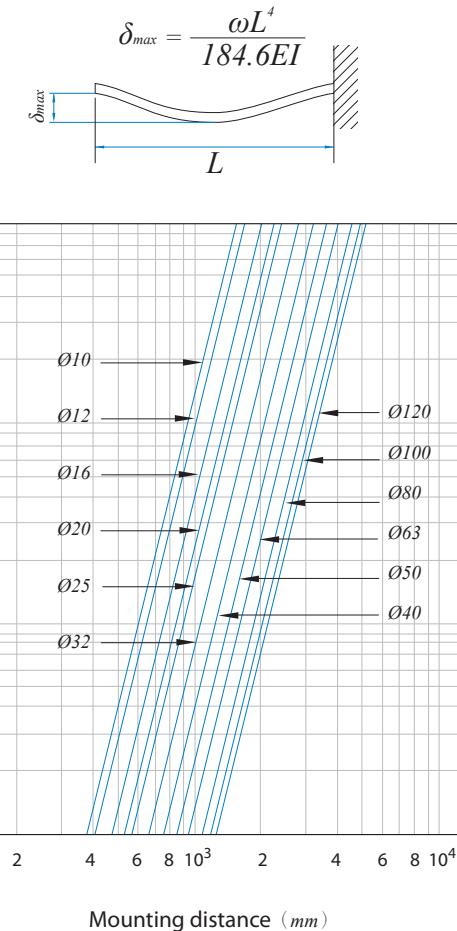


Fig. 3.7.2 Maximum deformation for fixed-supported

## 4.1 Selecting the Type of Nut

### (1) Type:

Selecting the type of Nut, please consider the accuracy; dimension (The length of Nut; internal diameter; external diameter), preload and the date of delivery.

### (2) Circulation:

#### a. External ball circulation:

Advantages

- Lower noise due to longer ball circulation paths
- Offers smoother ball running.
- Offers better solution and quality for long lead or large diameter ballscrews.

#### b. Internal ball circulation:

Advantages:

- Good for limited space of machine.
- Better structure for small lead or small diameter ballscrews.

### (3) Effective turns:

Selecting effective turns have to consider required capability; life and rigidity. Refer to the Table 4.1.

### (4) Flange:

PMI have three standard type (A type, B type and C type) Please make selection by area space for nut installation. PMI can also make special flange as per customers' requests.

### (5) Oil hole:

Standard nuts have oil hole. Please dimension in the diagram to manufacture.

Table4.1 The character of effective turns

Character	External ball circulation	Internal ball circulation
Motion	1.5circuit ×2row, 1.5circuit ×3row, 2.5circuit ×1row	1circuit ×3row, 1circuit ×4row
Rigidity	2.5circuit ×2row, 2.5circuit ×3row	1circuit ×6row

## 4.2 Calculating the Axial Load

### 4.2.1 Horizontal reciprocating moving mechanism

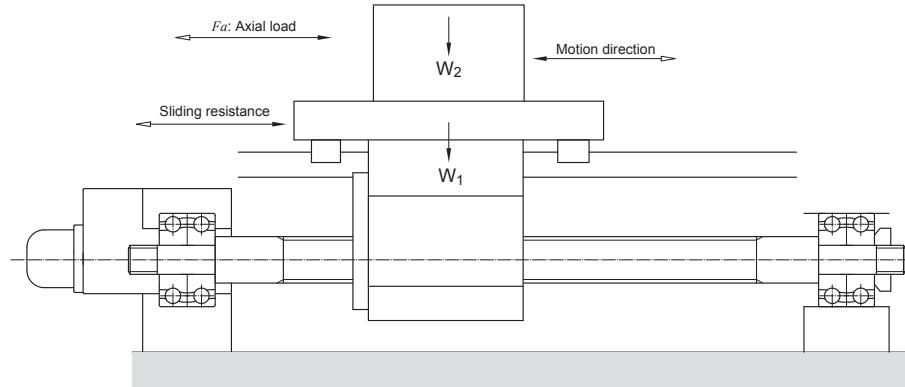


Fig.4.1 Horizontal reciprocating moving mechanism

For reciprocal operation to move work horizontally (back and forth) in an conveyance system, the axial load ( $F_a$ ) can be gotten using the following equations:

$$\text{Acceleration (leftward)} \quad F_{a1} = \mu \times mg + f + ma \quad \dots\dots\dots(4.1)$$

$$\text{Constant speed (leftward)} \quad F_{a2} = \mu \times mg + f \quad \dots\dots\dots(4.2)$$

$$\text{Deceleration (leftward)} \quad F_{a3} = \mu \times mg + f - ma \quad \dots\dots\dots(4.3)$$

$$\text{Acceleration (rightward)} \quad F_{a4} = -\mu \times mg - f - ma \quad \dots\dots\dots(4.4)$$

$$\text{Constant speed (rightward)} \quad F_{a5} = -\mu \times mg - f \quad \dots\dots\dots(4.5)$$

$$\text{Deceleration (rightward)} \quad F_{a6} = -\mu \times mg - f + ma \quad \dots\dots\dots(4.6)$$

Here:

*a* Acceleration

$$a = \frac{V_{max}}{t_a} \quad \begin{matrix} V_{max} \\ t_a \end{matrix} \quad \begin{matrix} \text{Rapid feed speed} \\ \text{time} \end{matrix}$$

*m* Total weight (table weight + work piece weight)

*μ* Friction coefficient of sliding surface

*f* Non-load resistance

#### 4.2.2 Vertical reciprocating moving mechanism

For reciprocal operation to move work vertically (up and down) in an conveyance system, the axial load ( $F_a$ ) can be gotten using the following equations:

$$\text{Acceleration (upward)} \quad F_{a_1}=mg+f+ma \quad \dots\dots\dots(4.7)$$

$$\text{Constant speed (upward)} \quad F_{a_2}=mg+f \quad \dots\dots\dots(4.8)$$

$$\text{Deceleration (upward)} \quad F_{a_3}=mg+f-ma \quad \dots\dots\dots(4.9)$$

$$\text{Acceleration (downward)} \quad F_{a_4}=mg-f-ma \quad \dots\dots\dots(4.10)$$

$$\text{Constant speed (downward)} \quad F_{a_5}=mg-f \quad \dots\dots\dots(4.11)$$

$$\text{Deceleration (downward)} \quad F_{a_6}=mg-f+ma \quad \dots\dots\dots(4.12)$$

Here:

*a* Acceleration

$$a = \frac{V_{\max}}{t_a} \quad \begin{matrix} V_{\max} \\ t_a \end{matrix} \quad \begin{matrix} \text{Rapid feed speed} \\ \text{time} \end{matrix}$$

*m* Total weight(table weight + work piece weight)

*μ* Friction coefficient of sliding surface

*f* Non-load resistance

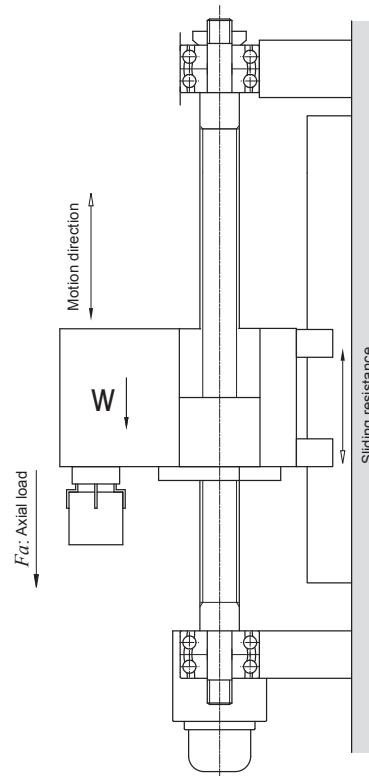


Fig.4.2 Vertical reciprocating moving mechanism

#### 4.3 Notes on Ball Nut Design

##### Abnormal load: (torsional load or radial load)

When Ballscrew takes only axial load, the best performance of it shall be found; the balls on the groove in between the Ballnut and screw shaft shall evenly take the load and rotate smoothly. In case there is torsional load or radial load on Ballnut, this kind load shall be taken unevenly by some balls only. It shall badly affect Ballscrew performance and even shorten ballscrew life. It is recommended to pay more attention to the mechanism design and Ballscrew assembly.

## 5.1 Axial Rigidity

"Lost Motion" shall happen due to weakness of rigidity of screw shaft and mating components of it. In order to get good positioning accuracy, it is necessary to consider axial and torsional rigidity of screw shaft and mating components of it.

### 5.1.1 Axial rigidity of the feed-screw system

Let the axial rigidity of a feed-screw system be  $K$ . Then, the elastic displacement in the axial direction can be obtained using equation (5.1)

$$\delta = \frac{Fa}{K_T} \quad (5.1)$$

$$\frac{1}{K_T} = \frac{1}{K_S} + \frac{1}{K_N} + \frac{1}{K_B} + \frac{1}{K_H} \quad (5.2)$$

Here

$\delta$  Feed-screw system elastic displacement in the axial direction ( $\mu m$ )

$F_a$  Axial load ( $kgf$ )

$K_T$  Axial rigidity of the feed-screw system ( $kgf/\mu m$ )

$K_S$  Axial rigidity of the screw shaft ( $kgf/\mu m$ )

$K_N$  Axial rigidity of the Nut ( $kgf/\mu m$ )

$K_B$  Axial rigidity of the support bearing ( $kgf/\mu m$ )

$K_H$  Rigidity of the Nut Bracket and support bearing bracket ( $kgf/\mu m$ )

#### (1) Axial rigidity of Screw shaft: $K_s$

The axial rigidity of a screw shaft varies depending on the shaft mounting method.

##### a. fixed - free (Axial direction)

$$K_s = \frac{A \times E}{x} \times 10^{-3} \quad (5.3)$$

Here

$K_s$  Axial rigidity of Screw shaft ( $kgf/\mu m$ )

$A$  Screw shaft cross-sectional area ( $A = \pi \cdot dr^2 / 4 \text{ mm}^2$ )

$dr$  Screw shaft thread minor diameter ( $mm$ )

$E$  Young's modulus ( $E = 2.1 \times 10^4 \text{ kgf/mm}^2$ )

$x$  Distance between mounting positions ( $mm$ )

##### b.fixed - fixed (Axial direction)

$$K_s = \frac{A \times E \times L}{x(L-x)} \times 10^{-3} \quad (5.4)$$

Here

$K_s$  Axial rigidity of Screw shaft ( $kgf/\mu m$ )

$L$  Distance between mounting positions ( $mm$ )

Note: Which  $x=L/2$ ,  $K_s$  becomes the minimum and the elastic displacement in the axial direction the maximum.

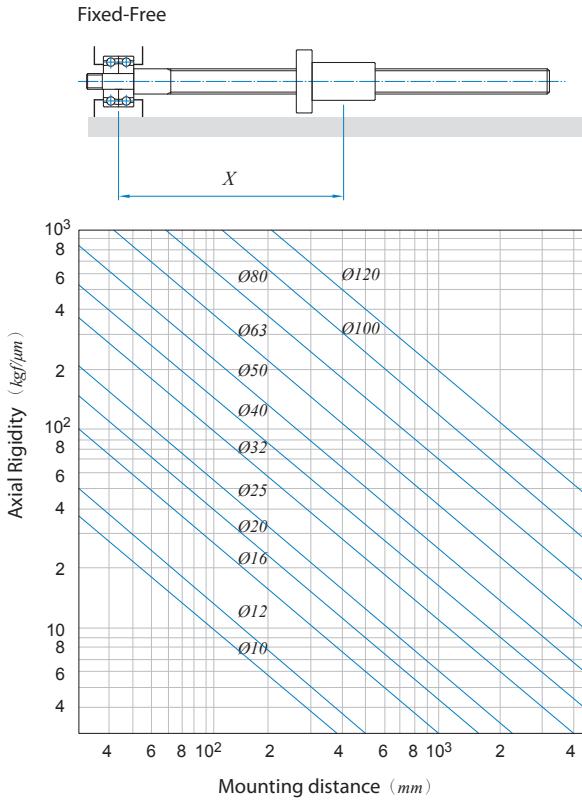


Fig.5.1 Rigidity of ball screw shaft (Fixed-Free)

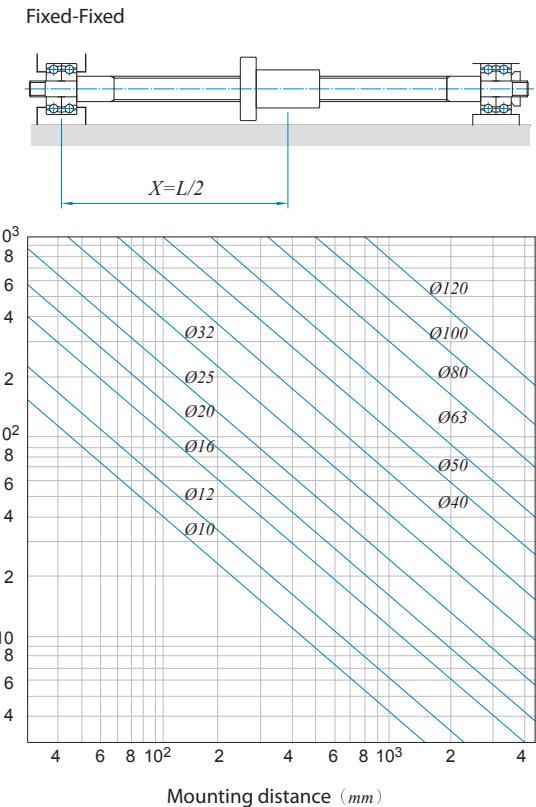


Fig.5.2 Rigidity of ball screw shaft (Fixed-Fixed)

## (2) Axial rigidity of Nut: $K_N$

Computation of the elastic displacement can be using equation (5.5):

$$\delta_a = \frac{C}{\sin \alpha} \left( \frac{Q^2}{D_w} \right)^{1/3} \times \zeta \quad (\mu m) \quad (5.5)$$

Here

- $C$  A constant (reference  $C \approx 2.4$ )
- $\alpha$  Contact angle of ball and grooved
- $D_w$  Ball diameter (mm)
- $Q$  Load of each balls ( $Q = F_a/Z \cdot \sin \alpha \text{ kgf}$ )
- $Z$  Number of balls
- $\zeta$  A coefficient of accuracy and inter conformation

### a.Non-preload type

Dimension tables include theoretical axial rigidity values when the axial load with a magnitude of 30% of the basic dynamic load rating ( $Ca$ ) is exerted on the Nut. These values, don't consider the rigidity of the Nut mounting brackets. Therefore, as a general rule, take 80% of the values given in the table.

When the axial load with a magnitude other than 30% of the basic dynamic load rating ( $Ca$ ) is exerted on the Nut, rigidity value can be calculated using equation (5.6).

$$K_N = 0.8 \times K \left( \frac{F_a}{0.3 Ca} \right)^{1/3} \quad (5.6)$$

here

- $K$  Rigidity value given in the dimension table (kgf/ $\mu m$ )
- $F_a$  Axial load (kgf)
- $Ca$  Basic dynamic load rating (kgf)

### b.Preloaded type

Dimension tables include theoretical axial rigidity values when the axial load with a magnitude of 10% of the basic dynamic load rating ( $Ca$ ) is exerted on the Nut. These values, don't consider the rigidity of the Nut mounting brackets. Therefore, as a general rule, take 80% of the values given in the table.

When the axial load with a magnitude other than 10% of the basic dynamic load rating ( $Ca$ ) is exerted on the Nut, rigidity value can be calculated using equation (5.7).

$$= 0.8 \times K \left( \frac{Fao}{\varepsilon \times Ca} \right)^{1/3} \quad (5.7)$$

here

- $K$  Rigidity value given in the dimension table (kgf/ $\mu m$ )
- $Fao$  Preload
- $\varepsilon$  A coefficient of rigidity  
 $\varepsilon = 0.10$  (spacer preload and offset preload)  
 $\varepsilon = 0.10$  (oversize preload)

## (3) Axial rigidity of support bearing: $K_B$

The axial rigidity of the support bearings for the Ballscrew varies by bearing type. A typical calculation for determining the axial rigidity of an angular ball bearing can be made using equation (5.8).

$$K_B = \frac{3Fao}{\delta_{ao}} \quad (5.8)$$

here

- $\delta_{ao}$  Displacement in the axial direction.

$$\delta_{ao} = \frac{0.44}{\sin \alpha} \left( \frac{Q^2}{D_w} \right)^{1/3} \quad \left. \right\} \quad (5.9)$$

$$Q = \frac{Fao}{Z \times \sin \alpha}$$

- $\alpha$  Initial contact angle of the support bearing
- $D_w$  Ball diameter of the support bearing
- $Q$  Load of each balls
- $Z$  Number of balls

## (4)Axial rigidity of nut bracket and support bearing bracket : $K_H$

Take this into consideration in the design of your system. Setting the rigidity as high as possible.

### 5.1.2 Torsional rigidity of the feed-screw system

The factors of positions error caused by twisting are:

1. Torsional deformation of screw shaft.
2. Torsional deformation of coupling.
3. Torsional deformation of motor.

But above deformations are too small in general machine (non-high speed machine), they are then ignored.

### 5.1.3 Ballscrew's preload and effect

In order to get high positioning accuracy, there are two ways to reach it. One is commonly known as to clear axial play to zero. The other one is to increase Ballscrew rigidity to reduce elastic deformation while taking axial load. Both two ways are done by preloading.

#### (1) Methods of preloading

##### a.Double-nut method:

A spacer inserted between two nuts exerts a preload. There are two ways for it.

One is illustrated in Fig.5.3. That is to use a spacer with thickness complies with required magnitude of preload. The spacer makes the gap between Nut A and B to be bigger, hence to produce a tension force on Nut A and B. It is called "extensive preload".

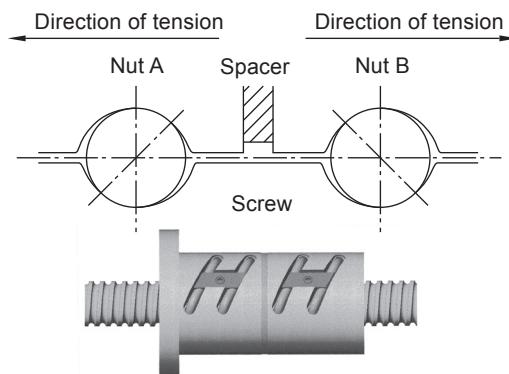


Fig.5.3 Extensive preload

Illustrated in Fig.5.4, is using a thinner spacer. The thickness complies with required magnitude of preload. The spacer is smaller than the gap between Nut A and B, compressing Nut A and B on opposite direction to preload Ballscrews. It's called "compressive preload".

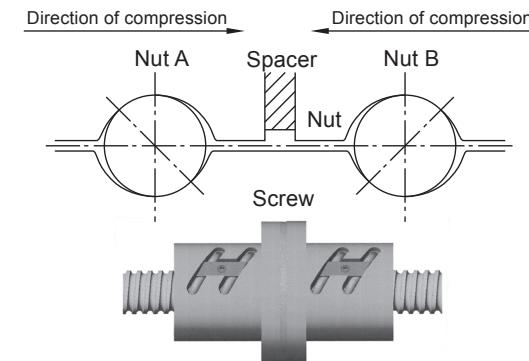


Fig.5.4 Compressive preload

##### b.Single-nut method:

As that illustrated on Fig. 5.5, using oversize balls onto the space between Ballnut and screw to get required preload. The balls shall make four-point contact with grooves of Ballnut and screw.

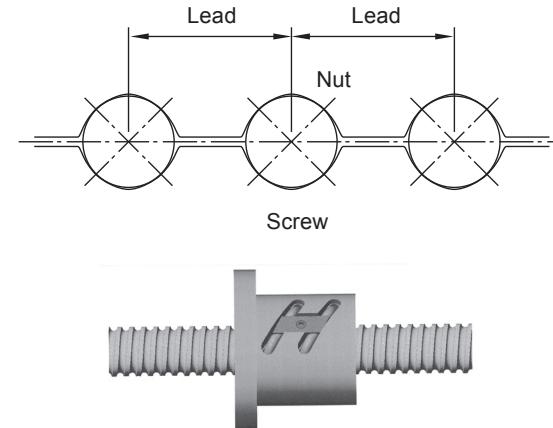


Fig.5.5 Four-point contact preload

There is another way for single nut Ballscrew preloading. That is to shift a very little distance, which complies with required magnitude of preload, on one lead of Ballnut as that illustrated on Fig. 5.6. to preload Ballscrew.

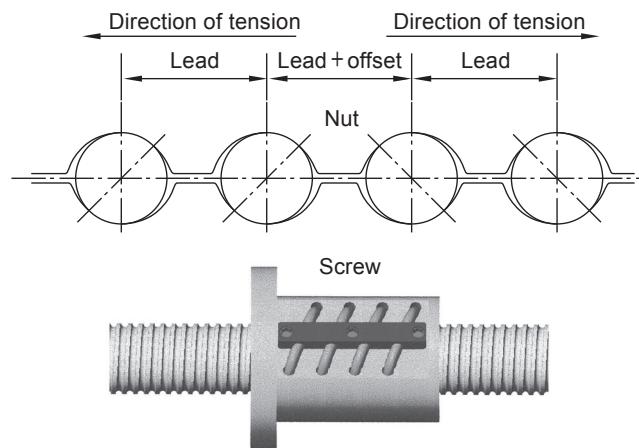


Fig.5.6 Lead offset preload

## (2) Relation between preload force and elastic deformation

Fig 5.7, Nuts A and B are assembled with preloading spacer. The preload forces on Nut A and B are  $F_{ao}$ , but with reversed direction. The elastic deformation on both Nuts are  $\delta_{ao}$ .

Then there is a external axial force  $F_a$  applied to Nut A as shown on Fig 5.6. The deformation of Nut A and B becomes:

$$\delta_A = \delta_{ao} + \delta_{a1}$$

$$\delta_B = \delta_{ao} - \delta_{a1}$$

The load in nut A and nut B are:

$$F_A = F_{ao} + F_a - F_a' = F_a + F_p$$

$$F_B = F_{ao} - F_a' = F_p$$

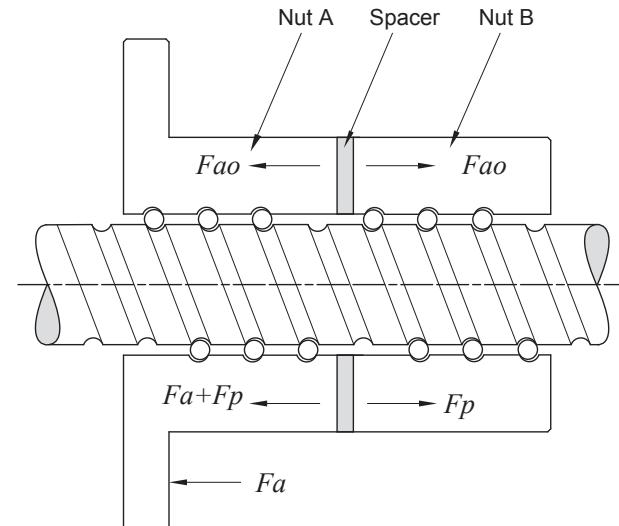


Fig.5.7 Double-nut positioning preload

It means  $F_a$  is offset with an amount  $F_a'$  because of the deformation of Nut B decreases. As a result, the elastic deformation of Nut A is reduced. This effect shall be continued until the deformation of Nut B becomes zero, that is, until the elastic deformation  $\delta_{al}$  caused by the external axial force equals  $\delta_{ao}$ , and the preload force applied to Nut B is completely released. The formula related the external axial force and elastic deformation is shown as below:

$$\begin{aligned}\delta_{ao} &= K \times F_{ao}^{2/3} \quad \text{and} \quad 2\delta_{ao} = K \times F_l^{2/3} \\ (F_l / F_{ao}) &= (2\delta_{ao} / \delta_{ao}) = 2 \\ F_l &= 2.8F_{ao} \approx 3F_{ao}\end{aligned}$$

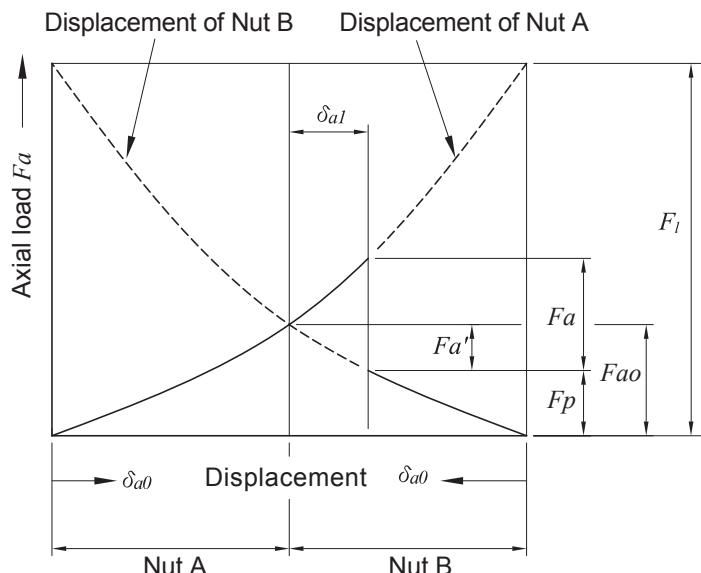


Fig.5.8 Positioning preload diagram

Therefore, the preload amount of a ballscrew is recommended to set as 1/3 of its axial load. Too much preload for a Ballscrew shall cause temperature raise and badly affect its life. However, taking the life and efficiency into consideration, the maximum preload amount of a Ballscrew is commonly set to be 10% of its rated basic dynamic load.

Shown on Fig.5.9, with the axial load to be three times as the preload, the elastic displacement for the non-preloaded ball nut is two times as that of the preloaded nut.

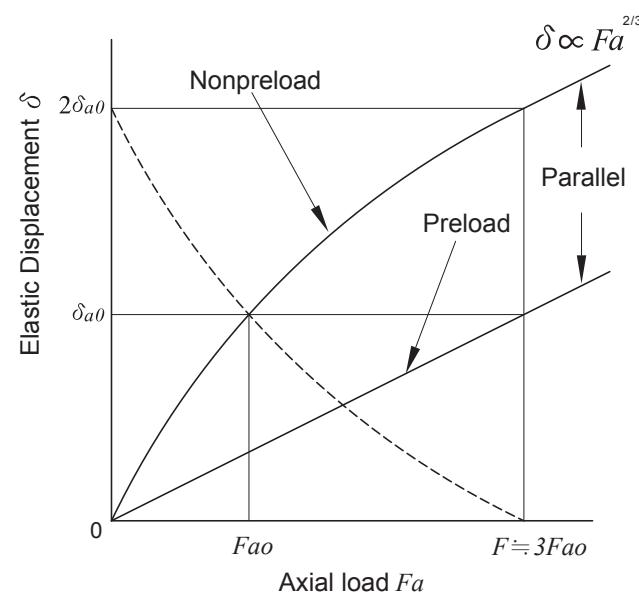


Fig.5.9 Elastic Displacement of the Ballscrew

## 5.2 Positioning Accuracy

### 5.2.1 Causes of error in positioning accuracy

Lead error and rigidity of feed system are common causes of feed accuracy error. Other causes like thermal deformation and feed system assembly are also playing important roles in feed accuracy.

### 5.2.2 Selecting the lead accuracy

Refer to page A22, the Specified travel line should coincide with the nominal travel line. However, in order to compensate either the elongation caused by the thermal expansion during machine operating or the shortening of length due to external load, the specified travel may be set to be positive or negative to the Nominal travel. Machine designer can show the value of Specified travel on the drawing for our manufacturing, or, we can help to decide it based on our more than ten years experience.

There is another way to compensate thermal effect by "pretension" to Ballscrew. Generally, the pretension force shall elongate the Ballscrew to be equivalent to the thermal expansion at about 2-3°C.

### 5.2.3 Considering thermal displacement

If the screw-shaft temperature increases during operation, the heat elongates the screw shaft, thereby reducing the positioning accuracy. Expansion and shrinkage of a screw shaft due to heat can be calculated using equation (5.10).

$$\Delta L_\theta = \rho \cdot \theta \cdot L \quad \dots \dots \dots \quad (5.10)$$

here

- $\Delta L_\theta$  Thermal displacement ( $\mu m$ )
- $\rho$  Thermal-expansion coefficient ( $12 \mu m/m^\circ C$ )
- $\theta$  Screw-shaft temperature change ( $^\circ C$ )
- $L$  Ballscrew length ( $mm$ )

That is to say, an increase in the screw shaft temperature of  $1^\circ C$  expands the shaft by  $12 \mu m$  per meter. The higher the Ballscrew speed, the greater the heat generation. Thus, temperature increases reduce positioning accuracy. Where high accuracy is required, anti-temperature-elevation measures must be provided as follows:

#### (1) To control temperature:

- Selecting appropriate preload.
- Selecting correct and appropriate lubricant.
- Selecting larger lead for the Ballscrew and decrease the rotation speed.

#### (2) Compulsory cooling:

- Ballscrew with hollow cooling.
- Lubrication liquid or cooling air can be used to cool down external surface of Ballscrew.
- Nut cooling system: to reduce temperature of nut by cooling liquid through it.

#### (3) To keep off effect upon temperature raise:

- Set a negative cumulative lead target value for the Ballscrew.
- Warm up the machine to stable machine's operating temperature.
- Pretension by using on Ballscrew while installing onto the machine.
- Use the Closed-loop positioning control.

## 6.1 Life of the Ballscrew

Even though the Ballscrew has been used with correct manner, it shall naturally be worn out and can no longer be used for a specified period. Its life is defined by the period from starting use to ending use caused by nature fail.

- a.Fatigue life - Time period for surface flaking off happened either on balls or on thread grooves.
- b.Accuracy life - Time period for serious loosing of accuracy caused by wearing happened on thread groove surface, hence to make Ballscrew can no longer be used.

## 6.2 Fatigue Life

The basic dynamic rate load ( $C_a$ ) of the Ballscrew is used to calculate its fatigue life when it is operated under a load.

### 6.2.1 Basic dynamic rate load $C_a$

The basic dynamic rate load ( $C_a$ ) is the revolution of  $10^6$  that 90% of identical Ballscrew units in a group, when operated independently of one another under the same conditions, can achieve without developing flaking.

### 6.2.2 Fatigue life

#### (1) Calculating life:

There are three ways to show fatigue life:

- a.Total number of revolutions
- b.Total operating time.
- c.Total travel.

$$L = \left( \frac{C_a}{F_a \times f_w} \right)^3 \times 10^6 \quad (6.1)$$

$$L_t = \frac{L}{60 \times n} \quad (6.2)$$

$$L_s = \frac{L \times l}{10^6} \quad (6.3)$$

here

- $L$  Fatigue life (total number of revolutions)(rev)
- $L_t$  Fatigue life (total operating time)(hr)
- $L_s$  Fatigue life (total travel)(km)
- $C_a$  Basic dynamic rate load(kgf)
- $F_a$  Axial load(kgf)
- $n$  Rotation speed(rpm)
- $l$  Lead(mm)
- $f_w$  Load factor (refer to Table6.1)

Table6.1 Load factor  $f_w$

Vibration and impact	Velocity (V)	$f_w$
Light	$V < 15 \text{ (m/min)}$	$1.0 \sim 1.2$
Medium	$15 < V < 60 \text{ (m/min)}$	$1.2 \sim 1.5$
Heavy	$V > 60 \text{ (m/min)}$	$1.5 \sim 3.0$

Too long or too short fatigue life are not suitable for Ballscrew selection. Using longer life make the Ballscrew's dimensions too large. It's an uneconomical result. Following table is a reference of the Ballscrew's fatigue life.

Machine center .....	20,000 hours
Production machine.....	10,000 hours
Automatic controller.....	15,000 hours
Surveying instruments.....	15,000 hours

**(2)Mean load:**

When axial load changed constantly. It is required to calculate the mean axial load ( $F_m$ ) and the mean rotational speed ( $N_m$ ) for fatigue life. Setting axial load ( $F_a$ ) as Y-axis; rotational number ( $n \cdot t$ ) as X-axis. Getting three kind curves or lines:

**a.Gradational variation curve (Fig.6.1)**

Mean load can be calculated by using equation (6.4):

$$F_m = \left( \frac{F_1^3 \cdot n_1 \cdot t_1 + F_2^3 \cdot n_2 \cdot t_2 + \dots + F_n^3 \cdot n_n \cdot t_n}{n_1 \cdot t_1 + n_2 \cdot t_2 + \dots + n_n \cdot t_n} \right)^{\frac{1}{3}} \quad (6.4)$$

Mean rotational speed can be calculated by using equation (6.5):

$$N_m = \frac{n_1 \cdot t_1 + n_2 \cdot t_2 + \dots + n_n \cdot t_n}{t_1 + t_2 + \dots + t_n} \quad (6.5)$$

Axial load (kgf)	Rotation speed (rpm)	Time Ratio (Sec or %)
$F_1$	$n_1$	$t_1$
$F_2$	$n_2$	$t_2$
.	.	.
$F_n$	$n_n$	$t_n$

**b.Similar straight line (Fig.6.2)**

When mean load variation curve like similar straight line. Mean rotational speed can be calculated using equation (6.6)

$$F_m = \frac{1}{3}(F_{min} + 2F_{max}) \quad (6.6)$$

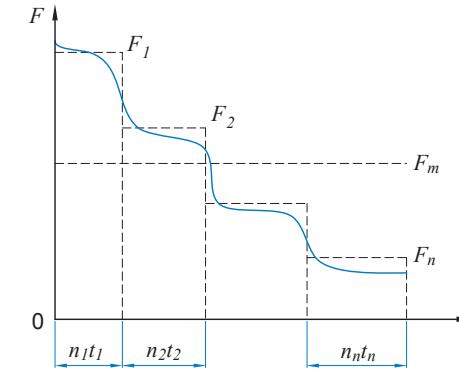


Fig. 6.1 Gradational variation curve's load

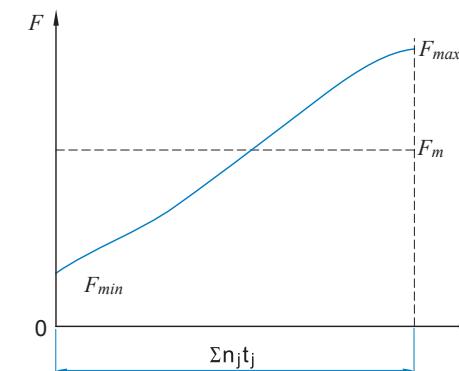


Fig. 6.2 Similar straight line's load

c. Sine curve there are two cases

1. When mean load variation curve shown as the diagram 6.3.1 below. Mean rotational speed can be calculated by using equation (6.7-1):

$$F_m = 0.65F_{max} \quad \dots \dots \dots \quad (6.7-1)$$

2. When mean load variation curve shown as the diagram 6.3.2 below. Mean rotational speed can be calculated by using equation (6.7-2):

$$F_m = 0.75F_{max} \quad \dots \dots \dots \quad (6.7-2)$$

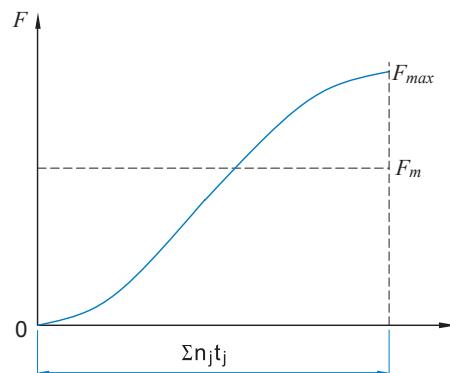


Fig. 6.3.1 Variation like Sine curve's load (1)

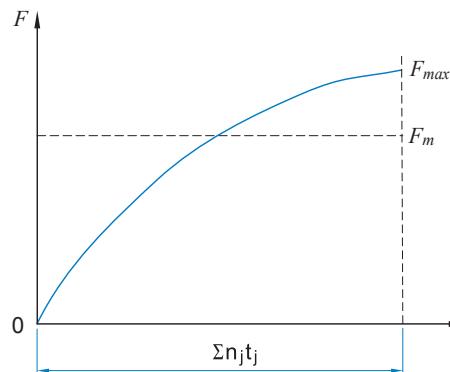


Fig. 6.3.2 Variation like Sine curve's load (2)

### 6.2.3 Affection of installation errors

When twist load or radial load is applied to Ballscrew, there shall be bad effect on ballscrew operation and its life, It is required to make the feed system (Ballscrew, support bearings, Guideways) to be more rigid. Hence to reduce installation errors.

Ballscrews must be meticulously installed onto the Yoke (bracket) of machine to achieve precise parallelism and squareness along moving direction of moving parts. It is very important to ensure minimum backlash happens.

Scales of reference calculate for support torque of ball screw, allow fig.6.4

Nut type : R40-10B2-FSWC

## specification

shaft diameter : 40 mm

ball diameter : 6.35 mm

effective turns : 2.5 circuit x 2 row

Axial play : 50  $\mu$ m

## conditions

Axial force  $F_a=300 \text{ kgf}$

Radial displacement:0

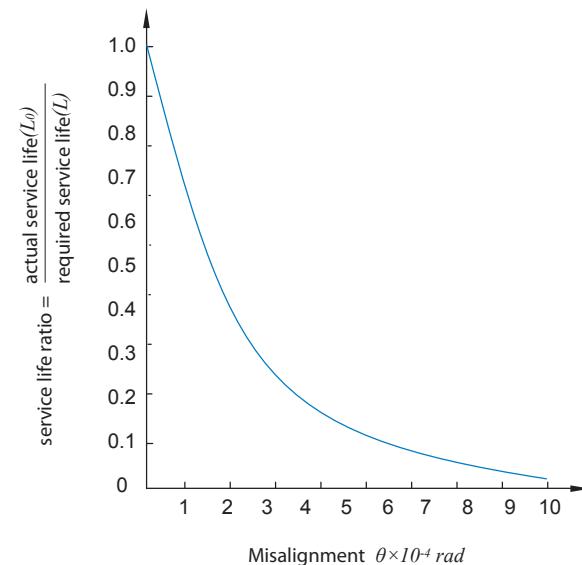


Fig.6.4 The effect on service life of a radial load caused by misalignment

## 6.3 Permissible Load on Thread Grooves

Even though the Ballscrew is seldom operated and is operated under low velocity, it is required to make the maximum load to be far smaller than its rated basic static load when making selection.

### 6.3.1 Basic static rate load $C_o$

The basic static rate load is the static load with a non-varying direction and magnitude that makes the sum of the permanent deformation of the rolling elements and raceway 0.0001 times the rolling element diameter. With the Ballscrew, the basic static rate load is defined in relation to the axial load.

### 6.3.2 Permissible axial load

$$F_{max} = C_o / f_s$$

here

$f_s$  Static safety factor

General industrial machine..... ..... 1.2~2

Machine tool..... ..... 1.5~3

## 6.4 Material and Hardness

### 6.4.1 Material and Hardness of PMI Ballscrews

Table 6.2 Material and hardness of Ballscrews

Denomination	Material	Heat treating	Hardness (HRC)
Precision ground	50CrMo4 QT/ Equivalent	Induction hardening	58~62
Rolled	S55C/ Equivalent	Induction hardening	58~62
Nut	SCM420H/ Equivalent	Carburized hardening	58~62

### 6.4.2 Hardness factor

If used PMI's standard materials else one, for a surface hardness of less than HRC58, the basic dynamic rate load ( $C_a$ ) and the basic static rate load ( $C_o$ ) must be adjusted. Adjustment is made by the following formula. Show in fig. 6.5

$$C_a' = f_H \times C_a$$

$$C_o' = f_{H'} \times C_o$$

Here

$f_H$  Hardness coefficient

$f_{H'}$  Static Hardness coefficient

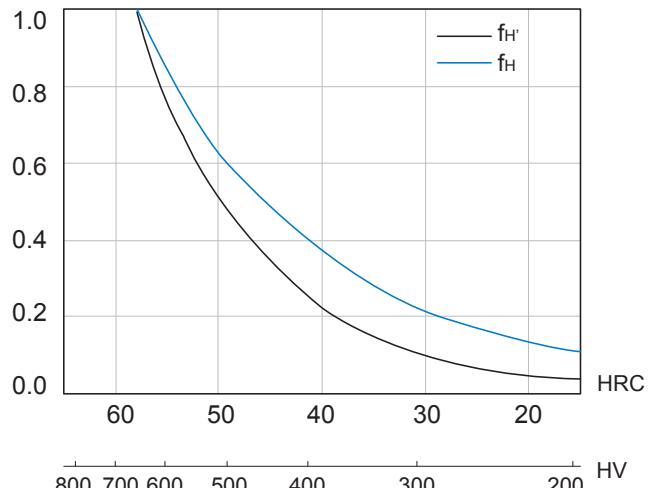


Fig. 6.5 Hardness coefficient

## 6.5 Heat Treating Inspection Certificate



SPECIMEN#	P90227																																																																												
CUSTOMER		P.O.NUMBER	SPECIFICATION																																																																										
PRODUCT	BALLSCREW	03-016030-1	R38-15B2-FSVC-557-685.8-C4																																																																										
MATERIAL	50CrMo4QT																																																																												
HEATTREAT	INDUCTION SURFACE HARDENING																																																																												
ITEM	INSPECTION DATA	<b>HEATTREATEDARE</b> (SEESKETCH)  HARDNESS INSPECTED EVERY 0.5mm (SERIES 2) HARDNESS INSPECTED EVERY 0.5mm (SERIES 1)																																																																											
HARDNESS	58 - 62 HRC AT SURFACE																																																																												
CASEDEPTH	1.5 mm BELOW THREAD ROOT																																																																												
MICRO-STRUCTURE	Martensite IN SURFACE AREA																																																																												
TEMPERING	Sorbit in CORE AREA																																																																												
DEPTH	Series1	Series2																																																																											
0	725	718																																																																											
1	705	698																																																																											
2	704	705																																																																											
3	698	681																																																																											
4	694	642																																																																											
5	679	562																																																																											
6	625	277																																																																											
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<b>HV VS. HRC</b> <table border="1"> <thead> <tr> <th>HV</th> <th>HRC</th> </tr> </thead> <tbody> <tr><td>800</td><td>64.0</td></tr> <tr><td>780</td><td>63.3</td></tr> <tr><td>760</td><td>62.5</td></tr> <tr><td>740</td><td>61.8</td></tr> <tr><td>720</td><td>61.0</td></tr> <tr><td>700</td><td>60.1</td></tr> <tr><td>690</td><td>59.7</td></tr> <tr><td>680</td><td>59.2</td></tr> <tr><td>670</td><td>58.8</td></tr> <tr><td>660</td><td>58.3</td></tr> <tr><td>650</td><td>57.8</td></tr> <tr><td>640</td><td>57.3</td></tr> <tr><td>630</td><td>56.8</td></tr> <tr><td>620</td><td>56.3</td></tr> <tr><td>610</td><td>55.7</td></tr> <tr><td>600</td><td>55.2</td></tr> <tr><td>590</td><td>54.7</td></tr> <tr><td>580</td><td>54.1</td></tr> <tr><td>570</td><td>53.6</td></tr> <tr><td>560</td><td>53.0</td></tr> <tr><td>540</td><td>51.7</td></tr> <tr><td>520</td><td>50.5</td></tr> <tr><td>500</td><td>49.1</td></tr> <tr><td>480</td><td>47.7</td></tr> <tr><td>460</td><td>46.1</td></tr> <tr><td>440</td><td>44.5</td></tr> <tr><td>420</td><td>42.7</td></tr> <tr><td>400</td><td>40.8</td></tr> <tr><td>380</td><td>38.8</td></tr> <tr><td>360</td><td>36.6</td></tr> <tr><td>340</td><td>34.4</td></tr> <tr><td>320</td><td>32.2</td></tr> <tr><td>300</td><td>29.8</td></tr> <tr><td>280</td><td>27.1</td></tr> <tr><td>260</td><td>24.0</td></tr> <tr><td>240</td><td>20.3</td></tr> </tbody> </table>				HV	HRC	800	64.0	780	63.3	760	62.5	740	61.8	720	61.0	700	60.1	690	59.7	680	59.2	670	58.8	660	58.3	650	57.8	640	57.3	630	56.8	620	56.3	610	55.7	600	55.2	590	54.7	580	54.1	570	53.6	560	53.0	540	51.7	520	50.5	500	49.1	480	47.7	460	46.1	440	44.5	420	42.7	400	40.8	380	38.8	360	36.6	340	34.4	320	32.2	300	29.8	280	27.1	260	24.0	240	20.3
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## 6.6 Lubrication

Lithium base lubricants are used for Ballscrew lubrication.

Their viscosity are 30~140 cst (40 °C) and ISO grades of 32~100.

Selecting:

- 1.High speed or Low temperature application: Using the lower viscosity lubricant.
- 2.High temperature, high load and low speed application: Using the higher viscosity lubricant.

Table 6.3 Checking and supply interval of lubricant

Manner	Checking interval	Checking item	Supply or replacing interval
Automatic interval oil supply	every week	oil volume and purity	To supply on each check, its volume depends on oil tank capacity
Lubricating grease	Within 2-3 months after starting operation of machine	foreign matter	Normally supply once a year as per the result of check
Oil bath	everyday before operation of machine	oil surface	To supply as per wasting condition

Table 6.4 calculate of supply lubricate oil

Lubrication method	Principles of inspection and add
oil	<p>Checked and add depending on the tank capacity every week. Oil should be changed when oil is dirty.</p> <p>Calculation of oil Capacity :</p> $\text{Capacity of supply oil every 10 min. } Q = \frac{\text{Shaft diameter(mm)}}{90} \text{ c.c.}$

Table 6.5 calculate of supply lubricate grease

Lubrication method	Principles of inspection and add
grease	<p>Checked every 2~3 months after begin of the operation and see whether foreign matter. Change grease when dirty.</p> <p>Add grease depending on the use condition and operation environment.</p> <p>The add capacity should be the 50% of the internal volume of the nut.</p> <p>Avoid using different brands of grease</p>

Ball diameter d	Ø1.558	Ø2.0	Ø2.381	Ø2.778	Ø3.175	Ø3.969	Ø4.762
G value	0.8	1.0	1.0	1.5	1.2	1.3	2.0
Ball diameter d	Ø6.350	Ø7.144	Ø7.938	Ø9.525	Ø12.7	Ø15.875	Ø19.05
G value	3.0	3.5	3.9	5.0	6.0	9.6	12

$$Q = \left[ \left( \sqrt{(\pi \times dm)^2 + Ld^2} \times \pi d^2 \times \text{effective turns} \right) \times \frac{I}{1000} + \left( \frac{\pi L \times (2DG + G^2)}{4} \right) \right] \times \frac{I}{1100}$$

*Q* Capacity of supply lubricate grease(cm<sup>3</sup>)

*D* Shaft diameter(mm)

*d* Ball diameter(mm)

*dm* Ball circle diameter(mm)

*G* Size factor of ball

*Ld* Lead(mm)

*L* Length of Nut(mm)

## 6.7 Dustproof

Same as the rolling bearings, if there is the particles such as chips or water get into the ballscrew, the wearing problem shall be deteriorated. In some serious cases, ballscrew shall then be damaged. In order to prevent these problems from happening, there are wipers assembly at both ends of ballnut and please use the Screw cover or Bellows for better dustproof. Should there be any more information required, please contact us. There is also the "O-Ring" at the wipers to seal the lubrication oil from leaking from ballnut.

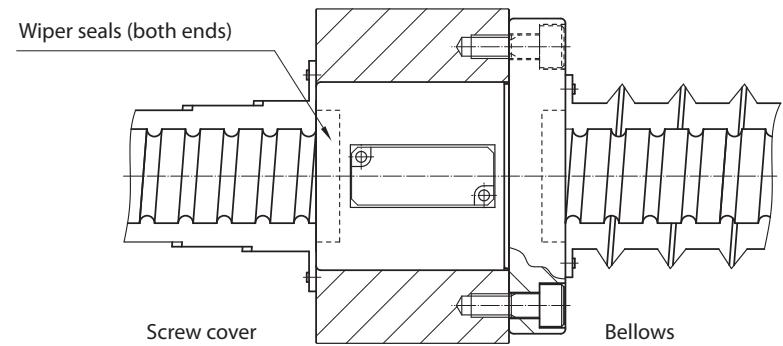


Fig.6.6 Dustproof by screw cover and bellows

## 7.1 Operating Torque of Ballscrew

### (1) Normal Drive

Rotational motion converted to linear motion is called normal drive. The torque required can be obtained by using equation (7.1)

$$T_a = \frac{F_a \times l}{2\pi \times \eta_1} \quad \dots \dots \dots \quad (7.1)$$

here

- $T_a$  Normal operation torque
- $F_a$  Axial load
- $l$  Lead
- $\eta$  Normal efficiency

### (2) Reverse operation

Linear motion converted rotational motion is called reverse operation motion. The torque required can be obtained using equation (7.2):

$$T_b = \frac{F_a \times l \times \eta_2}{2\pi} \quad \dots \dots \dots \quad (7.2)$$

here

- $T_b$  Reverse operation torque
- $\eta_2$  Reverse efficiency

### (3) Preload torque

Friction torque due to preload on the Ballscrew, The torque required can be obtained by using equation (7.3):

$$T_p = k \times \frac{F_{ao} \times l}{2\pi} \quad \dots \dots \dots \quad (7.3)$$

here

- $T_p$  Preload torque
- $F_{ao}$  Preload
- $k$  Coefficient of preload torque  
see equation(2.1)  
 $k=0.05 \times (\tan\beta)^{-0.5}$

## 7.2 Drive Torque of Motor

### (1) Driving torque at constant speed

The torque can counteract load and let Ballscrew to rotate uniformly is called driving torque for constant speed. Driving torque = preloading torque + friction torque for axial load + friction torque for bearing.

$$T_1 = \left( k \times \frac{F_{ao} \cdot l}{2\pi} + \frac{F_a \cdot l}{2\pi \cdot \eta} + T_B \right) \times \frac{N_1}{N_2} \quad \dots \dots \dots \quad (7.4)$$

here

- $T_1$  Driving torque at constant speed
- $F_{ao}$  Preload
- $F_a$  Axial load
- $F$  Cutting resistance
- $\mu$  Guiding surface friction coefficient
- $W$  Total weight (Working table weight + Working object weight)
- $T_B$  Friction torque for bearing
- $N_1$  Gear one
- $N_2$  Gear two

In general, driving torque of constant speed motion shall not over than 30% of rated torque of motor.

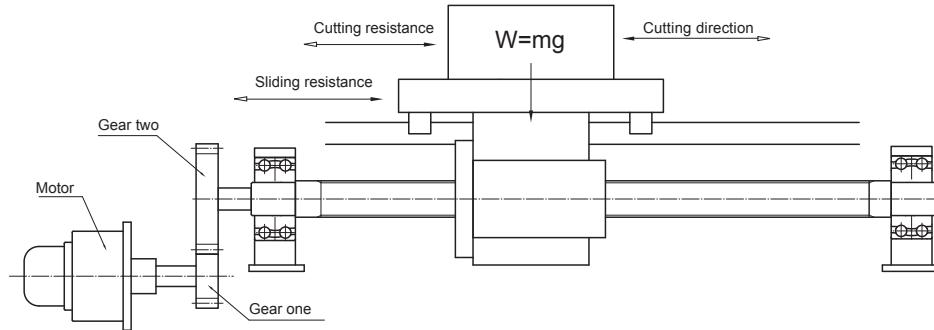


Fig.7.1 Cutting machine diagram

## (2) Driving torque at constant acceleration

The torque required to counteract load and to let Ballscrew to rotate at constant acceleration is driving torque at constant acceleration.

$$T_2 = T_I + J \cdot \dot{\omega} \quad (7.5)$$

$$J = J_M + J_{G1} + \left( \frac{N_1}{N_2} \right)^2 \times [J_{G2} + J_{SH} + J_w + J_C] \quad (7.6)$$

$$J_w = \frac{m}{g} \left( \frac{l}{2\pi} \right)^2 \quad (7.7)$$

Here

$T_2$  Driving torque at constant acceleration

$\dot{\omega}$  Motor's angular acceleration

$J$  Total inertial

$J_M$  Inertial of motor

$J_{G1}$  Inertial of gear one

$J_{G2}$  Inertial of gear two

$J_{SH}$  Inertial of screw shaft

$J_w$  Inertial of moving parts (Ballscrew, Table)

$J_c$  Inertial of Coupling

$m$  Total Masses (Working table mass + working piece mass)

$l$  Lead

$g$  Gravitational acceleration

- Cylindric inertia (Ballscrew, gear)

$$J = \frac{1}{32} \rho \pi D^4 L \quad (\text{kg} \cdot \text{m}^2) \quad (7.8)$$

$$= \frac{\pi r}{32g} D^4 L \quad (\text{kg} \cdot \text{m}^2) \quad (7.9)$$

$$= \frac{mD^2}{8} \quad (\text{kg} \cdot \text{m}^2) \quad (7.10)$$

Here

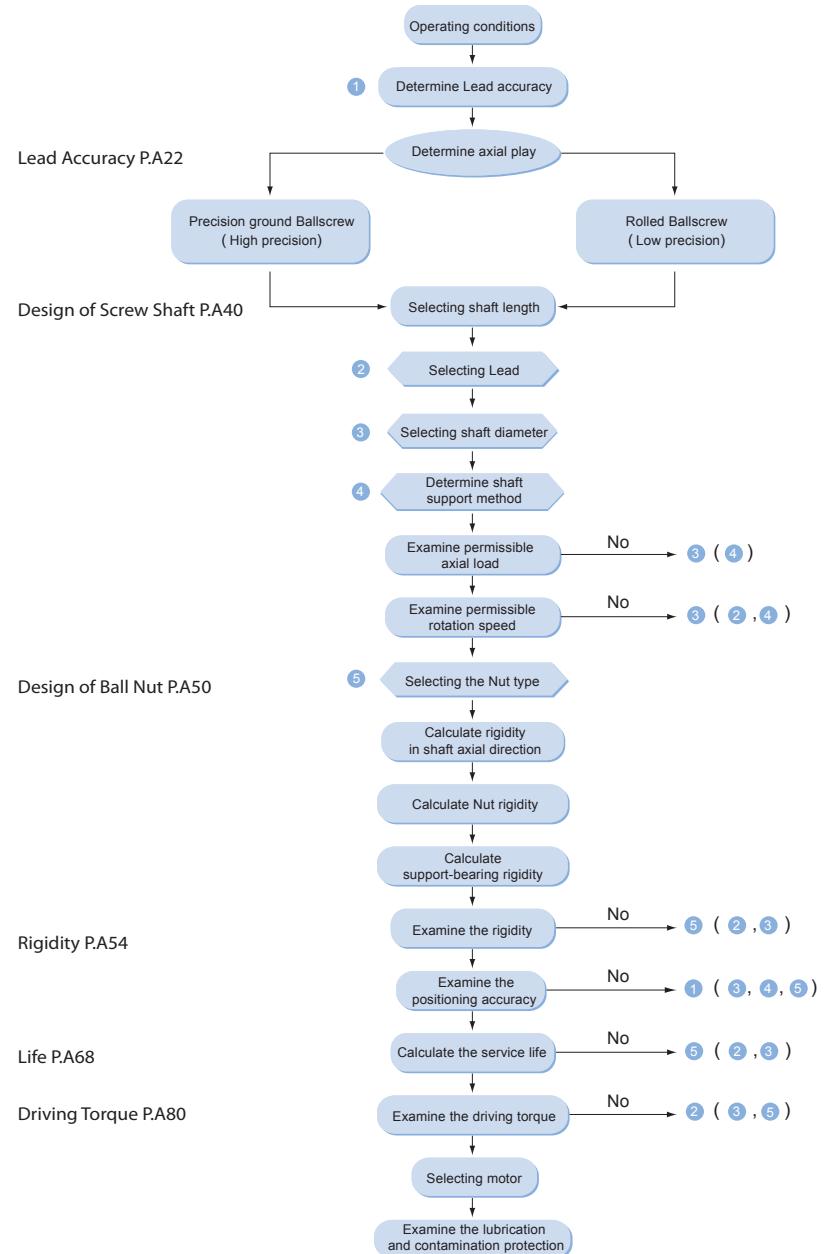
$\rho$  Material Density

$\gamma$  Specific Gravity

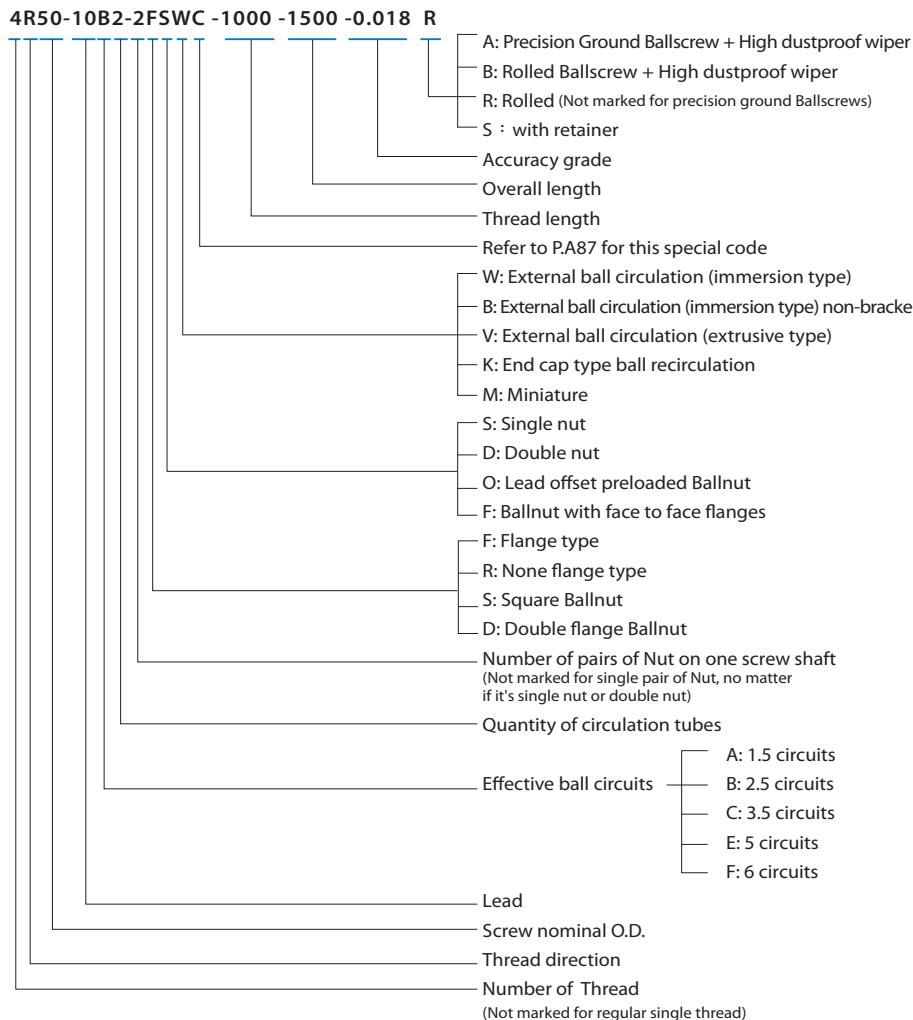
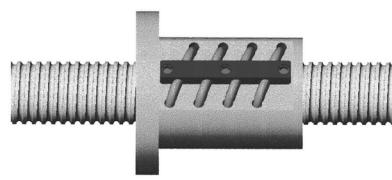
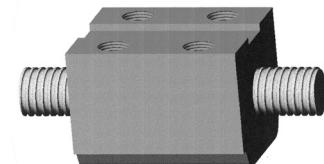
$D$  Diameter of Cylinder

$L$  Length of Cylinder

$m$  Mass of Cylinder



## 9.1 Nomenclature of External Circulation Ballscrew

TYPE  
FDWCTYPE  
DFWCTYPE  
FSWCTYPE  
FOWCTYPE  
RSWCTYPE  
SSWC

## 9.2 Nomenclature of Internal Circulation Ballscrew

4R50-10T 4-2FS I C -1000 -1500 -0.018 R

- A: Precision Ground Ballscrew + High dustproof wiper
- B: Rolled Ballscrew + High dustproof wiper
- R: Rolled (Not marked for precision ground Ballscrews)
- S : with retainer
- Accuracy grade
- Overall length
- Thread length
- Refer to P.A87 for this special code
- I: Internal ball circulation
- D: End Deflector
  
- S: Single nut
- D: Double nut
- O: Lead offset preloaded Ballnut
- F: Ballnut with face to face flanges
- F: Flange type
- R: None flange type
- S: Square Ballnut
- D: Double flange Ballnut
  
- Number of pairs of Nut on one screw shaft  
(Not marked for single pair of Nut, no matter if it's single or double nut)
- Quantity of circulation deflectors (or inserts)
- T: Number of circuit = 1 circuit
- Lead
- Screw nominal O.D.
- Thread direction
- Number of Thread (Not marked for regular single thread)

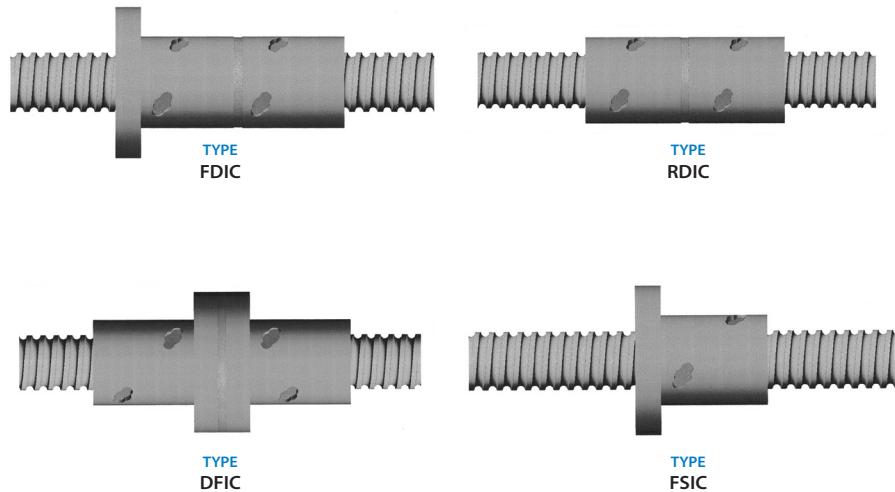


Table 9.1 Special code

C	Precision ground threads
W	Rolled threads
E	E type ball circulation tube (PMI's patent)
Q	Self lubrication
T	Ballnut rotation ( Instead of regular screw shaft rotation type Ballscrew )
D	E type tube + Self lubrication
H	Ballscrews For Heavy Load
N	Nut of DIN type

## 10.1 Cutting Machine

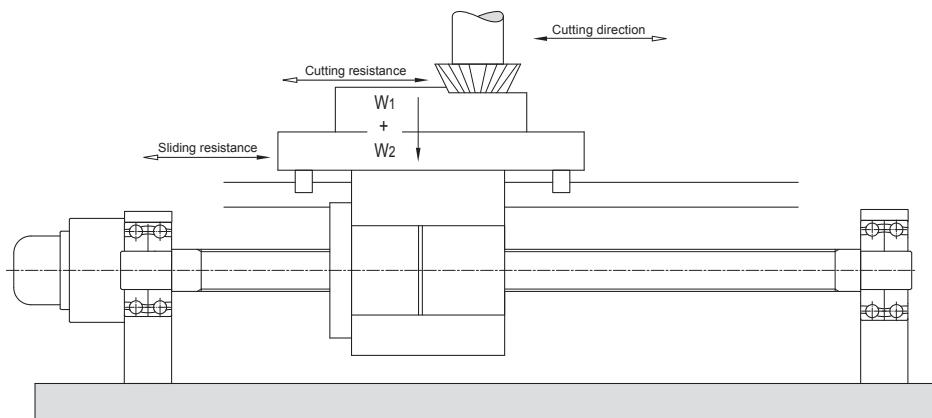


Fig.10.1 Cutting machine

### 1 ▶ Design Conditions

Table weight:	$W_1 = 1100 \text{ kgf}$
Work piece weight:	$W_2 = 800 \text{ kgf}$
Max. travel:	$S_{max} = 1000 \text{ mm}$
Rapid feed speed:	$V_{max} = 14 \text{ m/min}$
Life:	$L_t = 25000 \text{ h}$
Sliding surface friction coefficient:	$\mu = 0.1$
Driving motor:	$N_{max} = 2000 \text{ rpm}$
Positioning accuracy:	$\pm 0.030/1000 \text{ mm}$ (no load)
Repeatability accuracy:	$\pm 0.005 \text{ mm}$ (no load)
Lost Motion:	0.02 mm (no load)

### 2 ▶ Mechanical Conditions

Kinds of Operation	Calculation data		Feed speed <i>mm/min</i>	Time ratio(%)
	Axial load ( <i>kgf</i> )	Time		
Rapid feed	Cutting resistance	190	14000	30
Light cutting	500	190	600	55
Heavy cutting	950	190	120	15

$$\begin{aligned} \text{Sliding resistance: } Fa &= \mu (W_1 + W_2) \\ &= 0.1 \times (1100 + 800) \\ &= 190 \text{ (kgf)} \end{aligned}$$

### 3 ▶ Items to Be Decided

1. Screw nominal O.D., Lead, Type of Nut
2. Accuracy grade
3. Thermal displacement
4. Driving motor

## 1 Selecting Screw nominal O.D., Lead, Nut

(1) Lead(l) :

The highest rotation speed of motor

$$l \geq \frac{V_{max}}{N_{max}} = \frac{14000}{2000} = 7 \text{ (mm)}$$

◎Lead have to be 7mm or more.

(As per PMI catalog: select 8 and 10 mm for further analysis)

## (2) Basic dynamic rate load (Ca)

Kinds of Operation	Calculation data	Axial load		Feed speed		Time
				$l = 8$	$l = 10$	
Rapid feed		$F_1 = 190$		$N_1 = 1750$	$N_1 = 1400$	$t_1 = 30$
Light cutting		$F_2 = 690$		$N_2 = 75$	$N_2 = 60$	$t_2 = 55$
Heavy cutting		$F_3 = 1140$		$N_3 = 15$	$N_3 = 12$	$t_3 = 15$

Calculation of mean load and mean rotation

$$\text{Mean load } F_m = \left( \frac{F_1^3 \cdot n_1 \cdot t_1 + F_2^3 \cdot n_2 \cdot t_2 + \dots + F_n^3 \cdot n_n \cdot t_n}{n_1 \cdot t_1 + n_2 \cdot t_2 + \dots + n_n \cdot t_n} \right)^{\frac{l}{3}}$$

$$\text{Mean rotation } N_m = \frac{n_1 \cdot t_1 + n_2 \cdot t_2 + \dots + n_n \cdot t_n}{t_1 + t_2 + \dots + t_n}$$

Lead l (mm)	8	10
Mean load $F_m$ (kgf)	330	330
Mean rotation $N_m$ (rpm)	569	455

Calculation of basic dynamic rate load

$$L = \left( \frac{Ca}{Fa \times f_w} \right)^3 \times 10^6 \quad L_t = \frac{L}{60N_m}$$

$$\Rightarrow Ca = (60N_m \times L_t)^{1/3} \times F_m \times f_w \times 10^{-2}$$

As per design Conditions:

$$L_t = 25000 \text{ (hours)}$$

$$f_w = 1.2$$

When  $l=8\text{mm}$  .....  $Ca \geq 3756 \text{ (kgf)}$

If life > 25000 (hours) is needed,  
Ca must be > 3756 (kgf)

When  $l=10\text{mm}$  .....  $Ca \geq 3487 \text{ (kgf)}$

If life > 25000 (hours) is needed,  
Ca must be > 3487 (kgf)

## (3) Selecting the type of nut

In case stiffness is a major concern, lost motion becomes less important, following specifications are to be selected:

- External circulation Ballscrew
- Type: FDWC
- Number of circuit: B×2 or B×3

The value of Ca can be found as per this catalog:

Screw nominal O.D.(mm)	lead 8 (mm)		lead 10 (mm)	
	B×2	B×3	B×2	B×3
32	3210	-	4660	-
36	3265	-	4930	-
40	3410	-	5220	-
45	3650	5175	5480	7760
50	3900	5520	5790	8200

#### (4) Selecting screw shaft diameter

Ballscrew shaft diameter can be decided by critical rotation speed of high speed feed.

Assume both of the supporting ends are fixed.

So the permissible rotational speed :

$$n = \alpha \times \frac{60\lambda^2}{2\pi L^2} \sqrt{\frac{E Ig}{rA}} = f \frac{dr}{L^2} \times 10^7$$

$$\Rightarrow dr \geq \frac{n \times L^2}{f} \times 10^7$$

$L$  = Max. stroke + Nut length/2 + Unthread area length

$$= 1000 + 100 + 200 = 1300 \text{ (mm)}$$

Screw shaft supported method is fixed-fixed

$$\Rightarrow f = 21.9$$

$$\text{when } l = 8 \text{ (mm)} \dots dr \geq 13.5 \text{ (mm)}$$

If the highest rotational speed reaches 1750 rpm,

screw shaft diameter at thread root area must be bigger than 14 mm.

◎ So screw shaft diameter shall be ranged in between 20 and 50 mm.

$$\text{When } l = 10 \text{ (mm)} \dots dr \geq 10.8 \text{ (mm)}$$

If the highest rotational speed reaches 1400 rpm,

screw shaft diameter at thread root area must be bigger than 11 mm.

◎ So screw shaft diameter shall be ranged in between 16 and 50 mm.

#### (5) Considering rigidity

By initial conditions:

Lost motion : 0.02 mm (no load)

Assume total displacement of components (including screw shaft, ballnut and support bearing) of feed system is 0.016 mm. Thus the unilateral elastic displacement of feed system is

$$\Delta L \leq 8 \text{ (\mu m)}$$

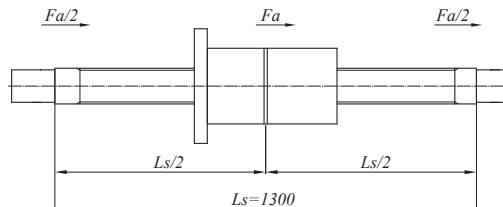
#### a. Axial rigidity of the screw shaft: $K_s$

Elastic displacement of the screw shaft:  $\Delta L_s$

$$K_s = \frac{A \times E \times L}{x(L-x)} \times 10^{-3}$$

The smallest elastic displacement is in the middle of screw shaft.

From following diagram Using  $x=L/2$



$$\Rightarrow K_s = \frac{\pi \times dr^2 \times E}{L_s} \times 10^3$$

$$\Delta L_s = \frac{Fa}{K_s} = \frac{Fa \times L_s}{\pi \times dr^2 \times E} \times 10^3$$

Here  $Fa$  is sliding resistance of 190 (kgf)

The results are in the table 10.1.

#### b. Axial rigidity of the nut: $K_n$

Elastic displacement of the nut:  $\Delta L_n$

Setting the preload to be 1/3 of maximum axial load.

$$Fao = F_{max}/3 = 1140/3 = 380 \text{ (kgf)}$$

$$K_n = 0.8 \times K \left( \frac{Fao}{\varepsilon \times Ca} \right)^{1/3}$$

$$\varepsilon = 0.1, \text{ then}$$

$$\Delta L_n = \frac{Fa}{K_n}$$

The results are in the table 10.1.

Table10.1

Nut model no.	$dr$	$Ca$	$K$	Screw		Nut		$\Delta L$
				$K_s$	$\Delta L_s$	$K_n$	$\Delta L_n$	
32-10B2-FDWC	27.05	4660	125	37.1	5.1	93.0	2.0	7.1
36-10B2-FDWC	31.05	4930	138	48.9	3.9	101.2	1.9	5.8
40-10B2-FDWC	35.05	5220	151	62.3	3.0	108.7	1.7	4.7
45-10B2-FDWC	38.05	5480	167	73.5	2.6	118.3	1.6	4.2
50-10B2-FDWC	42.05	5790	182	89.7	2.1	126.5	1.5	3.6

◎ With the condition of  $\Delta L \leq 8 (\mu m)$

Make following selection by ignoring the bearing rigidity, economical and safety consideration:

Type of Ballscrew : 40-10B2-FDWC

Screw shaft diameter : 40 (mm)

Lead : 10 (mm)

#### (6) Length of Ballscrew

$L = \text{Max. travel} + \text{Nut length} + \text{Unthreaded area length}$

$$= 1000 + 180 + 100 \quad (\text{including journal ends length})$$

$$= 1280$$

$$\approx 1300 \text{ (mm)}$$

#### (7) Preliminary check

##### a. Fatigue life

$$\begin{aligned} L_t &= \left( \frac{Ca}{F_m \times f_w} \right)^3 \times 10^6 \times \frac{1}{60n} \\ &= \left( \frac{4700}{330 \times 1.2} \right)^3 \times 10^6 \times \frac{1}{60 \times 455} \\ &\approx 61000 \text{ (hours)} > 25000 \text{ (hours)} \end{aligned}$$

##### b. Permissible rotational speed

$$\begin{aligned} n &= f \times \frac{dr}{L^2} \times 10^7 \\ &= 4540 \text{ (rpm)} \end{aligned}$$

Critical speed of screw shaft is 4540(rpm). It is much bigger than the maximum rotational speed of design. So the Ballscrew selected is safe.

#### 2 ◀ Selecting lead accuracy

Positioning accuracy required:  $\pm 0.030/1000 \text{ mm}$  (Max. travel) Refer to table 2.2, accumulated reference lead deviation ( $\pm E$ ) and total relative variation ( $e$ )

Accuracy grades: C4

$$E = \pm 0.025/1250 \text{ (mm)}$$

$$e = 0.018 \text{ (mm)}$$

#### 3 ◀ Considering thermal displacement

According to the load capability of support bearings, make the specified travel (T) compensation to be  $3^\circ\text{C}$

##### 1. Thermal displacement: $\Delta L_\theta$

$$\begin{aligned} \Delta L_\theta &= \rho \cdot \theta \cdot L \\ &= 12.0 \times 10^{-6} \times 3 \times 1300 \\ &= 0.047 \text{ (mm)} \end{aligned}$$

##### 2. Pretension force: $F_\theta$

$$\begin{aligned} F_\theta &= \Delta L_\theta \times K_S = \frac{\Delta L_\theta \cdot E \cdot \pi dr^2}{4L} \\ &= \frac{0.047 \times 2.1 \times 10^4 \times \pi \times 27.05^2}{4 \times 1300} \\ &= 436 \text{ (kgf)} \end{aligned}$$

Specified Travel (T): -0.047/1300

Pretension force: 436 (kgf)

Stretching: -0.047 (mm)

#### 4 Selecting driving motor

<Required specifications>

1. The highest rotation speeds is 1500 (rpm)
2. Time required to reach highest rotational speed is within 0.15 sec.

(1) Inertial

a. Screw shaft:

$$GD_s^2 = \frac{\pi\rho}{8} \times D^4 \times L = \frac{\pi \times 7.8 \times 10^{-3}}{8} \times 4^4 \times 130 = 101.9 \text{ (kgf}\cdot\text{cm}^2)$$

b. Moving parts:

$$GD_w^2 = W \left( \frac{l}{\pi} \right)^2 = (1100+800) \times \left( \frac{1.0}{\pi} \right)^2 = 192.5 \text{ (kgf}\cdot\text{cm}^2)$$

c. Coupling:

$$GD_j^2 = 40 \text{ (kgf}\cdot\text{cm}^2)$$

d. Total of inertial:

$$GD_L^2 = GD_s^2 + GD_w^2 + GD_j^2 = 334.4 \text{ (kgf}\cdot\text{cm}^2)$$

(2) Driving torque

In this case, the time sharing of machine working at acceleration condition is limited. Assuming the machine works at constant speed, the torque caused by angular acceleration is then neglected.

a. Preloading torque

$$T_p = k \times \frac{Fao \times l}{2\pi} = 0.18 \times \frac{380 \times 1.0}{2\pi} = 10.8 \text{ (kgf}\cdot\text{cm)}$$

$$k = 0.18$$

$$Fao = F_{max}/3$$

b. Friction torque

Rapid feed:

$$T_a = \frac{F_a \times l}{2\pi \times \eta} = \frac{190 \times 1.0}{2\pi \times 0.9} = 33.6 \text{ (kgf}\cdot\text{cm)}$$

Light cutting:

$$T_b = \frac{690 \times 1.0}{2\pi \times 0.9} = 122.1 \text{ (kgf}\cdot\text{cm)}$$

Heavy cutting:

$$T_c = \frac{1140 \times 1.0}{2\pi \times 0.9} = 201.7 \text{ (kgf}\cdot\text{cm)}$$

The maximum required driving torque is preloading torque plus friction torque of heavy cutting.

$$\begin{aligned} T_L &= T_p + T_c \\ &= 212.5 \text{ (kgf}\cdot\text{cm)} \end{aligned}$$

(3) Selecting driving motor

<Selecting conditions>

a. The highest rotation speed:  $N_{max} \geq 1500 \text{ (rpm)}$

b. Rated torque:  $T_M > T_L$

c. Rotor inertia:  $J_M \leq J_L / 3$

The specifications required for driving motor are then decided as per above conditions.

◎ Motor specifications:

Output	$W_M = 3.6 \text{ (kW)}$
Highest rotation speeds	$N_{max} = 1500 \text{ (rpm)}$
Rated torque	$T_M = 22.6 \text{ (N.m)}$
Rotor inertia	$GD_M^2 = 750 \text{ (kgf}\cdot\text{cm}^2)$

(4) Check required time period for reaching highest rotation speed

$$t_a = \frac{J}{T'_M T_L} \times \frac{2\pi N}{60} \times f$$

Here

$$J : \text{Total inertia } J = \frac{GD^2}{4g}$$

$$T'_M = 2 \times T_M$$

$T_L$  : Rotation Torque (rapid)

$f$  : Safe factor (choose 1.4 for this case)

$$t_a = \frac{(334.3+750)}{4 \times 980 \times (2 \times 230 - (18.1+33.6))} \times \frac{2\pi \times 1400}{60} \times 1.4 = 0.139 \text{ (sec)} < 0.15 \text{ (sec)}$$

This above motor specifications match design needs.

## 5 Calculating the stress of the Ballscrew

$$\sigma = \frac{F}{A} = \frac{F_{max}}{\pi dr^2/4} = \frac{1140 \times 9.8 \times 4}{\pi \times 35.05^2} = 11.56 \text{ N/mm}^2 = 1.16 \times 10^7 \text{ N/m}^2$$

( $dr$  is screw shaft thread root diameter)

$$dr = 40 + 1.4 - 6.35 = 35.05 \text{ (mm)}$$

$$\tau = \frac{T \times r}{J} = \frac{21540 \times 20}{148167} = 2.91 \text{ N/mm}^2 = 2.91 \times 10^6 \text{ N/m}^2$$

$$T_{max} = T_L = 219.8 \text{ (kgf cm)} = 21540 \text{ (N-mm)}$$

$$J = \frac{\pi dr^4}{32} = \frac{\pi (35.05^4)}{32} = 148167 \text{ (mm}^4\text{)}$$

$$\begin{aligned} \sigma_{max} &= \sqrt{\sigma^2 + \tau^2} \\ &= 11.9 \times 10^6 \text{ N/m}^2 \end{aligned}$$

50CrMo4 steel tension strength is  $1.1 \times 10^8 \text{ N/m}^2 > \sigma_{max}$

Yield strength is  $0.9 \times 10^8 \text{ N/m}^2 > \sigma_{max}$

◎So the Ballscrew selected is safe.

## 6 Calculating the buckling load of the screw shaft

$$P = \alpha \frac{\pi^2 n EI}{L^2} = m \frac{dr^4}{L^2} \times 10^3 = 20.3 \times \frac{35.05^4}{1100^2} \times 10^3 = 25300 \text{ (kgf)} > F_{max} \text{ (1140 kgf)}$$

◎So the Ballscrew selected is safe.

## 10.2 High Speed Porterage Apparatus (Horizontal application)

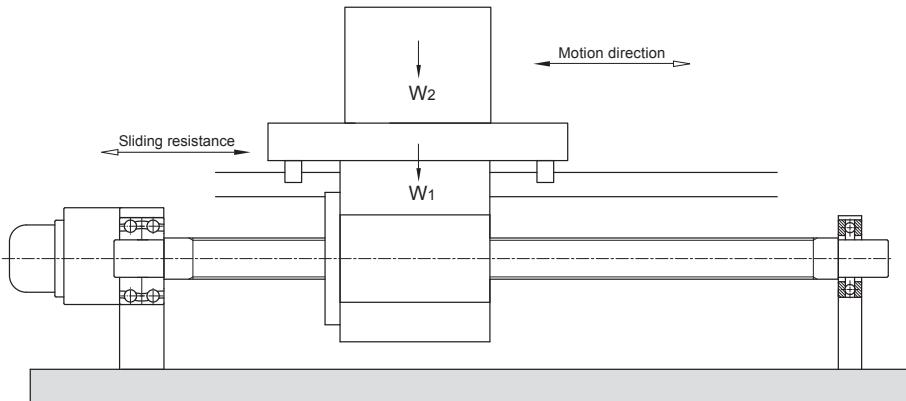


Fig.10.2 High speed porterage apparatus

### 1 ▶ Design Conditions:

Table weight:	$W_1 = 50 \text{ kgf}$
Work piece weight:	$W_2 = 25 \text{ kgf}$
Max. travel:	$S_{max} = 1000 \text{ mm}$
Rapid feed speed:	$V_{max} = 50 \text{ m/min}$
Life:	$L_i = 25000 \text{ hours}$
Guiding surface friction coefficient:	$\mu = 0.01$
Driving motor:	$N_{max} = 3000 \text{ rpm}$
Positioning Accuracy:	$\pm 0.10 \text{ at max. travel}$
Repeatability Accuracy:	$\pm 0.01 \text{ mm}$

### 2 ▶ Motion Conditions:

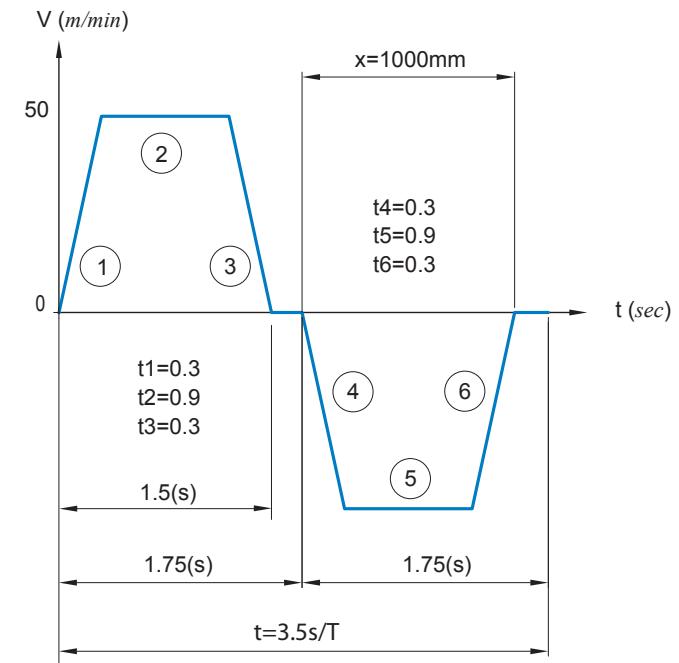


Fig.10.3 Porterage apparatus v-t diagram

### 3 \ Items to be decided

1. Screw nominal O.D., Lead
2. Accuracy grade
3. Type of nut
4. Driving motor

#### 1 \ Selecting Screw nominal O.D., Lead

##### (1) Lead ( $l$ )

The highest rotation speed of motor

$$l \geq \frac{V_{max}}{N_{max}} = \frac{50000}{3000} \doteq 17 \text{ (mm)}$$

◎Lead have to be 18 mm or more.

(As per PMI catalog : select 20 mm for further analysis)

If lead is 20 mm, the highest rapid feed speed 50 m/min shall be reached as long as the motor rotates at 2500 rpm.

##### (2) Initial selection of screw shaft length

$$\begin{aligned} L &= \text{Max. travel} + \text{Nut length} + \text{Unthreaded area length} \\ &= 1000 + 100 + 100 = 1200 \text{ (mm)} \end{aligned}$$

##### (3) Selecting screw shaft diameter

Ballscrew shaft diameter can be decided by critical rotation speed of high speed feed.

Assume the supporting ends are fixed-supported.

So the permissible rotational speed :

$$\begin{aligned} n &= \alpha \times \frac{60\lambda^2}{2\pi L^2} \sqrt{\frac{EIg}{\gamma A}} = f \frac{dr}{L^2} \times 10^7 \\ \Rightarrow dr &\geq \frac{n \times L^2}{f} \times 10^7 \end{aligned}$$

$$\begin{aligned} L &= \text{Max. travel} + \text{Nut length}/2 + \text{Unthread area length} \\ &= 1000 + 50 + 100 = 1150 \text{ (mm)} \end{aligned}$$

Screw shaft support method is fixed-supported

$$f = 15.1$$

$$dr \geq 21.9 \text{ (mm)}$$

If the high rotational speed is 2500 rpm,

Diameter at thread root area must be bigger than 22 mm.

◎So Screw-shaft diameter shall be ranged in between 25 and 36 mm

#### (4) Considering service life

First to analyze Fig.10.3 (V-t diagram)

The speed line is a straight one, hence it is a constant acceleration, periodically reciprocating motion.

Maximum velocity :  $V_{max} = 50 \text{ (m/min)} = 0.83 \text{ (m/s)}$

Acceleration time :  $t_f = 0.3 \text{ (s)}$

Deceleration time :  $t_d = 0.3 \text{ (s)}$

##### a. Running distance during acceleration

$$\begin{aligned} x_1 &= \left( \frac{V_0 + V}{2} \right) \times t = \left( \frac{0+0.83}{2} \right) \times 0.3 \\ &= 0.125 \text{ (m)} = 125 \text{ (mm)} \end{aligned}$$

##### b. Running distance during constant speed

$$\begin{aligned} x_2 &= V \cdot t = 0.83 \times 0.9 \\ &= 0.75 \text{ (m)} = 750 \text{ (mm)} \end{aligned}$$

##### c. Running distance from highest speed to stop

$$x_3 = \left( \frac{V_0 + V}{2} \right) \times t = \left( \frac{0.83+0}{2} \right) \times 0.3 = 0.125 \text{ (m)} = 125 \text{ (mm)}$$

##### d. The line segment

$$a_l = \frac{V_{max}}{t_f} = \frac{0.833}{0.3} = 2.8 \text{ (m/s}^2\text{)}$$

$$F_l = \mu (W_l + W_2) \times g + (W_l + W_2) \times a_l = 0.01 \times (50+25) \times 9.8 + (50+25) \times 2.8 = 217 \text{ (N)}$$

$$N_l = n_{max} / 2 = 2500 / 2 = 1250 \text{ (rpm)}$$

e. The line segment

$$F_2 = f = \mu(W_1 + W_2) \times g = 0.01 \times (50 + 25) \times 9.8 = 7.35 \text{ (N)}$$

$N_2 = 2500 \text{ (rpm)}$

f. The line segment

$$F_3 = \mu(W_1 + W_2) \times g + (W_1 + W_2) \times a_3 = 0.01 \times (50 + 25) \times 9.8 + (50 + 25) \times (-2.8) = -203 \text{ (N)}$$

$$N_3 = n_{\max}/2 = 2500/2 = 1250 \text{ (rpm)}$$

Whence the relationship between the applied axial load, running distance, time and mean rotation can be as follows:

Motion	Axial load	Running distance	Time	Mean rotation
Acceleration forward	217	125	0.3	1250
Constant speed forward	7.35	750	0.9	2500
Deceleration forward	-203	125	0.3	1250
Acceleration returning	-217	125	0.3	1250
Constant speed returning	-7.35	750	0.9	2500
Deceleration returning	203	125	0.3	1250

g. Calculation of mean load and mean rotation:

$$F_m = \left( \frac{F_1^3 \cdot n_1 \cdot t_1 + F_2^3 \cdot n_2 \cdot t_2 + \dots + F_n^3 \cdot n_n \cdot t_n}{n_1 \cdot t_1 + n_2 \cdot t_2 + \dots + n_n \cdot t_n} \right)^{\frac{1}{3}} = \left( \frac{217^3 \times 1250 \times 0.6 + 7.35^3 \times 2500 \times 1.8 + 203^3 \times 1250 \times 0.6}{1250 \times 0.6 + 2500 \times 1.8 + 1250 \times 0.6} \right)^{\frac{1}{3}}$$

$$= 132.4 \text{ (N)}$$

$$N_m = \frac{n_1 \cdot t_1 + n_2 \cdot t_2 + \dots + n_n \cdot t_n}{t} = \frac{1250 \times 0.6 + 2500 \times 1.8 + 1250 \times 0.6}{3.5} = 1714 \text{ (rpm)}$$

h. Calculation of life

$$L_t = \left( \frac{Ca}{F_m \times f_w} \right)^3 \times \frac{1}{60N_m} \times 10^6 = \left( \frac{1170 \times 9.8}{132.4 \times 2.5} \right)^3 \times \frac{1}{60 \times 1714} \times 10^6$$

$$= 404000 \geq 25000 \text{ (hours)}$$

◎ Above conforms design requirements.

2 \\ Selecting accuracy grade

Positioning accuracy of  $\pm 0.1/1000 \text{ mm}$  (Max. travel) From P.A24

Accuracy grade: C5

$$E = \pm 0.040/1000$$

$$e = 0.027$$

3 \\ Selecting Ballscrew type

Considering operation conditions, effective turns of A1 is selected.

Selecting following type:

R25-20A1-FSWE-1000-1160-0.018

Screw-shaft support method is fixed-supported

4 \\ Selecting driving motor

<Required specifications>

1.The highest rotation speed of 3000 (rpm)

2.Time required to reach highest rotational speed is within 0.30 sec

(1) Inertial

a. Screw shaft:

$$J_{sh} = \frac{\pi \rho}{32g} \times D^4 \times L = \frac{\pi \times 7.8 \times 10^{-3}}{32 \times 980} \times 2.5^4 \times 120 = 0.0037 \text{ (kgf.cm.sec}^2\text{)}$$

b. Moving parts:

$$J_w = \frac{W}{g} \left( \frac{l}{2\pi} \right)^2 = \frac{25+50}{980} \left( \frac{2}{2\pi} \right)^2 = 0.0078 \text{ (kgf.cm.sec}^2\text{)}$$

c. Coupling:

$$J_c = 0.0005 \text{ (kgf.cm.sec}^2\text{)}$$

d. Total of Inertial:

$$J_L = J_{sh} + J_w + J_c = 0.012 \text{ (kgf.cm.sec}^2\text{)}$$

## (2) Driving torque

a. During constant speed:

$$T_I = \frac{F_I \times l}{2 \times \eta} = \frac{7.35 \times 2}{2 \times 0.9} = 2.6 \approx 3.00 \text{ (N.cm)}$$

$\eta = 0.9$

b. During acceleration

$$T_2 = T_I + J \dot{\omega} = T_I + (J_L + J_M) \times \frac{2\pi n}{60t_I} = 3 + (0.009 + 0.01) \times 9.8 \times \left( \frac{2\pi \times 2500}{60 \times 0.3} \right) = 166 \text{ (N.cm)}$$

preselect motor, and give the specifications for the rate inertia

$$J_M = 0.01 \text{ (kgf.cm.sec}^2)$$

c. During deceleration

$$T_3 = T_I - J \dot{\omega} = T_I - (J_L + J_M) \times \frac{2\pi n}{60t_3} = 3 - (0.009 + 0.01) \times 9.8 \times \left( \frac{2\pi \times 2500}{60 \times 0.3} \right) = -160 \text{ (N.cm)}$$

## (3) Selecting driving motor

<Selecting conditions>

1. The highest rotation speed:  $N_{max} \geq 3000 \text{ (rpm)}$

2. Rated torque -----  $T_M > T_L$

3. Rotor inertia -----  $J_M \geq J_L / 3$

The specifications required for driving motor are then decided as per above conditions.

◎Motor specifications:

Output	$W_M = 400 \text{ (kW)}$
Highest rotation speeds	$N_{max} = 3000 \text{ (rpm)}$
Rated torque	$T_M = 1.27 \text{ (N.m)}$
Rotor inertia	$J_M = 0.01 \text{ (kgf.cm.sec}^2)$

## (4) Effective torque:

$$T_{rms} = \sqrt{\frac{T_2^2 \times t_a + T_I^2 \times t_b + T_3^2 \times t_c}{t}} = \sqrt{\frac{166^2 \times 0.6 + 3^2 \times 1.8 + 160^2 \times 0.6}{3.5}} = 95 \text{ (N.cm)} < 127 \text{ (N.cm)}$$

◎ It conforms to design requirements.

## (5) Time required to reach highest rotational speed.

$$t_a = \frac{J}{T_M' - T_L} \times \frac{2\pi n}{60} \times f$$

Here:

$J$ : Total inertia

$$T_M' = 2 \times T_M$$

$T_L$ : Rotation Torque (rapid)

$f$ : Safe factor (choose 1.4 for this case)

$$t_a = \frac{0.009 + 0.01}{2 \times 127 \times 3} \times \frac{2\pi \times 2500}{60} \times 1.4 = 0.27 \text{ (s)} < 0.3 \text{ (s)}$$

◎ It conforms to design requirements.

## 5 ◀ Calculating the stress of the Ballscrew

$$\sigma = \frac{F}{A} = \frac{F_{max}}{\pi dr^2/4} = \frac{217 \times 4}{\pi \times 22.425^2} = 0.61 \text{ N/mm}^2 = 6.1 \times 10^5 \text{ N/m}^2$$

$$dr = 25 + 1 - 4.762 = 21.238 \text{ (mm)}$$

( $dr$  is screw shaft thread minor diameter)

$$\tau = \frac{T \times r}{J} = \frac{1660 \times 12.5}{24827} = 0.84 \text{ N/mm}^2 = 8.4 \times 10^5 \text{ N/m}^2$$

$$T_{max} = T_L = 166 \text{ (N.cm)} = 1660 \text{ (N.mm)}$$

$$J = \frac{\pi dr^4}{32} = \frac{\pi (22.425^4)}{32} = 24827 \text{ (mm}^4)$$

$$\sigma_{max} = \sqrt{\sigma^2 + \tau^2} = 0.10 \times 10^8 \text{ N/m}^2$$

50CrMo4 steel tension strength is  $1.5 \times 10^8 \text{ N/m}^2$

Yield strength is  $0.9 \times 10^8 \text{ N/m}^2$

◎ So the Ballscrew selected is safe.

## 6 ◀ Calculating the buckling load of the screw shaft

$$\begin{aligned} P &= \alpha \frac{\pi^2 n EI}{L^2} = m \frac{dr^4}{L^2} \times 10^3 \\ &= 10.2 \times \frac{22.425^4}{1160^2} \times 10^3 \\ &= 1917 \text{ (kgf)} > F_{max} (22.14 \text{ kgf}) \end{aligned}$$

◎ So the Ballscrew selected is safe.

### 10.3 Vertical Portage Apparatus

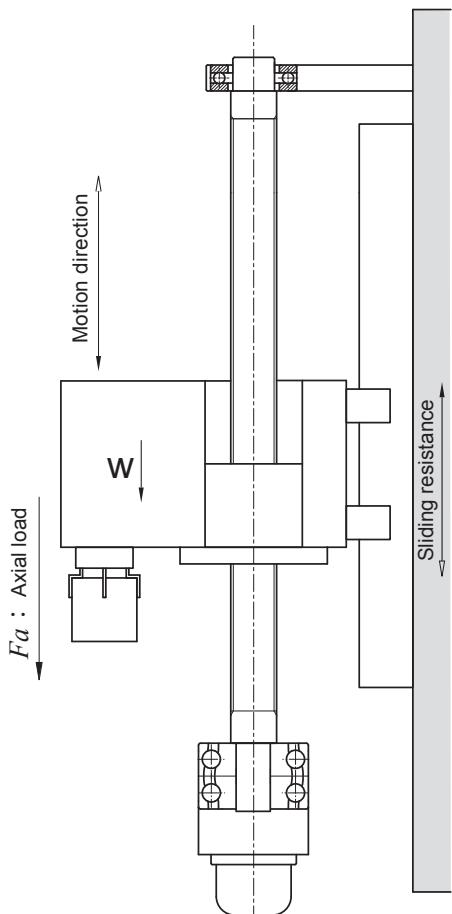


Fig.10.4 Vertical portage apparatus

#### 1 ▶ Design Conditions:

Table weight:	$W_1 = 300 \text{ kgf}$
Work piece weight:	$W_2 = 50 \text{ kgf}$
Max. travel:	$S_{max} = 1500 \text{ mm}$
Rapid feed speed:	$V_{max} = 15 \times 10^3 \text{ mm/min}$
Life:	$L_t = 20000 \text{ hours}$
Guiding surface friction coefficient:	$\mu = 0.01$
Driving motor:	$N_{max} = 1500 \text{ rpm}$
Positioning accuracy:	$\pm 0.8/1500 \text{ mm}$
Repeatability accuracy:	$\pm 0.3 \text{ mm}$

#### 2 ▶ Motion Conditions:

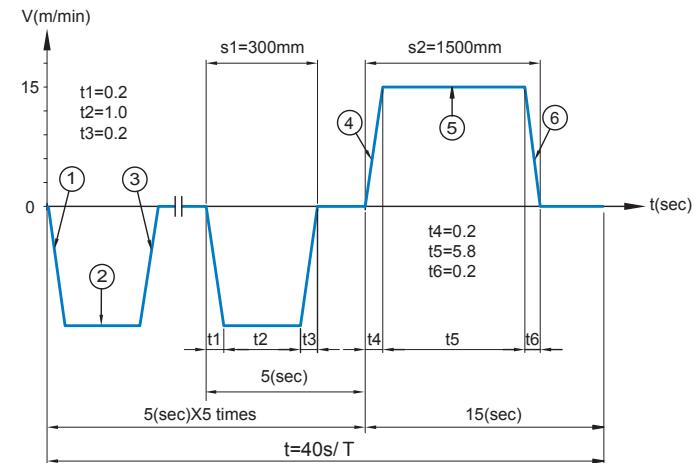


Fig.10.5 Portage apparatus v-t diagram

3 Items to be decided:

1. Accuracy grade
2. Screw nominal O.D., Lead
3. Driving motor

#### 1 Selecting accuracy grades

As per design condition: positioning accuracy required:  $0.8/1500 \text{ mm}$

$$\frac{\pm 0.8}{1500} = \frac{\pm 0.16}{300}$$

Refer to table 2.2, accumulated reference lead deviation ( $\pm E$ ) and total relative variation ( $e$ )

Accuracy grades C7

$E = \pm 0.05/300 \text{ mm}$

So the portage apparatus can use Rolled Ballscrew.

#### 2 Selecting screw nominal O.D., Lead

(1) Lead ( $l$ ) :

The highest rotation speed of motor

$$l \geq \frac{V_{max}}{N_{max}} = \frac{15000}{1500} = 10 \text{ (mm)}$$

So Lead have to be 10 mm or more.

(As per PMI catalog : select 10 mm for further analysis)

(2) Permissible axial load

Setting up is positive.

a. Force during acceleration (downward)

$$a_l = \frac{V_{max}}{t_l} = \frac{15000}{60 \times 0.2} = 1250 \text{ (mm/s}^2\text{)} = 1.25 \text{ (m/s}^2\text{)}$$

$$f = \mu (W_1 + W_2) \times g = 0.01(300+500) \times 9.8 = 35 \text{ (N) (Friction)}$$

$$F = ma \rightarrow F_l = (W_1 + W_2) \times g - f - (W_1 + W_2) \times a_l = 2958 \text{ (N)}$$

b. Force during constant speed (downward)

$$F = 0 \rightarrow F_2 = (W_1 + W_2) \times g - f = 3395 \text{ (N)}$$

c. Force during deceleration (downward)

$$F = ma \rightarrow F_3 = (W_1 + W_2) \times g + f + (W_1 + W_2) \times a_3 = 3833 \text{ (N)}$$

d. Force during acceleration (upward)

$$F = ma \rightarrow F_4 = (W_1 + W_2) \times g + f + (W_1 + W_2) \times a_4 = 3903 \text{ (N)}$$

e. Force during constant speed (upward)

$$F = 0 \rightarrow F_5 = (W_1 + W_2) \times g + f = 3465 \text{ (N)}$$

f. Force during deceleration (upward)

$$F = ma \rightarrow F_6 = (W_1 + W_2) \times g + f - (W_1 + W_2) \times a_6 = 3028 \text{ (N)}$$

So

$$Fa_{max} = F_4 = 3903 \text{ (N)}$$

(3) Buckling load:

$$P = \alpha \frac{\pi^2 n EI}{L^2} = m \frac{dr^4}{L^2} \times 10^3$$

$$dr = \left( \frac{P \times L^2}{m} \times 10^{-3} \right)^{1/4} = \left( \frac{3903 \times 1800^2}{9.8 \times 10.2} \times 10^{-3} \right)^{1/4} = 19 \text{ (mm)}$$

Screw shaft diameter at thread root area must be bigger than 19 mm.

So screw shaft diameter shall be ranged in between 25 and 50 mm.

(4) The length of screw shaft

$$\begin{aligned} L &= \text{Max. travel} + \text{Nut length} + \text{Unthreaded area length} \\ &= 1500 + 100 + 200 = 1800 \text{ (mm)} \end{aligned}$$

Slenderness ratio: 60 or less

$$D \geq \frac{L}{60} = \frac{1800}{60} = 30 \text{ (mm)}$$

So screw shaft diameter shall be ranged in between 32 and 50 mm.

## (5) Permissible rotational speed

Assume the supporting ends are fixed-supported

So the permissible rotational speed:

$$n = \alpha \times \frac{60\lambda^2}{2\pi L} \sqrt{\frac{Eig}{\gamma A}} = f \frac{dr}{L^2} \times 10^7$$

$$\Rightarrow dr \geq \frac{n \times L^2}{f} \times 10^{-7} \quad (f=15.1, L=1800)$$

$$\geq 30$$

If the highest rotational speed reaches 1500 rpm, screw shaft thread diameter at thread root area must be bigger than 30 mm.

◎ So screw shaft diameter shall be ranged in between 36 and 50 mm.

## (6) Calculating of basic dynamic rate load:

Motion	Axial load (N)	Mean rotation (rpm)	Time (sec)
Acceleration (down)	$F_1=2958$	$n_1=750$	$t_1=1.0$
Constant speed (down)	$F_2=3395$	$n_2=1500$	$t_2=5.0$
Deceleration (down)	$F_3=3833$	$n_3=750$	$t_3=1.0$
Acceleration (up)	$F_4=3903$	$n_4=750$	$t_4=0.2$
Constant speed (up)	$F_5=3465$	$n_5=1500$	$t_5=5.8$
Deceleration (up)	$F_6=3028$	$n_6=750$	$t_6=0.2$

Mean load

$$F_m = \left( \frac{F_1^3 \cdot n_1 \cdot t_1 + F_2^3 \cdot n_2 \cdot t_2 + \dots + F_n^3 \cdot n_n \cdot t_n}{n_1 \cdot t_1 + n_2 \cdot t_2 + \dots + n_n \cdot t_n} \right)^{\frac{1}{3}} = 3436 \text{ (N)}$$

Mean rotation

$$N_m = \frac{n_1 \cdot t_1 + n_2 \cdot t_2 + \dots + n_n \cdot t_n}{t} = 450 \text{ (rpm)}$$

As per design condition:

Life required is 20000 hours, Let  $f_w=1.2$

$$L_t = \left( \frac{Ca}{F_m \times f_w} \right)^3 \times \frac{1}{60N_m} \times 10^6$$

$$Ca = (60N_m \times L_t)^{1/3} \times F_m \times f_w \times 10^2 = 33576 \text{ (N)} = 3426 \text{ (kgf)}$$

◎ If the life required is > 20000 (hours),  
Ca has to be > 3426 (kgf)

## (7) Calculating basic static rate load:

$$Co = F_{max} \times f_s \quad f_s = 2.0$$

$$= 7806 \text{ (N)}$$

$$= 800 \text{ (kgf)}$$

Co has to be > 800 (kgf)

◎ Selection is made as follows:

Type of the Ballscrew: 40-10B2-FSWW

Screw shaft diameter: 40 (mm)

Lead:10 (mm)

Basic dynamic rate load: 3520 (kgf)

## 3 Selecting driving motor

<Required specifications>

1 The highest rotation speeds is 1500 mm/min

2 Time required to reach highest rotational speed is within 0.2 sec.

## (1) Inertial

a. Screw shaft:

$$GD_S^2 = \frac{\pi \rho}{8} \times D^4 \times L = \frac{\pi \times 7.8 \times 10^{-3}}{8} \times 4^4 \times 180 = 141.1 \text{ (kgf} \cdot \text{cm}^2\text{)}$$

b. Moving parts:

$$GD_w^2 = W \left( \frac{l}{\pi} \right)^2 = (300+50) \times \left( \frac{1.0}{\pi} \right)^2 = 192.5 \text{ (kgf} \cdot \text{cm}^2\text{)}$$

c. Coupling:

$$GD_J^2 = 1.0 \text{ (kgf} \cdot \text{cm}^2\text{)}$$

d. Total of Inertial:

$$GD_L^2 = GD_S^2 + GD_w^2 + GD_J^2 = 178 \text{ (kgf} \cdot \text{cm}^2\text{)}$$

(2) Driving torque:

### 1.Friction torque

#### a.Acceleration (downward):

$$T_1 = \frac{Fa \times l}{2\pi \times \eta} = \frac{2950 \times 1.0}{2\pi \times 0.9} = 520 \text{ (N}\cdot\text{cm)}$$

#### b.Constant speed (downward):

$$T_2 = \frac{Fa \times l}{2\pi \times \eta} = \frac{3395 \times 1.0}{2\pi \times 0.9} = 600 \text{ (N}\cdot\text{cm)}$$

#### c.Deceleration (downward):

$$T_3 = \frac{Fa \times l}{2\pi \times \eta} = \frac{3833 \times 1.0}{2\pi \times 0.9} = 680 \text{ (N}\cdot\text{cm)}$$

#### d.Acceleration (upward):

$$T_4 = 690 \text{ (N}\cdot\text{cm)}$$

#### e.Constant speed (upward):

$$T_5 = 610 \text{ (N}\cdot\text{cm)}$$

#### f.Deceleration (upward):

$$T_6 = 540 \text{ (N}\cdot\text{cm)}$$

### 2.Preloading torque

$$T_p = k \times \frac{Fao \times l}{2\pi} \quad \therefore Fao = 0 \quad \therefore T_p = 0$$

### 3.Torque required for acceleration:

$$T_7 = J \cdot w$$

$$= (J_L + J_M) \times \frac{2\pi n}{60l_1} = \frac{(178+120)}{4 \times 980} \times \left( \frac{2\pi \times 1500}{60 \times 0.2} \right) = 59.7 \text{ (kgf}\cdot\text{cm)} = 585 \text{ (N}\cdot\text{cm)}$$

$$GD_M = 120 \text{ (kgf}\cdot\text{cm}^2)$$

### 4.Total torque:

#### a.Acceleration (downward):

$$T_{k1} = T_1 + T_7 = 520 + 585 = 1105 \text{ (N}\cdot\text{cm)}$$

#### b.Constant speed (downward):

$$T_{t1} = T_2 = 600 \text{ (N}\cdot\text{cm)}$$

#### c.Deceleration (downward):

$$T_{g1} = T_3 + T_7 = 680 + 585 = 1265 \text{ (N}\cdot\text{cm)}$$

#### d.Acceleration (upward):

$$T_{k2} = T_4 + T_7 = 690 + 585 = 1275 \text{ (N}\cdot\text{cm)}$$

#### e.Constant speed (upward):

$$T_{t2} = T_5 = 610 \text{ (N}\cdot\text{cm)}$$

#### f.Deceleration (upward):

$$T_{g2} = T_6 + T_7 = 540 + 585 = 1125 \text{ (N}\cdot\text{cm)}$$

The maximum torque takes place at the time of acceleration.

$$T_{max} = T_{k2} = 1275 \text{ (N}\cdot\text{cm)}$$

## (3) Selecting driving motor

&lt;Selecting conditions&gt;

a.The highest rotation speeds:  $N_{max} \geq 1500 \text{ (rpm)}$ b.Rated torque:  $T_M = T_{rms}$ c.Rotor inertia:  $J_M \geq J_L/3$ 

The specifications required for driving motor are then decided as per above conditions

## ◎Motor specifications:

Output  $W_M = 2000 \text{ (W)}$ Highest rotation speeds  $N_{max} = 1500 \text{ (rpm)}$ Rated torque  $T_M = 13 \text{ (N.m)}$ Rotor inertia  $GD^2_M = 120 \text{ (kgf.cm}^2)$ 

## (4) Effective torque:

$$\begin{aligned} T_{rms} &= \sqrt{\frac{T_{k1}^2 \times t_1 + T_{l1}^2 \times t_2 + T_{g1}^2 \times t_3 + T_{k2}^2 \times t_4 + T_{l2}^2 \times t_5 + T_{g2}^2 \times t_6}{t}} \\ &= \sqrt{\frac{1105^2 \times 1.0 + 600^2 \times 5 + 1265^2 \times 1 + 1275^2 \times 0.2 + 610^2 \times 5.8 + 1125^2 \times 0.2}{20}} \\ &= 606 \text{ (N.cm)} < 1300 \text{ (N.cm)} \end{aligned}$$

◎It conforms to design requirements.

## 4 ◀ Calculating the stress of the Ballscrew

$$\begin{aligned} \sigma &= \frac{F}{A} = \frac{F_{max}}{\pi dr^2/4} \\ &= \frac{3903 \times 9.8 \times 4}{\pi \times 35.05^2} \quad dr = 40 + 1.4 - 6.35 = 35.05 \text{ (mm)} \\ &= 4.04 \text{ N/mm}^2 \quad (dr \text{ is screw shaft thread root diameter}) \\ &= 4.04 \times 10^6 \text{ N/m}^2 \\ \tau &= \frac{T \times r}{J} \quad T_{max} = T_L = 1275 \text{ (N.cm)} = 12750 \text{ (N.mm)} \\ &= \frac{12750 \times 20}{148167} \quad J = \frac{\pi dr^4}{32} = \frac{\pi (35.05^4)}{32} = 148167 \text{ (mm}^4) \\ &= 1.72 \text{ N/mm}^2 \\ &= 1.72 \times 10^6 \text{ N/m}^2 \\ \sigma_{max} &= \sqrt{\sigma^2 + \tau^2} \\ &= 4.39 \times 10^6 \text{ N/m}^2 \end{aligned}$$

50CrMo4 steel tension strength is  $1.1 \times 10^8 \text{ N/m}^2 > \sigma_{max}$ Yield strength is  $0.9 \times 10^8 \text{ N/m}^2 > \sigma_{max}$ 

◎So the Ballscrew selected is safe.

## 5 ◀ Calculating the buckling load of the screw shaft

$$\begin{aligned} P &= \alpha \frac{\pi^2 n EI}{L^2} = m \frac{dr^4}{L^2} \times 10^3 \\ &= 10.2 \times \frac{35.05^4}{1800^2} \times 10^3 \\ &= 4751 \text{ (kgf)} > F_{max} (398 \text{ kgf}) \end{aligned}$$

◎So the Ballscrew selected is safe.

PMI's design of hollow cooling system is especially good for high speed Ballscrews. It shall well dissipate heat generated by friction between balls and grooves during Ballscrew running, and then to minimize thermal deformation as to ensure positioning accuracy.

### 11.1 Introduction to Hollow Cooling Screw Shaft

The hollow cooling system is designed by PMI (Fig.11.1) It uses a coolant pipe through the hollow hole of Ballscrew. The hollow hole is through all of the Ballscrew, and one end is clogged with the oil seal by PMI patent. The coolant is pumped into coolant pipe and flow to the end of coolant pipe. Coolant then flow reversely along the hollow hole back into the coolant collector. It can cool down the Ballscrew. The coolant is then sucked back to the cooling unit to drop coolant temperature and pumped again to the coolant pipe to complete circulation.

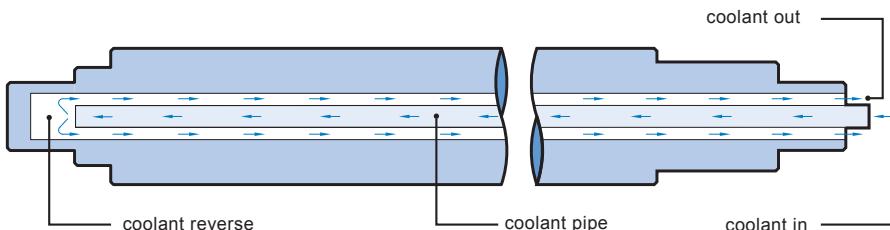


Fig.11.1 Hollow cooling diagram

### 11.2 Patent of Hollow Cooling Screw Shaft

#### 11.2.1 Hollow cooling system

Features:

- (i) Well and effectively control Ballscrew thermal expansion.
- (ii) Simple design and structure to save cost.



Fig.11.2 Hollow cooling system

#### 11.2.2 Cooling entrance

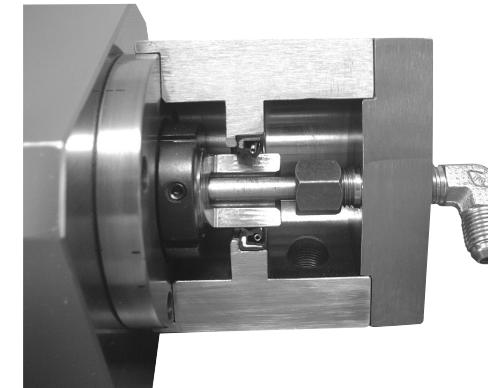


Fig.11.3 Cooling entrance

### 11.2.3 End sealing

Features:Easy for installing, disassembling and maintenance.

### 11.2.4 Coolant pipe support installation

Supported the coolant pipe. Let it don't touch Ballscrew.

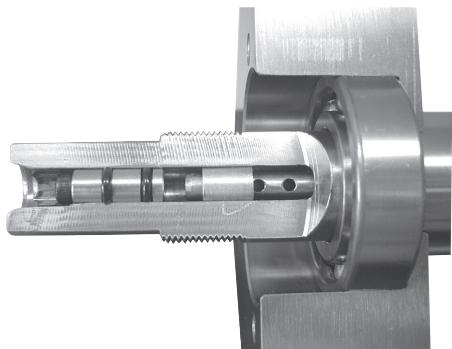


Fig 11.4 End sealing structure

### 11.2.5 Thermal control system test equipment



Fig.11.5 Thermal control system test equipment

## 11.3 Thermal control experiment

### 11.3.1 Test condition

Screw nominal O.D.: Ø40 mm  
 Lead: 10 mm  
 Rotation speed: 1000 rpm  
 Speed: 10 m/min  
 Load: 400 kgf  
 Slideways: Box ways

### 11.3.2 The results of experiment

As per the results by experiment, PMI's design of hollow cooling system proves an effective way for controlling the thermal expansion on the Ballscrew. Hence it is a very helpful design to high precision machine tools.

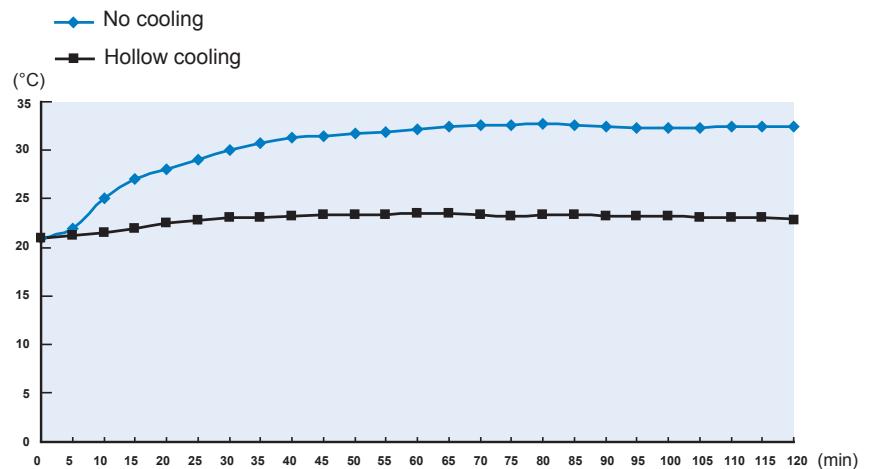


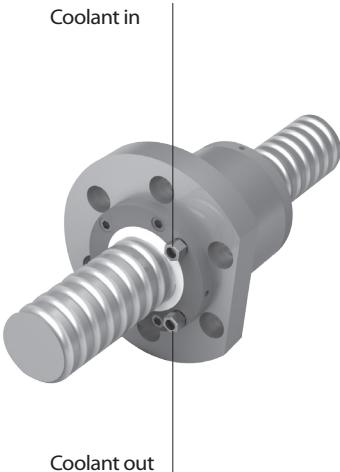
Fig.11.6 The results of experiment

## 11.4 Nut Cooling

### (1) The principle of design

Cool liquid is able to control the heat generation and thermal expansion by creating circulating cooling channel in the nut.

**Single Nut Cooling**



**Double Nut Cooling**

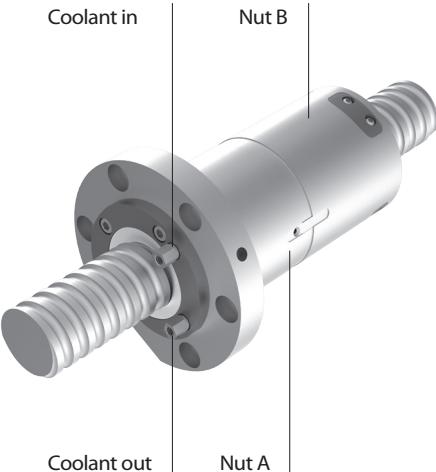


Fig.11.7 Single nut cooling and Double nut cooling diagram

### (2) Characteristics:

#### 1. Increase the positioning accuracy and the stability

Control the temperature rise of the ballscrew and reduced the heat deformation. The high velocity and accuracy of the machine will be reached.

#### 2. Decrease the warm-up time of machine

The stable temperature of the ballscrew be quickly, so the warm-up time of the machine could be shortened.

#### 3. Maintain capability of the lubrication oil

When the temperature of the ballscrew is stabilized, it is able to avoid the deterioration of the lubrication caused by high temperature.

Table11.1 Testing Parameters

Model no.	R45-12T5-FDDC-1274-1569-0.018
Operation travel(mm)	690
Feed speed(m/min)	7.2
Mean rotation (rpm)	523.3
Acceleration (m/s <sup>2</sup> )	5
Preload (kgf)	392
Table weight (kgf)	200
Mounting method	fixed-supported
Coolant	Mobil Velocite oil no.3 (ISO VG 2)
Coolant flow (L/min)	3.1
Coolant Temperature (°C)	Room temperature ±0.5

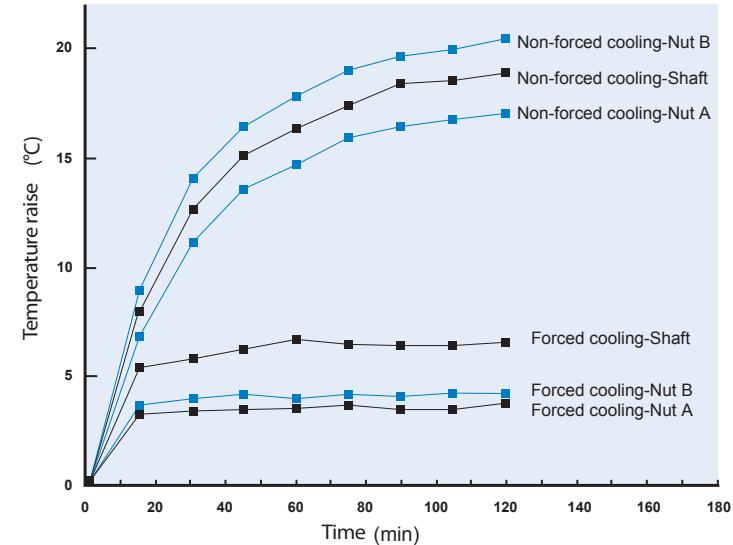
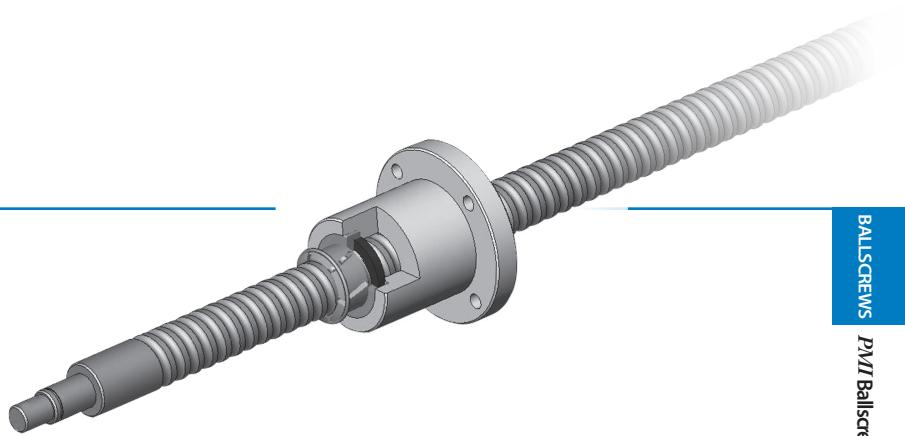


Fig.11.8 The results of experiment



## 12.1 BallScrew of High Dustproof-Type 1

### Design Concept

Scrapers specially developed for ballscrews, with a multi-layered contact structure that ensures effective dust removal.

### Features

#### High Compatibility

High dustproof scrapers can be used with various **PMI** products, including external and internal ball circulation nuts such as the E-type and D-type nuts etc...

#### Improved Dustproof Capacity

With a reduced mounting surface of the scraper spring, threads are more closely matched, making for a better scraping capacity.

#### Pioneering Design

Greatly improves dustproof effect

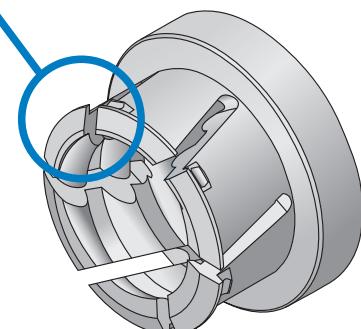


Fig.12.1 High dustproof type1

#### Long Endurance

The outer ring of the scraper is clamped by a spring. As the scraper gradually wears, the preload of scraper is automatically adjusted.

#### High Durability

With scrapers that closely fits the threads of the ballscrew and seal pads that match the axial cross section, the inside of the nut is completely safe from dust.

### Characteristics

#### 1.Seal Washer

As the ballscrew comes with specially designed grooves, the highly dustproof seal washer inside the scraper perfectly matches the threads, a feature that ensures the removal of scraps as well as insulation against dust.

#### 2.Scraper Design

The thread matching design of the scraper greatly boosts its efficiency. If the length of the nut deviates from average specifications, please contact **PMI** engineers.

#### 3.Shaft End Design

The shaft ends of the ballscrew should not be larger than the root diameter ( $dr$ ). If you have any questions concerning the size of the rest area of the ballscrew, please contact **PMI** engineers.

### Fits the Following Types of Nuts

FSWC.FDW.C.FSVC.FDVC.FSWE.FDWE.FSVE.FDVE.FSDC.FDDC.FSIC.FDIC.FOWC.FOVC.

(For detailed specifications, please refer to the specification table.)

For other specifications, please contact **PMI** engineers.

### Nomenclature

Example: R 32-10 B2-F S V E- 600 – 700 - 0.008 A

A Precision Ground Ballscrew + High dustproof wiper

### Applications of High Dustproof Ballscrews

Woodworking machines, laser processing machines, high accuracy transportation equipment, mechanical arms, and other machines that require a dustproof environment.

## 12.2 BallScrew of High Dustproof-Type 2

### Features

#### Design Concept

Wiper specially developed for ball screws, with a multi-step contact lips structure that ensures effective dust removal.

#### Long service life time

The contact Gothic arch thread of bulgy shape and the lips interference outside diameter of screw shaft, so the dust can't entry inside of nut.

#### High compatibility

High dustproof wiper can be used with various **PMI** products.

#### Nut length unchanging

Install high dustproof of type 2 , the nut length unchanging.

### Characteristics

#### Seal Washer

As the ballscrew comes with specially designed grooves, the highly dustproof seal washer inside the scraper perfectly matches the threads, a feature that ensures the removal of scraps as well as insulation against dust.

No necessary for a complete thread on end of ball screw shaft (see page A47)

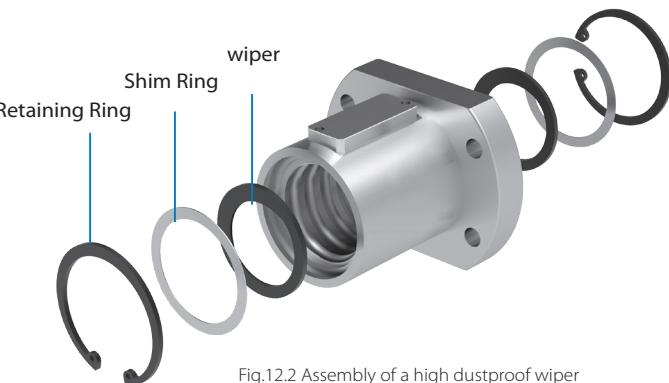


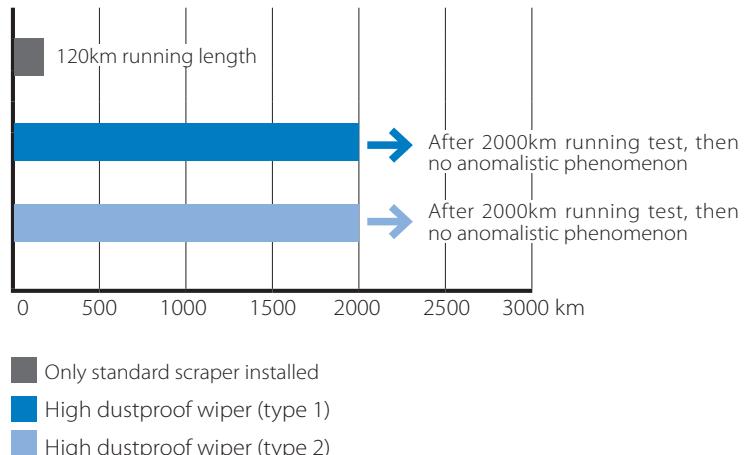
Fig.12.2 Assembly of a high dustproof wiper

### Additional Remarks

- Using the high dustproof scraper may induce an increase in preload. If your machine has a strict requirement on the range of preload, please contact **PMI** engineers.
- High dustproof seal washers should not be used in an environment where the temperature exceeds 80°C.
- Due to potential sealing problems with returning tubes, please contact **PMI** engineers if you need to use external ball circulation nuts (such as FSWC and FSVC).

### Test Condition

Specifications	R40-10-FSVE
Running Length	300 mm (per cycle)
Motor Speed	150 rpm
Test Environment	Sawdust automatic circulation system
Minimal Size of Dust Particles	below 0.01mm



## 12.3 BallScrew of High Dustproof-Type 3

### Features

#### Design Concept

The dustproof seals develop focus on general tool machine industrial that doesn't obviously increase of preload torque and temperature rise.

#### Long service life time

Provide the kind of seals that have better strength, service life and prevent fine dust or metal bit into the nut.

#### Improved Dustproof Capacity

A special ball screw groove profile together with the grease retaining film seals.

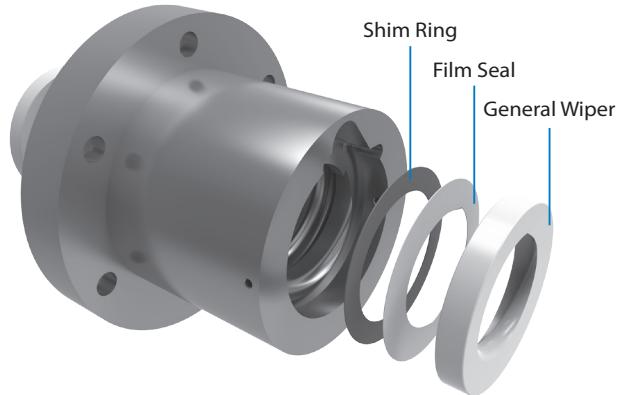
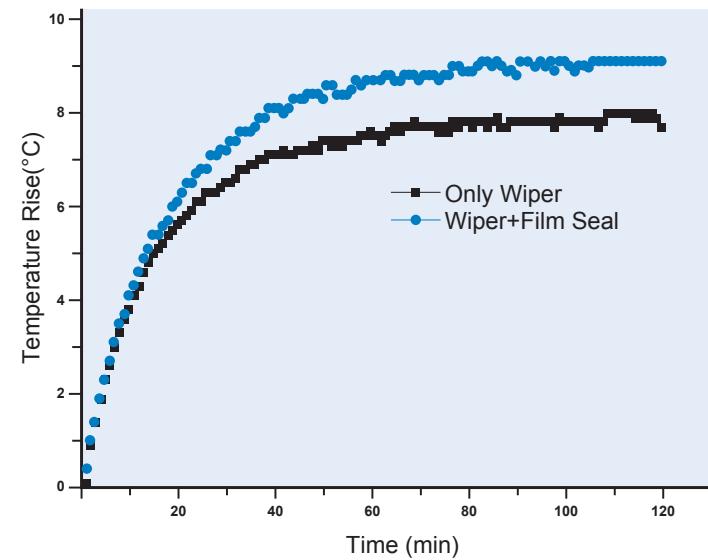


Fig.12.3 Assembly of a Film seal

### Heat generate and preload torque

The preload torque increase only 1~2 kgf-cm with film seals for ballscrew. Compare with non-contact wiper, the suppression temperature rise at 1.5~2°C.



## PMI Precision Ground BallScrew

## 13.1 Internal Ball Circulation Nuts

## Features:

The advantage of internal ball circulation nut is that the outer diameter is smaller than that of external ball circulation nut. Hence it is suitable for the machine with limit space for Ballscrew installation.

It is strictly required that there is at least one end of screw shaft with complete threads. Reference A47 Also the rest area next to this complete thread must be with smaller diameter than the nominal diameter of the screw shaft. Above are required for easy assembling the ballnut onto the screw shaft.

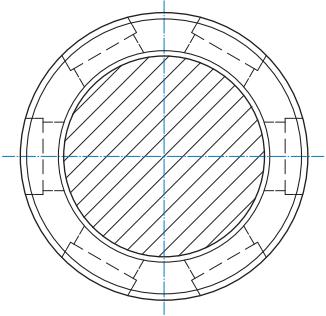
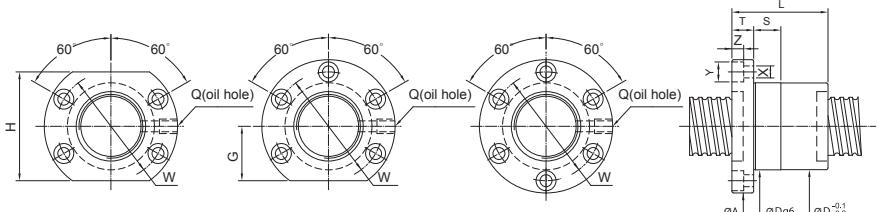
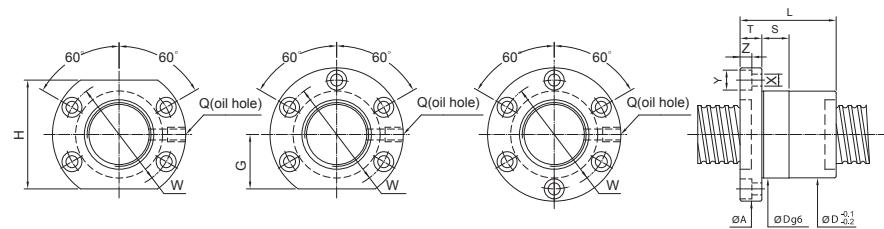


Fig. 13.1 Internal ball circulation's side view

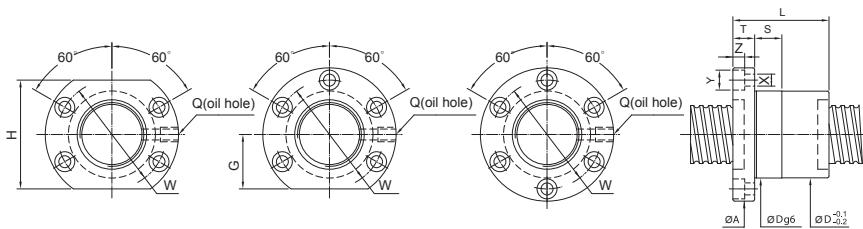


SCREW SIZE		BALL DIA.	EFFECTIVE TURNS	BASIC RATE LOAD(kgf)		NUT		FLANGE					FIT		BOLT			OIL HOLE	STIFFNESS
O.D.	LEAD			Dynamic (1x10 <sup>6</sup> REV.) Ca	Static Co	Dg6	L	A	T	W	G	H	S	X	Y	Z	Q	kgf/μm	
14	3	2	3	260	460	26	37	46	10	36	-	-	10	4.5	8	4.5	M6×1P	13	
	4	2.381	3	420	805	26	42	46	10	36	20	40	10	4.5	8	4.5	M6×1P	14	
	2.778	4	840	1870		42												21	
16	5	3.175	3	720	1010	26	42	46	10	36	20	40	10	4.5	8	4.5	M6×1P	16	
	4	2.381	3	435	920	28	42	49	10	39	20	40	10	4.5	8	4.5	M6×1P	16	
	5	3.175	3	765	1240	30	42	49	10	39	20	40	10	4.5	8	4.5	M6×1P	18	
	4	980	4	1650	30	55	49	10	39	20	40	10	4.5	8	4.5		23		
20	6	3.175	4	980	1650	30	55	54	12	40	20	40	12	5.5	9.5	5.5	M6×1P	23	
	4	2.381	4	600	1530	34	44	60	12	48	22	44	12	5.5	9.5	5.5	M6×1P	25	
	5	3.175	3	860	1710		47											21	
	6	3.175	4	1100	2280	34	53	57	12	45	20	40	12	5.5	9.5	5.5	M6×1P	28	
	6	1560	3420	3420	3420	62												42	
25	6	3.969	3	1080	2050	34	53	57	12	45	20	40	12	5.5	9.5	5.5	M6×1P	22	
	4	3.969	4	1380	2730	34	61	57	12	45	20	40	12	5.5	9.5	5.5	M6×1P	28	
	10	3.175	3	860	1710	36	66	57	12	45	20	40	12	5.5	9.5	5.5	M6×1P	21	
	4	2.381	3	500	1440	40	40	63	12	51	22	44	15	5.5	9.5	5.5	M8×1P	23	
	5	3.175	3	980	2300		47											26	
28	5	3.175	4	1250	3070	40	53	63.5	12	51	22	44	15	5.5	9.5	5.5	M8×1P	33	
	5	1520	3830	3830	3830	57												42	
	6	3.969	3	1275	2740	40	53	63.5	12	51	22	44	15	5.5	9.5	5.5	M8×1P	26	
	6	3.969	4	1630	3650	40	61	63.5	12	51	22	44	15	5.5	9.5	5.5	M8×1P	34	
	8	3.969	4	1630	3650	40	69	63.5	12	51	22	44	15	5.5	9.5	5.5	M8×1P	34	
30	8	3.969	5	1970	4560	40	77	63.5	12	51	22	44	15	5.5	9.5	5.5	M8×1P	43	
	3.175	3	980	2300	38	70	68	15	55	26	52	15	6.6	11	6.5	M8×1P	26		
	4	1250	3070	3070	3070	81												33	
	10	3.175	3	1620	3205		80											27	
	4.762	4	2070	4270	42	85	68.5	15	55	26	52	15	6.6	11	6.5	M8×1P	35		
32	5	2510	5340	5340	5340	91												44	
	6	3.175	3	1030	2630	43	50	68	12	55	26	52	15	6.6	11	6.5	M8×1P	28	
	10	3.175	4	1320	3510	45	77	73	12	60	30	60	15	6.6	11	6.5	M8×1P	37	



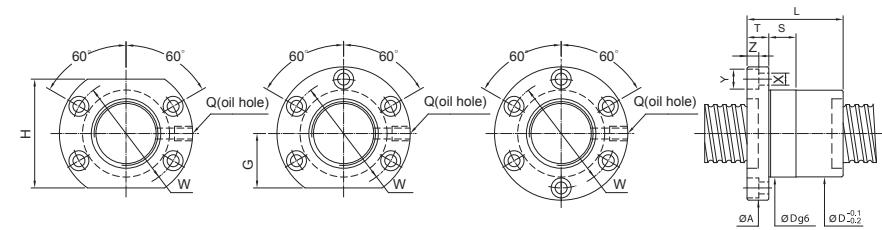
Unit: mm

SCREW SIZE	BALL	EFFECTIVE	BASIC RATE LOAD(kgf)		NUT		FLANGE				FIT		BOLT			OIL HOLE	STIFFNESS			
			O.D.	LEAD	DIA.	TURNs	Dynamic (1x10 <sup>6</sup> REV.) Ca	Static Co	Dg6	L	A	T	W	G	H	S	X	Y	Z	Q
32	4	2.381	3	560	1840	43	40	68	15	55	26	52	15	6.6	11	6.5	M8×1P	28	45	
		5	870	3070	49															
	5	3.175	3	1095	3060	47														31
		4	1400	4080	48	53	73.5	12	60	30	60	15	6.6	11	6.5	M8×1P	41			
	6	1980	6120	62																60
		3	1500	3750	53															32
	6	3.969	4	1920	5000	48	61	73.5	12	60	30	60	15	6.6	11	6.5	M8×1P	43		
		6	2720	7500	73															63
	8	4.762	3	1820	4230	50	68	83	16	66	32	64	15	6.6	11	6.5	M8×1P	32		
		4	2330	5640	77															43
36	10	6.35	3	2605	5310	54	80	90	88	16	70	34	68	15	9	14	8.5	M8×1P	33	
		4	3340	7080	90															45
	12	6.35	3	2605	5310	50	86	88	16	70	34	68	15	9	14	8.5	M8×1P	33		
		5	3.175	4	1490	4690	52	56	88	16	70	34	68	15	9	14	8.5	M8×1P	46	
	8	4.762	4	2530	6630	55	73	88	16	72	29	58	15	9	14	8.5	M8×1P	48		
		10	6.35	3	2810	6210	58	78	98	18	77	36	72	20	11	17.5	11	M8×1P	37	
	10	6.35	4	3600	8280	89														49
		4	1575	5290	56															49
40	5	3.175	5	1910	6610	55	61	88.5	16	72	29	58	15	9	14	8.5	M8×1P	61		
		6	2230	7940	65															73
	6	3.969	3	1660	4810	56														39
		4	2130	6410	55	65	88.5	16	72	34	68	15	9	14	8.5	M8×1P	51			
	6	3.969	6	3020	9620	77														75
		3	2120	5720	64															40
	8	4.762	4	2720	7620	60	77	93	16	76	36	72	20	9	14	8.5	M8×1P	52		
		6	3850	11430	94															77
12	10	6.35	3	3010	7100	83														41
		4	3850	9470	64	93	106	18	84	43	86	20	11	17.5	11	M8×1P	53			
	5	4670	11830	99																67
		6.35	3	3010	7100	82														41
	7.144	4	3850	9470	63	100	106	18	84	43	86	20	11	17.5	11	M8×1P	53			
		5	4670	11830	108															67
	7.144	3	4010	9250	70	93	110	18	85	45	90	20	11	17.5	11	M8×1P	43			
		4	5130	12330	103															56



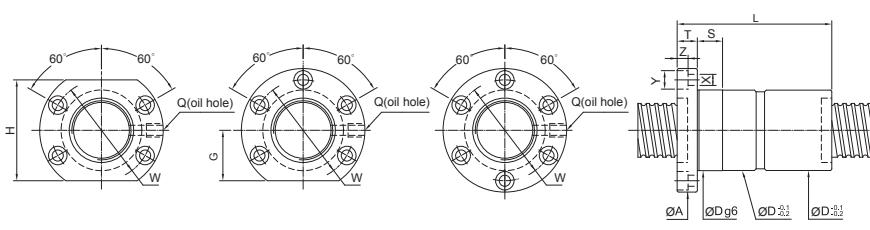
Unit: mm

SCREW SIZE	BALL	EFFECTIVE	BASIC RATE LOAD(kgf)		NUT		FLANGE				FIT		BOLT			OIL HOLE	STIFFNESS			
			O.D.	LEAD	DIA.	TURNs	Dynamic (1x10 <sup>6</sup> REV.) Ca	Static Co	Dg6	L	A	T	W	G	H	S	X	Y	Z	Q
45	8	4.762	4	2870	8620	64	72	92	16	75	36	72	15	9	14.5	9	M6×1P	54		
		12	7.144	3	4160	10750	70	86	110	16	90	42	84	20	11	17.5	11	PT1/8"	48	
	12	7.144	4	5330	14330	70	99	110	16	90	42	84	20	11	17.5	11	PT1/8"	62		
		16	6.35	3	3220	8200	70	102	110	16	90	42	84	20	11	17.5	11	PT1/8"	45	
	6	3.175	4	1730	6760	55														60
		6	2100	8450	66	61	98	16	82	36	72	20	9	14	8.5	PT1/8"	74			
	6	3.969	5	2380	8250	65														86
		6	3370	12380	77															61
	8	4.762	4	3010	9610	79														63
		8	3650	12010	70	84	113	18	90	42	84	20	11	17.5	11	PT1/8"	77			
50	10	6.35	3	3430	9300	83														92
		5	4390	12400	93															49
	10	5	5320	15500	74	99	116	18	94	42	84	20	11	17.5	11	M8×1P	80			
		6	6220	18600	114															95
	12	7.144	4	5520	16330	75	104	121	22	97	47	94	20	14	20	13	PT1/8"	67		
		7.938	3	4510	11150	75	99	121	22	97	47	94	20	14	20	13	PT1/8"	84		
	12	7.938	4	5770	14870	75	111	121	22	97	47	94	20	14	20	13	PT1/8"	60		
		16	6.35	3	3430	9300	74	104	116	18	94	42	84	20	11	17.5	11	PT1/8"	49	
	20	7.938	3	4510	11150	78	146	121	28	97	47	94	20	14	20	13	PT1/8"	50		



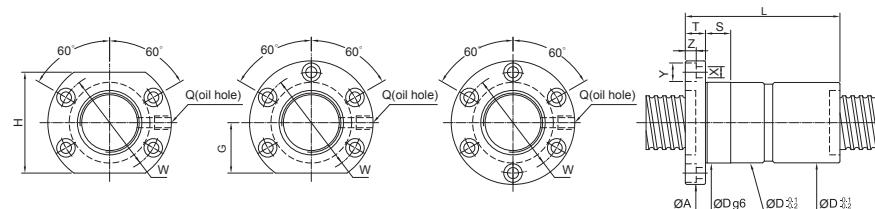
Unit: mm

SCREW SIZE	BALL	EFFECTIVE	BASIC RATE LOAD(kg)		NUT		FLANGE			FIT		BOLT			OIL HOLE	STIFFNESS kgf/ $\mu$ m	
			Dynamic ( $1 \times 10^6$ REV.) Ca	Static Co	Dg6	L	A	T	W	G	H	S	X	Y	Z	Q	
63	6 3.969	4	2610	10550	80	67	122	18	100	45	90	20	11	17.5	11	PT1/8"	73
	6 3700	6	15830	80	80												107
	8 4.762	4	3375	12200	82	80	124	18	102	46	92	20	11	17.5	11	PT1/8"	76
	6 4780	6	18300	96													111
	10 6.35	4	5020	16450	85	98	132	22	107	48	96	20	14	20	13	PT1/8"	79
	6 7110	6	24680	118													116
	12 7.938	4	6580	19430	90	111	136	22	112	52	104	20	14	20	13	PT1/8"	80
	6 9320	6	29150	136													111
	20 9.525	3	8490	23610	95	146	153	28	123	59	118	20	18	26	17.5	PT1/8"	79
	4 10870	4	31480	156													89
80	4	5510	21200	98													95
	10 6.35	5	6670	26500	105	105	151	22	127	57	114	20	14	20	13	PT1/8"	118
	6 7810	6	31800	118													140
	12 7.938	4	7500	25700	110	111	156	22	132	59	118	20	14	20	13	PT1/8"	98
	6 10620	6	38550	136													143
	20 9.525	3	9770	31700	115	146	173	28	143	66	132	20	18	26	17.5	PT1/8"	97
	4 12510	4	42270	168													127
100	3	4760	20090	84													91
	10 6.35	4	6090	26790	95	171	22	147	67	134	25	14	20	13	PT1/8"	120	
	5 7380	5	33490	125	104												148
	6 8630	6	40190	115													176
	4	14440	54960	140													140
	16 9.525	5	17490	68700	135	157	205	28	169	73	146	30	18	26	17.5	PT1/8"	173
	6 20460	6	82440	175													205
20 9.525	4	14440	54960	159													140
	5 17490	5	68700	135	180	205	28	169	73	146	30	18	26	17.5	PT1/8"	173	
	6 20460	6	82440	200													205



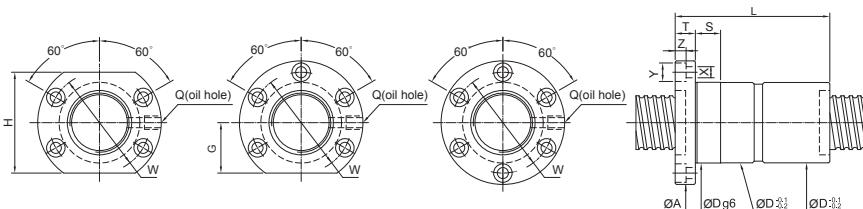
Unit: mm

SCREW SIZE	BALL	EFFECTIVE	BASIC RATE LOAD(kg)		NUT		FLANGE			FIT		BOLT			OIL HOLE	STIFFNESS kgf/ $\mu$ m	
			Dynamic ( $1 \times 10^6$ REV.) Ca	Static Co	Dg6	L	A	T	W	G	H	S	X	Y	Z	Q	
16	4 2.381	3	435	920	30	66	46.5	10	39	20	40	10	4.5	8	4.5	M6×1P	31
	5 3.175	3	765	1240	30	80	49	10	39	20	40	10	4.5	8	4.5	M6×1P	35
	5 3.175	4	980	1650													47
	5 3.175	3	860	1710	34	82	57	12	45	20	40	12	5.5	9.5	5.5	M6×1P	43
	5 3.175	4	1100	2280													56
	6 3.969	3	1080	2050	34	93	57	12	45	20	40	12	5.5	9.5	5.5	M6×1P	43
	6 3.969	4	1380	2730													56
	5 3.175	3	980	2300	40	82	63.5	12	51	22	44	15	5.5	9.5	5.5	M8×1P	51
	5 3.175	4	1250	3070													67
	6 3.969	3	1275	2740	40	93	63.5	12	51	22	44	15	5.5	9.5	5.5	M8×1P	52
25	6 3.969	4	1630	3650	40	107	63.5	12	51	22	44	15	5.5	9.5	5.5	M8×1P	68
	3.175	3	980	2300	40	129	68	15	55	26	52	15	6.6	11	6.5	M8×1P	51
	10 4.762	3	1620	3205	42	140	68.5	15	55	26	52	15	6.6	11	6.5	M8×1P	53
	4 2070	4	2070	4270													70
	3	1095	3060	82													63
	5 3.175	4	1400	4080	48	92	73.5	12	60	30	60	15	6.6	11	6.5	M8×1P	82
	6 1980	6	1980	6120													122
32	3	1500	3750	93													65
	6 3.969	4	1920	5000	48	109	73.5	12	60	30	60	15	6.6	11	6.5	M8×1P	86
	6 2720	7500															125
	8 4.762	3	1820	4230	50	117	83	16	66	32	64	15	6.6	11	6.5	M8×1P	66
	4 2330	5640															86
	10 6.35	3	2605	5310	50	139	88.5	16	70	34	68	15	9	14	8.5	M8×1P	67
	4 3340	7080															89
36	12 6.35	3	2605	5310	50	153	88	16	70	34	68	15	9	14	8.5	M8×1P	67
	5 4040	8850															110
	5 3.175	4	1490	4690	52	96	88	16	70	34	68	15	9	14	8.5	M8×1P	91
	8 4.762	4	2530	6630	55	138	88	16	72	34	68	15	9	14	8.5	M8×1P	95
	10 6.35	3	2810	6210	58	138	98	18	77	36	72	20	11	17.5	11	M8×1P	75
	4 3600	8280															98

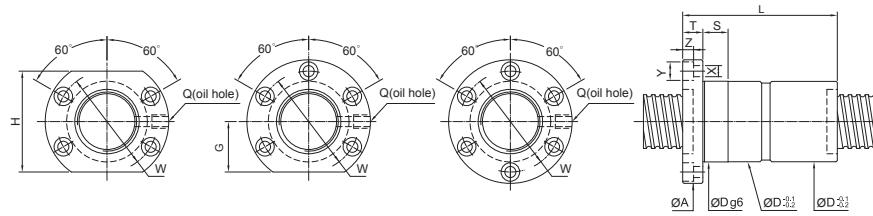


Unit: mm

SCREW SIZE	BALL	EFFECTIVE	BASIC RATE LOAD(kgf)		NUT		FLANGE			FIT		BOLT			OIL HOLE	STIFFNESS kgf/ $\mu$ m		
			Dynamic (1x10 <sup>6</sup> REV.) Ca	Static Co	Dg6	L	A	T	W	G	H	S	X	Y	Z	Q		
40	4	1575	5290	96												100		
		5	1910	6610	55	111	88.5	16	72	29	58	15	9	14	8.5	M8×1P	124	
		6	2230	7940		122											147	
	6	3.969	1660	4810	97												77	
		4	2130	6410	55	113	88.5	16	72	34	68	15	9	14	8.5	M8×1P	103	
		6	3020	9620		137											149	
	8	4.762	2120	5720	121												80	
		4	2720	7620	60	134	93	16	76	36	72	20	9	14	8.5	M8×1P	105	
		6	3850	11430		172											154	
	10	6.35	3010	7100	142												82	
		4	3850	9470	65	162	106	18	84	43	86	20	11	17.5	11	M8×1P	107	
		5	4670	11830		189											133	
45	6.35	3	3010	7100	63	154											82	
		5	4670	11830		204	106	18	84	43	86	20	11	17.5	11	M8×1P	133	
	7.144	3	4010	9250	70	160	110	18	85	45	90	20	11	17.5	11	M8×1P	86	
		4	5130	12330		185											114	
	8	4.762	2870	8620	64	136	92	16	75	36	72	15	9	14.5	9	M6×1P	109	
	12	7.144	3	4160	10750	70	158	110	16	90	45	90	20	11	17.5	11	PT1/8"	94
		4	5330	14330		183											124	
	16	6.35	3	3220	8200	70	198	110	16	90	45	90	20	11	17.5	11	PT1/8"	90

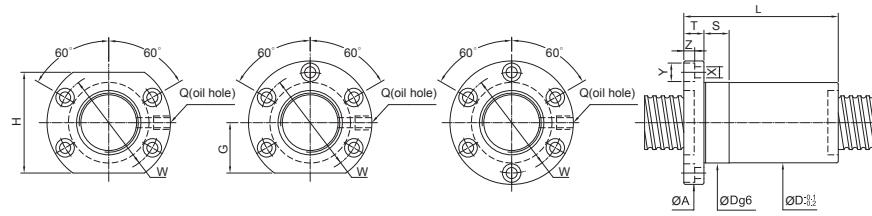


SCREW SIZE	BALL	EFFECTIVE	BASIC RATE LOAD(kgf)		NUT		FLANGE			FIT		BOLT			OIL HOLE	STIFFNESS kgf/ $\mu$ m		
			Dynamic (1x10 <sup>6</sup> REV.) Ca	Static Co	Dg6	L	A	T	W	G	H	S	X	Y	Z	Q		
50	4	1730	6760	96												119		
		5	2100	8450	66	111	98	16	82	36	72	20	9	14	8.5	PT1/8"	148	
		6	2450	10140		122											174	
	6	2380	8250		111												123	
		5	2880	10310	66	122	98	16	82	36	72	20	9	14	8.5	PT1/8"	151	
		6	3370	12380		142											181	
	8	3010	9610	136													125	
		5	3650	12010	70	157	113	18	90	42	84	20	11	17.5	11.0	PT1/8"	155	
		6	4260	14420		174											185	
	10	3430	9300	143													99	
		4	4390	12400	74	162	114	18	92	42	84	20	11	17.5	11	PT1/8"	129	
		5	5320	15500		189											161	
	12	6220	18600	205													191	
		7.144	6680	20420	75	213	121	22	97	47	94	20	14	20	13	PT1/8"	166	
		3	4510	11150	75	171	121	22	97	47	94	20	14	20	13	PT1/8"	101	
	4	5770	14870		195												132	
	16	6.35	3	3430	9300	74	201	114	18	92	42	84	20	11	17.5	11	PT1/8"	99
	20	7.938	3	4510	11150	78	253	121	28	97	47	94	20	14	20	13	PT1/8"	101



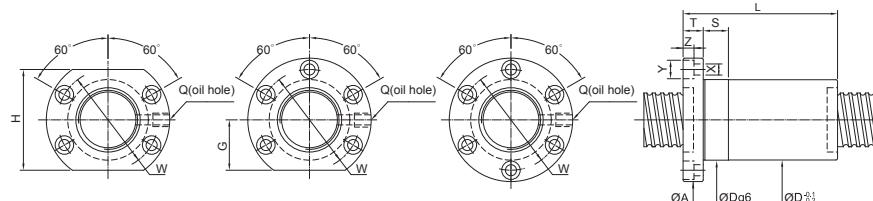
Unit: mm

SCREW SIZE	BALL DIA.	EFFECTIVE TURNS	BASIC RATE LOAD(kgf)		NUT		FLANGE			FIT		BOLT		OIL HOLE	STIFFNESS kgf/μm			
			Dynamic (1×10 <sup>6</sup> REV.) Ca	Static Co	Dg6	L	A	T	W	G	H	S	X	Y	Z			
63	6	3.969	4	2610	10550	80	120	122	18	100	45	90	20	11	17.5	11	PT1/8"	146 217
			6	3700	15830	144												
	8	4.762	4	3375	12200	82	141	124	18	102	46	92	20	11	17.5	11	PT1/8"	151 222
			6	4780	18300	178												
	10	6.35	4	5020	16450	85	166	132	22	107	48	96	20	14	20	13	PT1/8"	158 232
			6	7110	24680	209												
80	12	7.938	4	6580	19430	90	195	136	22	112	52	104	20	14	20	13	PT1/8"	161 236
			6	9320	29150	248												
	20	9.525	3	8490	23610	95	255	153	28	123	59	118	20	18	26	17.5	PT1/8"	157 207
			4	10870	31480	296												
	10	6.35	4	5510	21200	166												190
			5	6670	26500	105	185	151	22	127	57	114	20	14	20	13	PT1/8"	235
100			6	7810	31800	209												280
	12	7.938	4	7500	25700	110	195	156	22	132	59	118	20	14	20	13	PT1/8"	196 288
			6	10620	38550	248												
	20	9.525	3	9770	31700	254												193
			4	12510	42270	115	297	173	28	143	66	132	20	18	26	17.5	PT1/8"	254 373
			6	17720	63410	376												
100	10	6.35	3	4760	20090	143												173
			4	6090	26790	164												228
			5	7380	33490	125	171	22	147	67	134	25	14	20	13	PT1/8"	281 334	
			6	8630	40190	210												
	16	9.525	4	14440	54960	252												266
			5	17490	68700	135	285	205	28	169	73	146	30	18	26	17.5	PT1/8"	329 391
100			6	20460	82440	318												391
	20	9.525	4	14440	54960	299												266
			5	17490	68700	135	340	205	28	169	73	146	30	18	26	17.5	PT1/8"	329 391
			6	20460	82440	381												



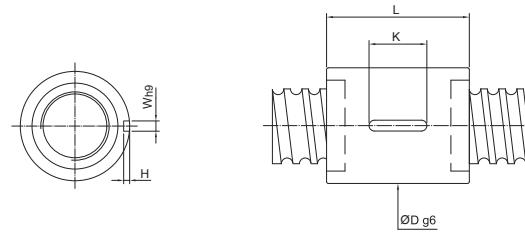
Unit: mm

SCREW SIZE	BALL DIA.	EFFECTIVE TURNS	BASIC RATE LOAD(kgf)		NUT		FLANGE			FIT		BOLT		OIL HOLE	STIFFNESS kgf/μm		
			Dynamic (1×10 <sup>6</sup> REV.) Ca	Static Co	Dg6	L	A	T	W	G	H	S	X	Y	Z		
20	5	3.175	2×(2)	610	1140	34	53									29	
			3×(2)	860	1710	34	67	57	12	45	20	40	12	5.5	9.5	5.5 M6×1P	43
25	6	3.969	2×(2)	760	1370	34	61									29	
			3×(2)	1080	2050	34	77	57	12	45	20	40	12	5.5	9.5	5.5 M6×1P	50
28	4	2.381	2×(2)	350	960	40	44									30	
			3×(2)	500	1440	40	56	63	12	51	22	44	15	5.5	9.5	5.5 M8×1P	46
32	5	3.175	2×(2)	690	1530	40	53									35	
			3×(2)	980	2300	40	67	63.5	12	51	22	44	15	5.5	9.5	5.5 M8×1P	51
32	6	3.969	3×(2)	1250	3070	40	76									67	
			4×(2)	1275	2740	40	77	63.5	12	51	22	44	15	5.5	9.5	5.5 M8×1P	52
32	8	3.969	3×(2)	1275	2740	40	85	63.5	12	51	22	44	15	5.5	9.5	5.5 M8×1P	52
			4×(2)	1140	2140	42	88	69	15	55	26	52	15	6.6	11	6.5 M8×1P	36
32	10	4.762	2×(2)	1610	3210	42	102									53	
			3×(2)	1030	2630	43	69	68	12	55	26	52	15	6.6	11	6.5 M8×1P	56
32	10	3.175	2×(2)	730	1750	45	77	73	12	60	30	60	15	6.6	11	6.5 M8×1P	38
			3×(2)	560	1840	43	56	68	12	55	26	52	15	6.6	11	6.5 M8×1P	55
32	4	2.381	5×(2)	870	3070	43	73									89	
			3×(2)	1095	3060	48	67	73.5	12	60	30	60	15	6.6	11	6.5 M8×1P	63
32	5	3.175	4×(2)	1400	4080	48	77									82	
			3×(2)	1500	3750	48	77	73.5	12	60	30	60	15	6.6	11	6.5 M8×1P	65
32	6	3.969	4×(2)	1920	5000	48	90									86	
			3×(2)	1820	4230	50	95	83	16	66	32	64	15	6.6	11	6.5 M8×1P	66
32	8	4.762	4×(2)	2330	5640	50	112									86	
			3×(2)	2605	5310	50	124	88	16	70	34	68	15	9	14	8.5 M8×1P	67
32	10	6.35	3×(2)	2605	5310	50	124									67	
			3×(2)	2605	5310	50	124	88	16	70	34	68	15	9	14	8.5 M8×1P	67



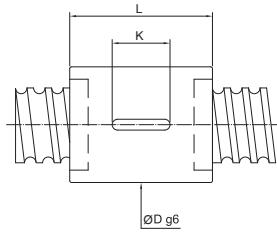
Unit: mm

SCREW SIZE	BALL	EFFECTIVE	BASIC RATE LOAD(kgf)		NUT	FLANGE				FIT	BOLT			OIL HOLE	STIFFNESS kgf/μm					
			O.D.	LEAD	DIA.	TURNs	Dynamic (1×10 <sup>5</sup> REV.) Ca	Static Co	Dg6	L	A	T	W	G	H	S	X	Y	Z	Q
40	5	3.175	3×(2)	1230	3970	65														75
			4×(2)	1575	5290	55	80	88.5	16	72	29	58	15	9	14	8.5	M8×1P	100		
			6×(2)	2230	7940	101														147
	6	3.969	4×(2)	2130	6410	55	93	88.5	16	72	34	68	15	9	14	8.5	M8×1P	103		
			6×(2)	3020	9620	118														149
	8	4.762	4×(2)	2720	7620	60	116	93	16	76	36	72	20	9	14	8.5	M8×1P	105		
	10	6.35	3×(2)	3010	7100	64	123	106	18	84	43	86	20	11	17.5	11	PT1/8"	82		
			4×(2)	3850	9470	143														107
	12	6.35	4×(2)	3850	9470	63	160	106	18	84	43	86	20	11	17.5	11	PT1/8"	107		
50	5	3.175	3×(2)	1350	5070	65														89
			4×(2)	1730	6760	66	80	98	16	82	36	72	20	9	14	8.5	PT1/8"	119		
			6×(2)	2450	10140	101														174
	6	3.969	4×(2)	2380	8250	66	93	98	16	82	36	72	20	9	14	8.5	PT1/8"	123		
			6×(2)	3370	12380	118														181
	8	4.762	4×(2)	3010	9610	70	119	113	18	90	42	84	20	11	17.5	11	PT1/8"	125		
	10	6.35	3×(2)	3430	9300	74	123	116	18	92	42	84	20	11	17.5	11	M8×1P	99		
			4×(2)	4390	12400	143														129
	12	7.144	4×(2)	5530	16330	75	164	121	22	97	47	97	20	14	20	13	PT1/8"	135		
63	12	7.938	3×(2)	4510	11150	75	147	121	22	97	47	97	20	14	20	13	PT1/8"	101		
			4×(2)	5770	14870	164													132	
	6	3.969	4×(2)	2610	10550	80	96	122	18	100	45	90	20	11	17.5	11	PT1/8"	146		
			6×(2)	3700	15830	121													217	
	8	4.762	4×(2)	3375	12200	82	119	124	18	102	46	92	20	11	17.5	11	PT1/8"	151		
	10	6.35	4×(2)	5020	16450	85	147	132	22	107	48	96	20	14	20	13	PT1/8"	158		
	12	7.938	3×(2)	5140	14570	90	147	136	22	112	52	104	20	14	20	13	PT1/8"	122		
			4×(2)	6580	19430	171													161	
	20	9.525	2×(2)	5990	15740	95	156	153	28	123	59	118	20	18	26	17.5	PT1/8"	107		
80	10	6.35	2×(2)	3360	13390	95	171	22	147	67	134	25	14	20	13	PT1/8"	118			
			3×(2)	4760	20090	115													173	
	16	9.525	2×(2)	11280	41220	115	175	205	28	169	73	146	30	18	26	17.5	PT1/8"	201		
	20	9.525	3×(2)	7960	27480	115	159	205	28	169	73	146	30	18	26	17.5	PT1/8"	137		

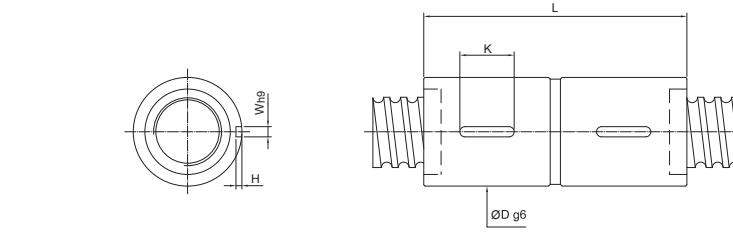


SCREW SIZE	BALL	EFFECTIVE	BASIC RATE LOAD(kgf)		NUT	KEYWAY			STIFFNESS						
			O.D.	LEAD	DIA.	TURNs	Dynamic (1×10 <sup>5</sup> REV.) Ca	Static Co	Dg6	L	K	W	H	kgf/μm	
16	5	3.175	3				765		1240	30	40	20	3	1.8	18
	5	3.175	3				860		1710	41					21
			4				1100		2280	34	48	20	3	1.8	28
	20	6	3.969				1080		2050	34					22
			4				1380		2730	56	25	4	2.5		28
	25	5	3.175				980		2300	40					26
			4				1250		3070	48	20	4	2.5		33
	25	6	3.969				1275		2740	40					26
			4				1630		3650	56	25	4	2.5		34
32	5	3.175	3				1095		3060	41					31
			4				1400		4080	48					41
			6				1980		6120	61					60
	6	3.969	3				1500		3750	46					32
			4				1920		5000	50					43
	6	2720	6				7500		70	32					63
			4				1820		4230	50					32
	8	4.762	3				2330		5640	70	25	5	3.0		43
	10	6.35	3				2605		5310	50					33
			4				3340		7080	79	32	6	3.5		45
40	5	3.175	4				1575		5290	48					49
	6	3.969	4				2230		7940	61					73
			6				2130		6410	56					51
	8	4.762	4				3020		9620	70					75
			6				2720		7620	91					52
	10	6.35	3				3850		11430	60					77
	10	3.175	3				3010		7100	65					41
			4				3850		9470	79	32	6	3.5		53

SCREW SIZE		BALL	EFFECTIVE	BASIC RATE LOAD(kgf)		NUT		KEYWAY			STIFFNESS
O.D.	LEAD	DIA.	TURNS	Dynamic (1×10 <sup>6</sup> REV.) Ca	Static Co	Dg6	L	K	W	H	kgf/μm
50	5	3.175	4	1730	6750	66	48	20	4	2.5	60
			6	2450	10130		61	25			86
	6	3.969	4	2380	8250	66	56	25	5	3.0	61
			6	3370	12380		70	32			90
	8	4.762	4	3010	9610	70	70				63
			6	4260	14420		91	32	5	3.0	92
63	3	3.175	4	3430	9300		68				49
	10	6.35	4	4390	12400	74	79	32	6	3.5	65
			6	6220	18600		102				95
	12	7.938	3	4510	11150	75	82	40	6	3.5	50
			4	5770	14870		92				66
	6	3.969	4	2610	10550	80	56	25	6	3.5	73
80	6	3.969	6	3700	15830		70	32			107
	8	4.762	4	3375	12200	82	70	32	6	3.5	76
			6	4780	18300		91	40			111
	10	6.35	4	5020	16450	85	79	32	8	4.0	79
			6	7110	24680		85	40			116
	12	7.938	4	6580	19430	90	95	40	8	4.0	80
100	6	9.525	4	9320	29150		123	50			118
	10	6.35	4	5510	21200	105	79	32	8	4.0	95
			6	7810	31800		102	40			140
	12	7.938	4	7500	25700	110	95	40	8	4.0	98
			6	10620	38550		123	50			143
	20	9.525	3	9770	31700	115	126	50	10	5.0	97
100			4	12510	42270		149	63			127
	10	6.35	3	4760	20090		72				91
			4	6090	26790	125	82				120
	5			7380	33490		94	50	10	5	148
			6	8630	40190		104				176
	16	9.525	4	14440	54960		128				140
20	5	17490		68700	135	77	63	10	5		173
		20460		82440			162				205
	6	17490		68700	135	164	63	10	5		173
20	9.525	4	14440	54960			144				140
		20460		82440			187				205



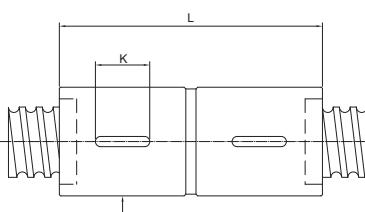
Unit: mm



Unit: mm

SCREW SIZE		BALL	EFFECTIVE	BASIC RATE LOAD(kgf)		NUT		KEYWAY			STIFFNESS
O.D.	LEAD	DIA.	TURNS	Dynamic (1×10 <sup>6</sup> REV.) Ca	Static Co	Dg6	L	K	W	H	kgf/μm
16	5	3.175	3	765	1240	28	75	20	3	1.8	35
			4	980	1650		85				47
	5	3.175	3	860	1710	34	75	20	3	1.8	43
			4	1100	2280		85				56
	6	3.969	3	1080	2050	34	87	20	4	2.5	43
			4	1380	2730		103	25			56
20	5	3.175	3	980	2300	40	75	20	4	2.5	51
			4	1250	3070		85				67
	6	3.969	3	1275	2740	40	87	20	4	2.5	52
			4	1630	3650		103	25			68
	5	3.175	3	1095	3060		75	20			63
			4	1400	4080	48	85	20	4	2.5	82
25	6	3.969	3	1480	6120		105	25			122
			4	1980							
	5	3.175	3	1500	3750		87	20			65
			4	1920	5000	50	103	25	5	3.0	86
	6	3.969	3	2720	7500		127	32			125
			4	2330	5640	50	127	25	5	3.0	86
32	8	4.762	3	1820	4230	50	109	25	5	3.0	66
			4	2330	5640		127				
	10	6.35	3	2605	5310	50	135	25	6	3.5	67
			4	3340	7080		155	32			89
	5	3.175	4	1575	5290	55	85	20	4	2.5	100
			6	2230	7940		105	25			147
40	6	3.969	4	2130	6410	55	103	25	5	3.0	103
			6	3020	9620		127	32			149
	8	4.762	4	2720	7620	60	127	25	5	3.0	105
			6	3850	11430		161	40			154
	10	6.35	3	3010	7100	65	135	25	6	3.5	82
			4	3850	9470		155	32			107

## RDIC



Unit: mm											
SCREW SIZE		BALL	EFFECTIVE	BASIC RATE LOAD(kgf)		NUT		KEYWAY		STIFFNESS	
O.D.	LEAD	DIA.	TURNS	Dynamic (1×10 <sup>6</sup> REV.) Ca	Static Co	Dg6	L	K	W	H	kgf/μm
50	5	3.175	4	1730	6750	66	85	20	4	2.5	119
			6	2450	10130		105	25			174
	6	3.969	4	2380	8250	66	103	25	5	3.0	123
			6	3370	12380		127	32			181
	8	4.762	4	3010	9610	70	127				125
			6	4260	14420		161	32	5	3.0	185
63	10	6.35	3	3430	9300	74	135	32			99
			4	4390	12400		155	32	6	3.5	129
			6	6220	18600		197	40			191
	12	7.938	3	4510	11150	75	161				101
			4	5770	14870		185	40	6	3.5	132
	6	3.969	4	2610	10550	80	106	25			146
80			6	3700	15830		130	32	6	3.5	217
	8	4.762	4	3375	12200	82	131	32			151
			6	4780	18300		165	40	6	3.5	222
	10	6.35	4	5020	16450	85	160	32	8	4.0	158
			6	7110	24680		202	40			232
	12	7.938	4	6580	19430	90	185	40	8	4.0	161
100			6	9320	29150		238	50			236
	10	6.35	4	5510	21200	105	160	32			190
			6	7810	31800		202	40	8	4.0	280
	12	7.938	4	7500	25700	110	185	40			196
			6	10620	38550		238	50	8	4.0	288
	20	9.525	3	9770	31700	115	245	50	10	5.0	193
			4	12510	42270		289	63			254
	10	6.35	3	4760	20090	125	132				173
			4	6090	26790		164				228
			5	7380	33490		174				281
			6	8630	40190		204				334
	16	9.525	4	14440	54960	135	240				266
			5	17490	68700		274	63	10	5	329
			6	20460	82440		306				391
	20	9.525	4	14440	54960		284				266
			5	17490	68700	135	324	63	10	5	329
			6	20460	82440		366				391

PMI Precision Ground BallScrew

## 13.2 End Deflector Series

## Features

It is important for a high-lead ballscrew to be with characteristics of high rigidity, low noise and thermal control.

PMI takes its patented design and treatments to achieve the following characteristics:

## High DN Value

Max. DN Value: 220,000

## Low Noise

The average and accurate ball circle diameter (BCD) through whole threads make the ballscrews to obtain the stable and consistent drag torque as well as to reduce the noise.

The audio frequency is low and downy due to the designed of plastic circulation system.

## Space Saving

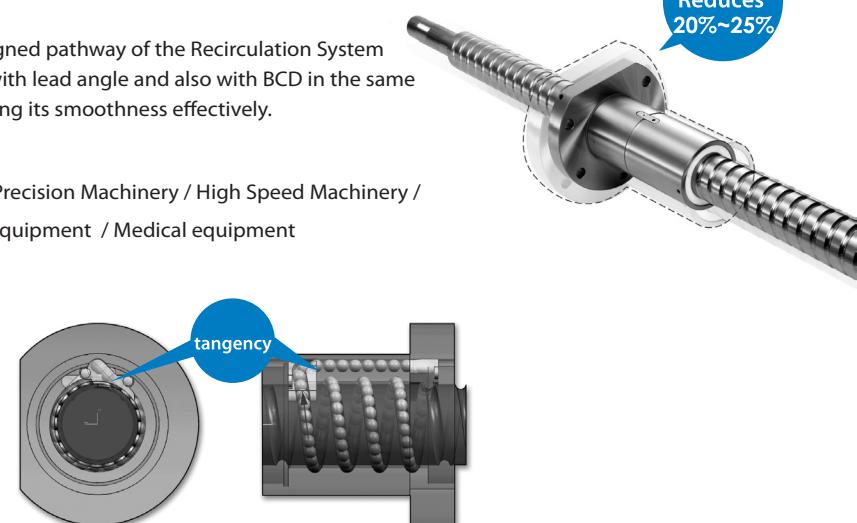
The ballnut diameter reduces 20%~25% substantially and the length of nut is shorter. The total space shall be reduced to approximately 50% consequently.

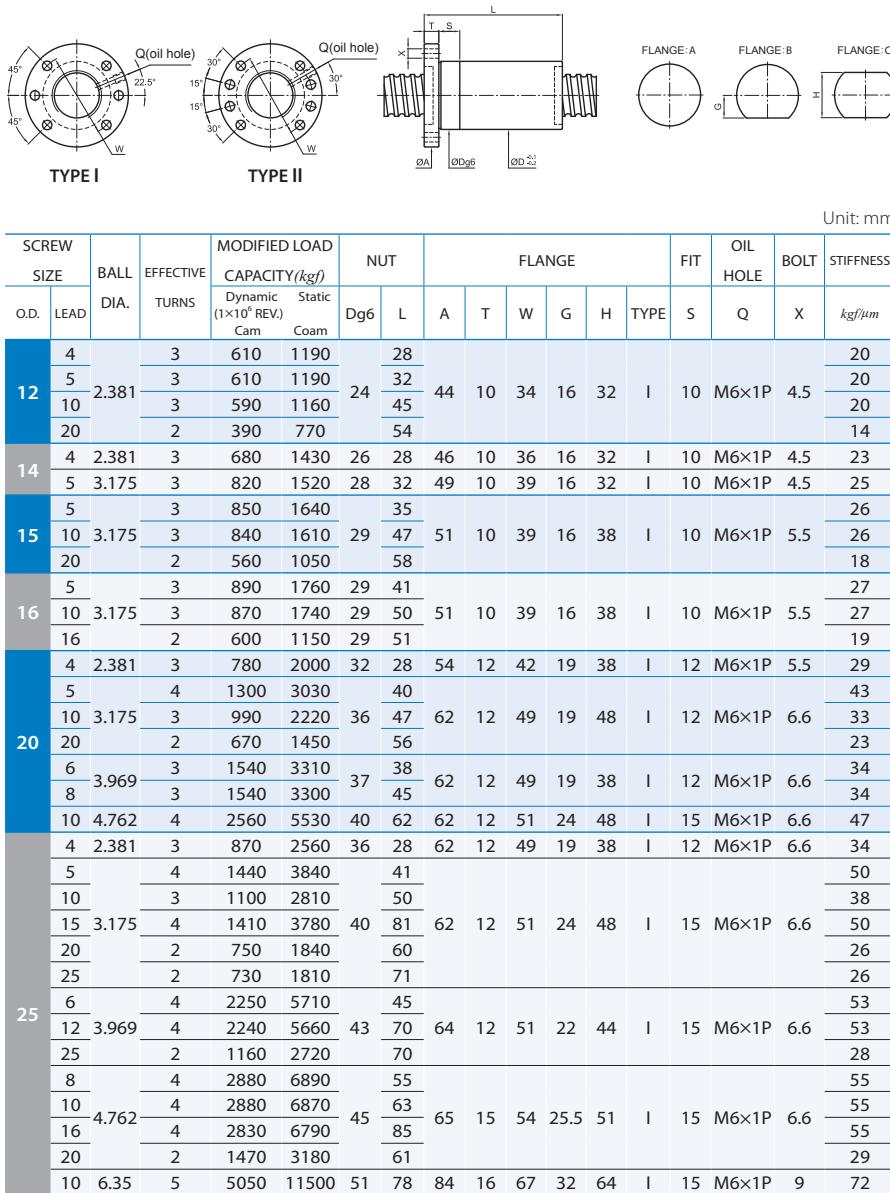
## Circulation

The specially designed pathway of the Recirculation System makes a contact with lead angle and also with BCD in the same tangency, improving its smoothness effectively.

## Applications

CNC Machinery / Precision Machinery / High Speed Machinery / Semi-Conductor Equipment / Medical equipment

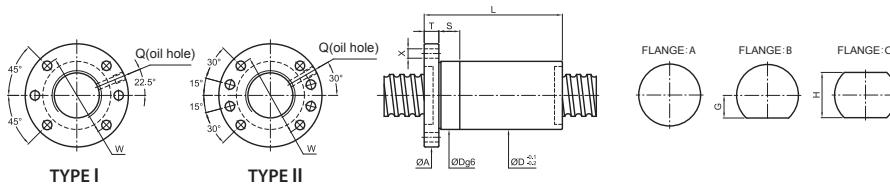




Coam and Cam are the modified static and dynamic load capacities, calculated according to ISO-3408-5

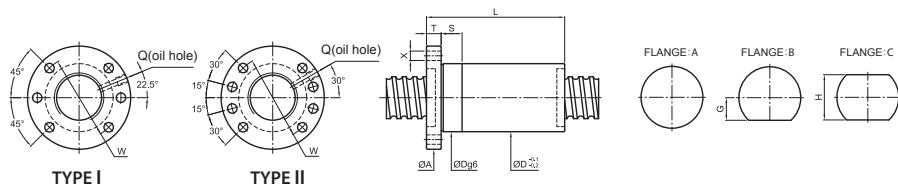
SCREW SIZE	BALL	EFFECTIVE	MODIFIED LOAD CAPACITY(kgf)		NUT		FLANGE				FIT	OIL HOLE	BOLT	STIFFNESS		
			Dynamic (1x10 <sup>6</sup> REV.)	Static Coam	Dg6	L	A	T	W	G						
			O.D.	LEAD	DIA.	TURNs										
5	3.175	5	1850	5460	43	48	65	12	51	24	48	I	15	M8×1P	6.6	67
6	3.969	5	2880	7980	46	52	66	12	50	26	52	I	15	M8×1P	6.6	70
8		3	2350	5720		46										46
10	4.762	3	2340	5710	48	52	74	12	60	30	60	I	15	M8×1P	6.6	46
16		5	3680	9690		102										73
10		5	5280	12530	78	54	87	16	72	34.5	69	I	15	M8×1P	9	77
12	6.35	5	5270	12500	88	87	16	72	34.5	69	I	15	M8×1P	9	77	
5	3.175	4	1610	4970	50	41	87	16	72	34.5	69	I	15	M8×1P	9	61
6		5	3050	9140		52										77
10	3.969	4	2550	7500	53	62	87	16	72	34.5	69	I	15	M8×1P	9	63
32		2	1300	3540		84										40
8		5	3900	10930	67											80
10		5	3890	10910		77										80
12	4.762	5	3890	10890	87	116	87	16	72	34.5	69	I	15	M8×1P	9	80
15		5	3860	10850	53											80
20		2	1700	4230		70										34
32		2	1640	4120		84										34
10		5	4900	13360		78										84
12	5.556	5	4890	13340	88	107	87	16	72	34.5	69	I	15	M8×1P	9	84
16		5	4860	13280	55											79
20		3	3140	8110		87										53
10		5	5720	14490		78										85
12	6.35	5	5710	14470	88	92	87	16	72	34.5	69	I	15	M8×1P	9	85
16		4	4520	11100	57											69
20		3	3530	8340		88										54

Coam and Cam are the modified static and dynamic load capacities, calculated according to ISO-3408-5



		SCREW SIZE	BALL DIA.	EFFECTIVE TURNS	MODIFIED LOAD CAPACITY(kgf)		NUT		FLANGE				FIT	OIL HOLE	BOLT	STIFFNESS		
O.D.	LEAD				Dynamic (1x10 <sup>6</sup> REV.) Cam	Static Coam	Dg6	L	A	T	W	G	H	TYPE	S	Q	X	kgf/mm
36	6.35	8	4.762	5	4170	12580	56	63	80	11	68	34	68	I	15	M8×1P	9	86
		10		5	6050	16460												93
		12		5	6080	16430												93
		16		5	6050	16360	61	109	91	18	76	34	68	II	15	M8×1P	9	93
		20		4	4910	12890												76
		36		2	2570	6250												41
38	6.35	10		5	6260	17740												97
		12		5	6260	17410												97
		16		5	6220	17350												97
		40		3	3830	10220												71
		5	3.175	4	1760	6260	58	42	91	18	76	34	68	II	15	M8×1P	9	71
40	6.35	6	3.969	5	3420	11810	58	52	91	18	76	34	68	II	15	M8×1P	9	92
		8	4.762	4	3610	11260	60	56	91	18	76	34	68	II	15	M8×1P	9	77
		10		5	6430	18440												101
		12		5	6420	18410												101
		15		5	6380	18350												101
		16		5	6390	18330		65	103									101
		20		4	5190	14450												82
		40		2	2700	6950												43
		12	7.144	5	7530	20800												103
		16		5	7500	20730												103

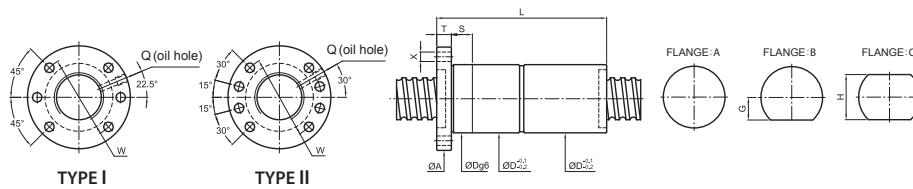
Coam and Cam are the modified static and dynamic load capacities, calculated according to ISO-3408-5



		SCREW SIZE	BALL DIA.	EFFECTIVE TURNS	MODIFIED LOAD CAPACITY(kgf)		NUT		FLANGE				FIT	OIL HOLE	BOLT	STIFFNESS			
O.D.	LEAD				Dynamic (1x10 <sup>6</sup> REV.) Cam	Static Coam	Dg6	L	A	T	W	G	H	TYPE	S	Q	X	kgf/mm	
45	7.144	8	4.762	4	3770	12580	66	55	98	18	83	37	74	II	20	M8×1P	11	84	
		10		5	6910	21330												110	
		12	6.35	5	6910	21310	70	89	105	18	88	40	80	II	20	M8×1P	11	110	
		16		5	6880	21250												110	
		12	7.144	5	7930	23300												113	
		20		4	6440	18340		73	105	18	88	40	80	II	20	M8×1P	11	91	
50	6.35	5	3.175	5	2360	9950	70	48	105	18	88	40	80	II	20	M8×1P	11	105	
		8	4.762	5	4780	17550	70	64	105	18	88	40	80	II	20	M8×1P	11	109	
		10		5	7160	23320												119	
		12	6.35	5	7150	23300		75	90	118	18	100	46	92	II	20	M8×1P	11	119
		16		5	7120	23250			109									119	
		20		3	4460	13520												74	
55	7.938	20	7.938	4	7810	22680	80	114	121	18	104	50	100	II	25	M8×1P	11	101	
		12	6.35	5	7340	25280	80	96	118	18	100	46	92	II	20	M8×1P	11	128	
		10	6.35	5	7800	29210	88	84	135	22	115	50	110	II	20	M8×1P	11	141	
		16	9.525	5	13640	43620	102	116	147	20	127	56	112	II	25	M8×1P	14	167	
		20		5	15350	56760												196	
		25	9.525	4	12530	44860	118	146	165	25	145	65	130	II	25	M8×1P	14	159	
80	3	30		3	9610	32980												121	

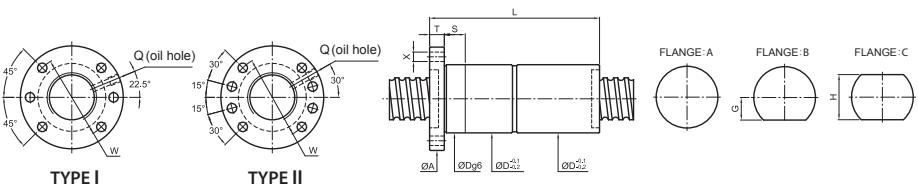
Coam and Cam are the modified static and dynamic load capacities, calculated according to ISO-3408-5

## FDDC



						MODIFIED LOAD CAPACITY(kgf)																			
SCREW SIZE	BALL	EFFECTIVE					FLANGE																		
			O.D.	LEAD	DIA.	TURNs	Dynamic (1x10 <sup>6</sup> REV.)	Static Coam	Dg6	L	A	T	W	G	H	TYPE	S	Q	X	kgf/μm					
20	4	2.381	3	780	2000	32	61	54	12	42	19	38	I	12	M6×1P	5.5	44								
	5		4	1300	3030		80													65					
	10	3.175	3	990	2220	36	97	62	12	49	19	48	I	12	M6×1P	6.6	50								
	20		2	670	1450		116													33					
	6	3.969	3	1540	3310		81	62	12	49	19	38	I	12	M6×1P	6.6	51								
	8		3	1540	3300		37	93												51					
	10	4.762	4	2560	5530	40	107	62	12	51	24	48	I	15	M6×1P	6.6	70								
25	4	2.381	3	870	2560	36	60	62	12	49	19	38	I	12	M6×1P	6.6	53								
	5		4	1440	3840		81													77					
	10		3	1100	2810		100													58					
	15	3.175	4	1410	3780	40	166	62	12	51	24	48	I	15	M6×1P	6.6	77								
	20		2	750	1840		120													39					
	25		2	730	1810		146													39					
	6		4	2250	5710		87													80					
	12	3.969	4	2240	5660	43	142	64	12	51	22	44	I	15	M6×1P	6.6	80								
	25		2	1160	2720		145													41					
	8		4	2880	6890		111													83					
	10		4	2880	6870		128	65	15	54	25.5	51	I	15	M6×1P	6.6	83								
	16	4.762	4	2830	6790	45	173													83					
	20		2	1470	3180		122													42					
	10	6.35	5	5050	11500	51	153	84	16	67	32	64	I	15	M6×1P	9	108								

Coam and Cam are the modified static and dynamic load capacities, calculated according to ISO-3408-5



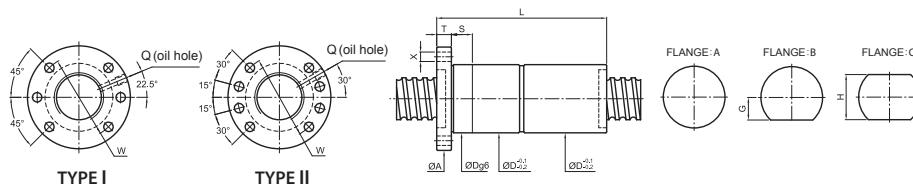
						MODIFIED LOAD CAPACITY(kgf)																				
SCREW SIZE	BALL	EFFECTIVE					FLANGE																			
			O.D.	LEAD	DIA.	TURNs	Dynamic (1x10 <sup>6</sup> REV.)	Static Coam	Dg6	L	A	T	W	G	H	TYPE	S	Q	X	kgf/μm						
28	5	3.175	5	1850	5460	44	93	65	12	51	24	48	I							M8×1P	6.6	104				
	6	3.969	5	2880	7980	46	106	66	12	50	26	52	I							M8×1P	6.6	108				
	8		3	2350	5720		94															69				
	10	4.762	3	2340	5710	48	102	74	12	60	30	60	I							15	M8×1P	6.6	69			
	16		5	3680	9690		206															112				
	10	6.35	5	5280	12530		158	87	16	72	34.5	69	I							M8×1P	9	118				
	12		5	5270	12500		172															118				
32	5	3.175	4	1610	4970	50	81	87	16	72	34.5	69	I							15	M8×1P	9	93			
	6		5	3050	9140		106															120				
	10	3.969	4	2550	7500	53	126	87	16	72	34.5	69	I							15	M8×1P	9	96			
	32		2	1300	3540		172															60				
	8		5	3900	10930		132															124				
	10		5	3890	10910		147															124				
	12	4.762	5	3890	10890		171	87	16	72	34.5	69	I							15	M8×1P	9	124			
	15		5	3860	10850		221															124				
	20		2	1700	4230		140															51				
	32		2	1640	4120		186															51				
	10		5	4900	13360		153															129				
	12	5.556	5	4890	13340		172	87	16	72	34.5	69	I							15	M8×1P	9	129			
	16		5	4860	13280		211															121				
	20		3	3140	8110		177															79				
	10		5	5720	14490		153															131				
	12	6.35	5	5710	14470		172	87	16	72	34.5	69	I							15	M8×1P	9	131			
	16		4	4520	11100		180															105				
	20		3	3530	8340		178															80				

Coam and Cam are the modified static and dynamic load capacities, calculated according to ISO-3408-5

## FDDC

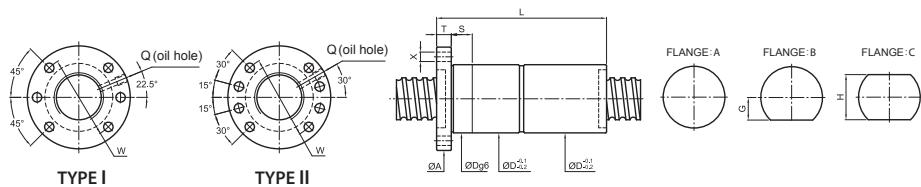
Product  
BALLSCREWS  
Specifications | End Deflector Series

## FDDC



		SCREW SIZE	BALL	EFFECTIVE TURNS	MODIFIED LOAD CAPACITY(kgf)		NUT		FLANGE				FIT	OIL HOLE	BOLT	STIFFNESS	
O.D.	LEAD				Dynamic ( $1 \times 10^6$ REV.)	Static Coam	Dg6	L	A	T	W	G	H	TYPE	S	Q	X
36	8	4.762	5	4170	12580	56	127	80	11	68	34	68	II	15	M8×1P	9	133
	10		5	6050	16460		153										142
	12		5	6080	16430		172										142
	16	6.35	5	6050	16360	61	213	91	18	76	34	68	II	15	M8×1P	9	142
	20		4	4910	12890		217										115
	36		2	2570	6250		194										59
38	10		5	6260	17740		155										149
	12		5	6260	17410	63	172	93	18	78	35	70	II	20	M8×1P	9	149
	16		5	6220	17350		213										149
	40		3	3830	10220		282										106
40	5	3.175	4	1760	6260	60	87	91	18	76	34	68	II	15	M8×1P	9	111
	6	3.969	5	3420	11810	60	108	91	18	76	34	68	II	15	M8×1P	9	142
	8	4.762	4	3610	11260	62	118	91	18	76	34	68	II	15	M8×1P	9	118
	10		5	6430	18440		158										155
	12		5	6420	18410		172	95	18	80	36	72	II	20	M8×1P	9	155
	15		5	6380	18350	68	226										155
	16		5	6390	18330		212										155
	20		4	5190	14450		220	98	18	83	37	74	II	20	M8×1P	11	125
	40		2	2700	6950		210										64
	12	7.144	5	7530	20800	70	174	98	18	83	37	74	II	20	M8×1P	11	158
	16		5	7500	20730		212										158

Coam and Cam are the modified static and dynamic load capacities, calculated according to ISO-3408-5



		SCREW SIZE	BALL	EFFECTIVE TURNS	MODIFIED LOAD CAPACITY(kgf)		NUT		FLANGE				FIT	OIL HOLE	BOLT	STIFFNESS	
O.D.	LEAD				Dynamic ( $1 \times 10^6$ REV.)	Static Coam	Dg6	L	A	T	W	G	H	TYPE	S	Q	X
45	8	4.762	4	3770	12580	66	114	98	18	83	37	74	II	20	M8×1P	11	130
	10		5	6910	21330		158										170
	12	6.35	5	6910	21310	70	171	105	18	88	40	80	II	20	M8×1P	11	170
	16		5	6880	21250		215										170
	12	7.144	5	7930	23300	73	168	105	18	88	40	80	II	20	M8×1P	11	173
	20		4	6440	18340		220										139
50	5	3.175	5	2360	9950	70	98	105	18	88	40	80	II	20	M8×1P	11	164
	8	4.762	5	4780	17550	70	128	105	18	88	40	80	II	20	M8×1P	11	169
	10		5	7160	23320		158										185
	12	6.35	5	7150	23300	75	174	118	18	100	46	92	II	20	M8×1P	11	185
55	16		5	7120	23250		215										185
	20		3	4460	13520	75	185	118	18	100	46	92	II	20	M8×1P	11	112
	20	7.938	4	7810	22680	80	220	121	18	104	46	92	II	20	M8×1P	11	154
	12	6.35	5	7340	25280	80	174	118	18	100	46	92	II	20	M8×1P	11	198
63	10	6.35	5	7800	29210	88	164	135	22	115	50	100	II	20	M8×1P	14	220
	16	9.525	5	13640	43620	102	228	147	20	127	56	112	II	25			257
	20		5	15350	56760		283										305
80	25	9.525	4	12530	44860	118	296	165	25	145	65	130	II	25	M8×1P	14	245
	30		3	9610	32980		254										185

Coam and Cam are the modified static and dynamic load capacities, calculated according to ISO-3408-5

PMI Precision Ground BallScrew

### 13.3 External Ball Circulation Nuts

#### Features:

- Lower noise due to longer ball circulation paths.
- Offers smoother ball circulation.
- Offers better solution and quality for high lead or large diameter ballscrews.

#### Type:

There are two types of Ballnut of the external circulation Ballscrews. They are "immersion type" of Fig.13.2 and "extrusive type" of Fig.13.3. The "immersion type" means the ball circulation tubes are inside the circular surface of Ballnut as shown on specifications of this catalogue are of "immersion type".

In some cases, as per designs on customer's drawings, there are smaller outer diameters ballnuts required. Then the ball circulation tubes shall extrude out of Ballnut circular surface.

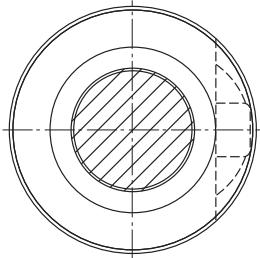


Fig.13.2 Immersion type

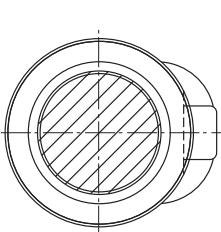
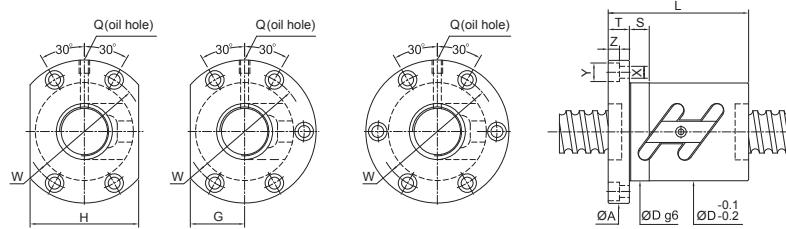
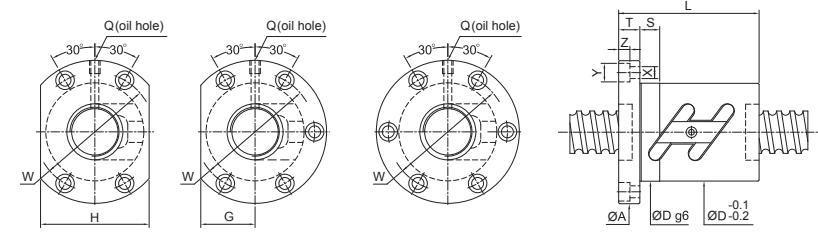


Fig.13.3 Extrusive type

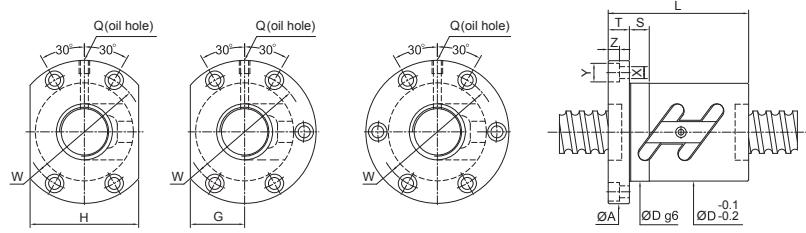


SCREW SIZE		BALL DIA.	EFFECTIVE TURNS circuit x row	BASIC RATE LOAD(kgf)		NUT		FLANGE				FIT	BOLT			OIL HOLE	STIFFNESS	Unit: mm
O.D.	LEAD			Dynamic (1x10 <sup>6</sup> REV.) C <sub>a</sub>	Static C <sub>o</sub>	Dg6	L	A	T	W	G	H	S	X	Y	Z	Q	kgf/ $\mu$ m
10	3	2.000	2.5x1	250	430	37												9
	4	2.000	2.5x1	250	430	26	40	46	10	36	14	28	10	4.5	8	4.5	M6x1P	9
	5	2.000	2.5x1	250	430	42												9
12	4	2.381	2.5x1	380	640	30	40	50	10	40	16	32	10	4.5	8	4.5	M6x1P	12
	5	2.381	2.5x1	380	640	42												12
14	4	2.381	2.5x1	410	750	34	40	57	11	45	17	34	10	4.5	9.5	5.5	M6x1P	14
	5	3.175	2.5x1	675	1145	42												15
	4	2.381	2.5x1	420	800	40												14
15	5	3.175	2.5x1	680	1210	34	42	57	10	45	17	34	10	5.5	9.5	5.5	M6x1P	15
	10	3.175	2.5x1	680	1210	55												16
			1.5x2	490	1010	44												18
16	4	2.381	2.5x1	430	850	34	41	57	11	45	17	34	10	5.5	9.5	5.5	M6x1P	15
			3.5x1	560	1180	42												21
			1.5x2	805	1525	45												19
20	5	3.175	2.5x1	690	1270	40	41	63	11	51	21	42	15	5.5	9.5	5.5	M6x1P	16
			2.5x2	1250	2540	56												31
			3.5x1	920	1780	46												22
			1.5x2	805	1525	52												19
20	6	3.175	2.5x1	690	1270	40	44	63	11	51	21	42	15	5.5	9.5	5.5	M6x1P	16
			3.5x1	920	1780	52												22
	10	3.175	2.5x1	690	1270	40	56	63	11	51	21	42	15	5.5	9.5	5.5	M6x1P	16
20			1.5x2	530	1270	44												21
	4	2.381	2.5x1	480	1060	40	40	63.5	11	51	21	42	15	5.5	9.5	5.5	M6x1P	18
			2.5x2	820	2120	50												35
			3.5x1	600	1480	43												25
20			1.5x2	965	2070	45												24
	5	3.175	2.5x1	830	1730	44	42	67	11	55	26	52	10	5.5	9.5	5.5	M6x1P	20
			2.5x2	1510	3460	56												39
			3.5x1	1110	2420	46												26
20			1.5x2	1285	2545	56												24
	6	3.969	2.5x1	1100	2120	48	49	71	11	59	27	54	10	5.5	9.5	5.5	M6x1P	20
			3.5x1	1470	2970	56												28
20			1.5x2	1285	2545	61												24
	8	3.969	2.5x1	1100	2120	48	54	75	13	61	27	54	15	6.6	11	6.5	M6x1P	20
20			3.5x1	1470	2970	62												28



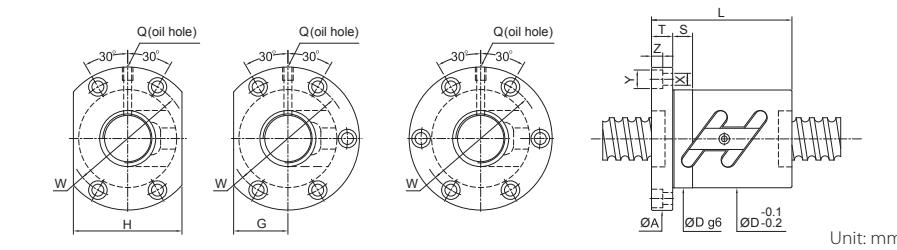
Unit: mm

SCREW SIZE	BALL DIA.	EFFECTIVE TURNS circuit x row	BASIC RATE LOAD(kgf)		NUT		FLANGE				FIT		BOLT		OIL HOLE	STIFFNESS	
			Dynamic (1×10 <sup>6</sup> REV.) Ca	Static Co	Dg6	L	A	T	W	G	H	S	X	Y	Z	Q	kgf/μm
25	4 2.381	1.5×2	600	1630	44											26	
		2.5×1	510	1355	46	40	69	11	57	26	52	15	5.5	9.5	5.5	M6×1P	22
		2.5×2	930	2710	49	49											42
		3.5×1	680	1900	42												30
	5 3.175	1.5×2	1065	2575	45												28
		2.5×1	910	2150	50	41	73	11	61	28	56	15	5.5	9.5	5.5	M6×1P	24
		2.5×2	1650	4300	56	56											46
		3.5×1	1210	3010	46												33
	6 3.969	1.5×2	1420	3215	56												29
		2.5×1	1210	2680	53	49	76	11	64	29	58	15	5.5	9.5	5.5	M6×1P	24
		2.5×2	2190	5360	62	62											47
		3.5×1	1610	3750	56												34
	8 4.762	1.5×2	1820	3840	61												30
		2.5×1	1560	3200	58	61	85	13	71	32	64	15	6.6	11	6.5	M6×1P	25
		3.5×1	2080	4480	66												35
		1.5×2	1820	3840	71												30
	10 4.762	2.5×1	1560	3200	58	65	85	15	71	32	64	15	6.6	11	6.5	M6×1P	25
		3.5×1	2080	4480	75												35
		2.5×1	1210	2680	53	60	76	11	64	32	64	15	5.5	9.5	5.5	M6×1P	24
		3.5×1	1110	2960	46												31
	5 3.175	1.5×2	950	2470	55	42	83	12	69	31	62	15	6.6	11	6.5	M8×1P	26
		2.5×2	1720	4940	56	56											50
		3.5×1	1270	3460	47												36
		1.5×2	1480	3605	57												32
28	6 3.969	2.5×1	1270	3000	55	50	83	12	69	31	62	15	6.6	11	6.5	M8×1P	26
		2.5×2	2300	6000	63	63											51
		3.5×1	1690	4200	57												37
		1.5×2	1935	4325	65												33
	8 4.762	2.5×1	1650	3600	60	63	93	15	76	36	72	15	9	14	8.5	M8×1P	28
		3.5×1	2200	5040	68												38
	10 4.762	1.5×2	1935	4325	74												33
		2.5×1	1650	3600	60	67	93	15	76	36	72	15	9	14	8.5	M8×1P	28
		3.5×1	2200	5040	77												38



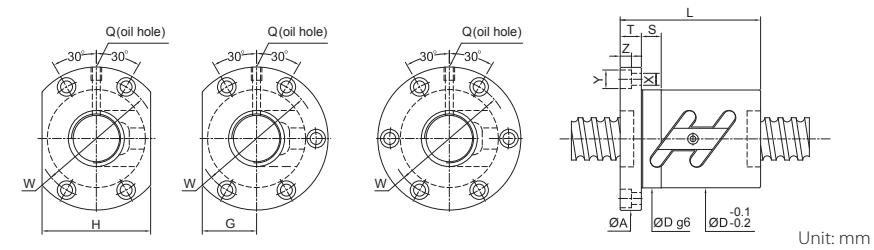
Unit: mm

SCREW SIZE	BALL DIA.	EFFECTIVE TURNS circuit x row	BASIC RATE LOAD(kgf)		NUT		FLANGE				FIT		BOLT		OIL HOLE	STIFFNESS		
			Dynamic (1×10 <sup>6</sup> REV.) Ca	Static Co	Dg6	L	A	T	W	G	H	S	X	Y	Z	Q	kgf/μm	
32	4 2.381	1.5×2	565	1750	54	40	81	12	67	32	64	15	6.6	11	6.5	M6×1P	26	
		2.5×2	1020	3500	50	50											50	
		1.5×2	1180	3410	47												34	
		2.5×1	1010	2840	43												29	
	5 3.175	2.5×2	1830	5680	58	57	85	12	71	32	64	15	6.6	11	6.5	M8×1P	56	
		2.5×3	2590	8520	72												82	
		3.5×1	1350	3980	47												40	
		1.5×2	1560	4135	57												35	
	6 3.969	2.5×1	1330	3450	62	45	88	12	75	34	68	15	6.6	11	6.5	M8×1P	29	
		2.5×2	2410	6900	63	63											57	
		3.5×1	1770	4830	57												40	
		1.5×2	2010	5010	64												36	
	8 4.762	2.5×1	1720	4180	66	63	80	98	15	82	38	76	15	9	14	8.5	M8×1P	30
		2.5×2	3120	8360	74	74											59	
		3.5×1	2300	5850	68												42	
		1.5×2	3000	6530	78												38	
	10 6.35	2.5×1	2570	5440	74	68	108	15	90	41	82	15	9	14	8.5	M8×1P	32	
		2.5×2	4660	10880	97	97											61	
		3.5×1	3430	7620	78												44	
		1.5×2	3000	6530	88												38	
	12 6.35	2.5×1	2570	5440	74	77	108	18	90	41	82	15	9	14	8.5	M8×1P	32	
		2.5×2	4660	10880	110	110											62	
		3.5×1	3430	7620	91												44	
36	5 3.175	1.5×2	1240	3850	50												38	
		2.5×2	1920	6420	65	60											62	
		2.5×3	2720	9630	75	75											90	
		3.5×1	1410	4490	50												44	
	6 3.969	2.5×2	2600	7900	66	66											63	
		2.5×3	3680	11850	84	84	98	15	82	38	76	15	9	14	8.5	M8×1P	93	
	10 6.35	1.5×2	3180	7410	81												41	
		2.5×1	2720	6180	75	71	118	18	98	45	90	15	11	17.5	11	M8×1P	35	
		2.5×2	4930	12360	103	103											68	
	12 6.35	3.5×1	3630	8650	81												48	
		2.5×1	2720	6180	77												35	
		2.5×2	4930	12360	75	77	110	118	18	98	45	90	15	11	17.5	11	M8×1P	68
		3.5×1	3630	8650	91												48	



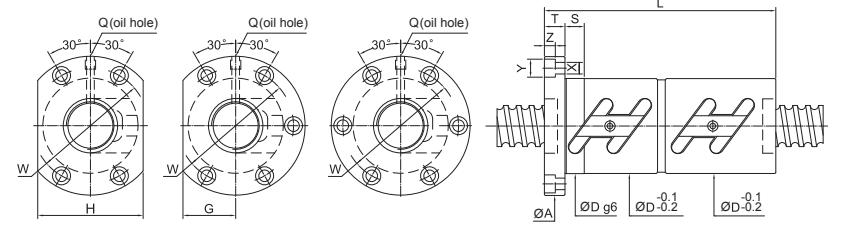
Unit: mm

SCREW SIZE	BALL DIA.	EFFECTIVE TURNS circuit x row	BASIC RATE LOAD(kgf)		NUT		FLANGE			FIT		BOLT			OIL HOLE	STIFFNESS	
			Dynamic (1x10 <sup>6</sup> REV.) Ca	Static Co	Dg6	L	A	T	W	G	H	S	X	Y	Z	Q	kgf/μm
40	5 3.175	1.5x2	1280	4275	50												41
		2.5x1	1090	3560	48												34
		2.5x2	1980	7120	67	60	101	15	83	39	78	15	9	14	8.5	M8×1P	66
		2.5x3	2800	10680		75											98
		3.5x1	1450	4980		50											47
	6 3.969	1.5x2	1750	5300	60												42
		2.5x1	1500	4420	53												35
		2.5x2	2720	8840	70	66	104	15	86	40	80	15	9	14	8.5	PT1/8"	69
		2.5x3	3850	13260		84											101
		3.5x1	2000	6190		60											49
	8 4.762	1.5x2	2220	6320	64												43
		2.5x1	1900	5270	74	63											36
		2.5x2	3450	10540	83	108	15	90	41	82	15	9	14	8.5	PT1/8"	70	
		3.5x1	2540	7380		68											50
		1.5x2	3370	8335	81												45
45	10 6.35	2.5x1	2880	6950	82	71	124	18	102	47	94	20	11	17.5	11	PT1/8"	35
		2.5x2	5220	13900	103	103											74
		3.5x1	3840	9730		81											52
	12 6.35	2.5x1	2880	6950	77												38
		2.5x2	5220	13900	86	112	128	18	106	48	96	20	11	17.5	11	PT1/8"	74
	3.5x1	3840	9730		91												52
55	10 6.35	2.5x2	5480	15700	88	101	132	18	110	50	100	20	11	17.5	11	PT1/8"	81
		2.5x3	7760	23550	131												119
	12 7.144	2.5x1	3550	8950	84												43
		2.5x2	6440	17900	90	112	132	18	110	50	100	20	11	17.5	11	PT1/8"	82
		2.5x3	9120	26850		148											121



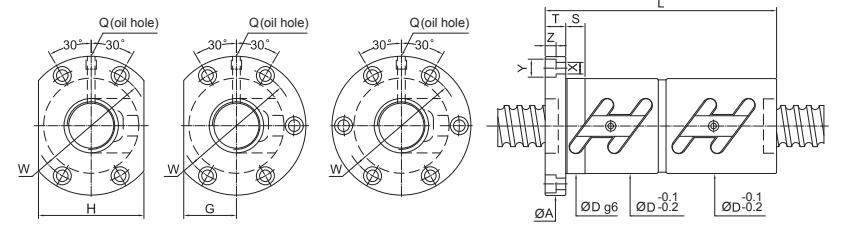
Unit: mm

SCREW SIZE	BALL DIA.	EFFECTIVE TURNS circuit x row	BASIC RATE LOAD(kgf)		NUT		FLANGE			FIT		BOLT			OIL HOLE	STIFFNESS	
			Dynamic (1x10 <sup>6</sup> REV.) Ca	Static Co	Dg6	L	A	T	W	G	H	S	X	Y	Z	Q	kgf/μm
63	10 6.35	1.5x2	1410	5305	50												49
		1.5x3	2000	7960	80	60	114	15	96	43	86	15	9	14	8.5	PT1/8"	72
		2.5x2	2190	8840		60											80
		3.5x1	1610	6190		50											57
		1.5x2	1920	6600		60											50
	6 3.969	2.5x2	2980	11000	84	67											82
		2.5x3	4220	16500	85	118	15	100	45	90	15	9	14	8.5	PT1/8"	121	
	8 4.762	3.5x1	2190	7700		60											58
		1.5x2	2515	7810		68											52
		2.5x2	3900	13020	87	86	128	18	107	49	98	20	11	17.5	11	PT1/8"	85
80	10 6.35	2.5x3	5520	19530	109	109	128	18	113	51	102	20	11	17.5	11	PT1/8"	125
		3.5x1	2870	9110		71											60
		1.5x2	3725	10450		81											54
		2.5x1	3190	8710		71											45
		2.5x2	5790	17420	93	101	135	18	113	51	102	20	11	17.5	11	PT1/8"	88
	12 7.144	2.5x3	8200	26130		131											130
		3.5x1	4260	12190		81											63
	12 7.938	2.5x1	3700	10050	100	88											46
		2.5x2	6710	20100	116	146	22	122	55	110	20	14	20	13	PT1/8"	89	
		2.5x3	12250	41340		160											167
45	10 6.35	2.5x2	7130	28500	130	105											95
		2.5x3	10100	42750	134	176	22	152	66	132	20	14	20	13	PT1/8"	140	
	12 7.938	2.5x1	3510	11200		75											55
		2.5x2	6370	22400	108	105	154	22	130	58	116	20	14	20	13	PT1/8"	106
		2.5x3	9020	33600		135											156
80	12 7.938	2.5x1	4770	13780		88											59
		2.5x2	8650	27560	115	124	161	22	137	61	122	20	14	20	13	PT1/8"	113
	16 9.525	2.5x3	12250	41340		160											167
		2.5x2	7130	28500	130	105											129
		2.5x3	10100	42750	134	176	22	152	66	132	20	14	20	13	PT1/8"	190	
120	12 7.938	2.5x2	9710	35560	136	124											137
		2.5x3	13760	53340	160	182	22	158	68	136	20	14	20	13	PT1/8"	202	
	16 9.525	2.5x2	16450	59280	143	160											170
160	16 9.525	2.5x3	23300	88920	208	204	28	172	77	154	30	18	26	17.5	PT1/8"	250	



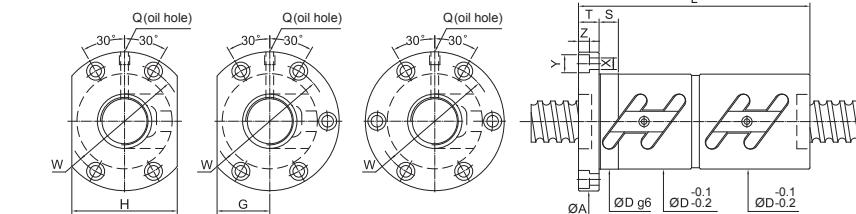
Unit: mm

SCREW SIZE	BALL	EFFECTIVE TURNS circuit x row	BASIC RATE LOAD(kgf)		NUT		FLANGE			FIT		BOLT		OIL HOLE	STIFFNESS	
			Dynamic (1x10 <sup>6</sup> REV.) Ca	Static Co	Dg6	L	A	T	W	G	H	S	X	Y	Z	kgf/μm
16	4 2.381	1.5x2	490	1010	81											36
		2.5x1	430	850	34	70	57	11	45	17	34	15	5.5	9.5	5.5 M6x1P	30
		3.5x1	560	1180		78										42
	5 3.175	1.5x2	805	1525	90											39
		2.5x1	690	1270	40	77	63	11	51	20	40	15	5.5	9.5	5.5 M6x1P	33
		2.5x2	1250	2540	105											63
		3.5x1	920	1780		88										45
	6 3.175	1.5x2	805	1525	90											39
		2.5x1	690	1270	40	80	63	11	51	20	40	15	5.5	9.5	5.5 M6x1P	33
		3.5x1	920	1780		90										45
	4 2.381	1.5x2	530	1270	83											42
		2.5x1	480	1060	40	67	63	11	51	24	48	15	5.5	9.5	5.5 M6x1P	36
		2.5x2	820	2120	40	89										69
		3.5x1	600	1480		75										49
20	5 3.175	1.5x2	965	2070	99											47
		2.5x1	830	1730	44	76	67	11	55	26	52	15	5.5	9.5	5.5 M6x1P	40
		2.5x2	1510	3460	105											77
		3.5x1	1110	2420		80										55
	6 3.969	1.5x2	1285	2545	98											49
		2.5x1	1100	2120	48	82	71	11	59	27	54	15	5.5	9.5	5.5 M6x1P	41
		3.5x1	1470	2970		93										45
28	8 3.969	1.5x2	1285	2545	108											49
		2.5x2	1100	2120	48	102	75	13	61	28	56	15	6.6	11	6.5 M6x1P	41
		3.5x1	1470	2970		110										56



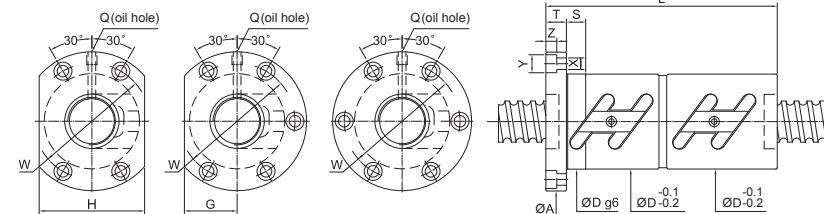
Unit: mm

SCREW SIZE	BALL	EFFECTIVE TURNS circuit x row	BASIC RATE LOAD(kgf)		NUT		FLANGE			FIT		BOLT		OIL HOLE	STIFFNESS	
			Dynamic (1x10 <sup>6</sup> REV.) Ca	Static Co	Dg6	L	A	T	W	G	H	S	X	Y	Z	kgf/μm
25	4 2.381	1.5x2	600	1630	83											51
		2.5x1	510	1355	46	67	69	11	57	26	52	15	5.5	9.5	5.5 M6x1P	43
		2.5x2	930	2710		91										84
	5 3.175	3.5x1	680	1900		75										59
		1.5x2	1065	2575		80										57
		2.5x1	910	2150	50	77	73	11	61	28	56	15	5.5	9.5	5.5 M6x1P	48
	6 3.969	2.5x2	1650	4300		105										92
		3.5x1	1210	3010		86										65
		1.5x2	1420	3215		91										58
	8 4.762	2.5x1	1210	2680	53	82	76	11	64	29	58	15	5.5	9.5	5.5 M6x1P	49
		2.5x2	2190	5360		116										94
		3.5x1	1610	3750		93										67
28	10 4.762	1.5x2	1820	3840	111											60
		2.5x1	1560	3200	58	95	85	13	71	32	64	15	6.6	11	6.5 M6x1P	50
		3.5x1	2080	4480		111										69
	5 3.175	1.5x2	1820	3840	134											60
		2.5x1	1560	3200	58	117	85	15	71	32	64	15	6.6	11	6.5 M6x1P	50
30	8 4.762	3.5x1	2080	4480	138											69
		1.5x2	1110	2960		86										62
		2.5x1	950	2470	55	78	83	12	69	31	62	15	6.6	11	6.5 M8x1P	52
	6 3.969	2.5x2	1720	4940		106										101
		3.5x1	1270	3460		86										72
32	8 4.762	1.5x2	1480	3605	98											63
		2.5x1	1270	3000	55	89	83	12	69	31	62	15	6.6	11	6.5 M8x1P	53
		2.5x2	2300	6000		117										103
	10 4.762	3.5x1	1690	4200	94											73
		1.5x2	1935	4325	113											66
34	8 4.762	2.5x1	1650	3600	60	97	93	15	76	36	72	15	9	14	8.5 M8x1P	55
		3.5x1	2200	5040		113										76
	10 4.762	1.5x2	1935	4325	134											66
36	2.5x1	1635	3600	60	117	93	15	76	36	72	15	9	14	8.5 M8x1P	55	
	3.5x1	2200	5040		138											76



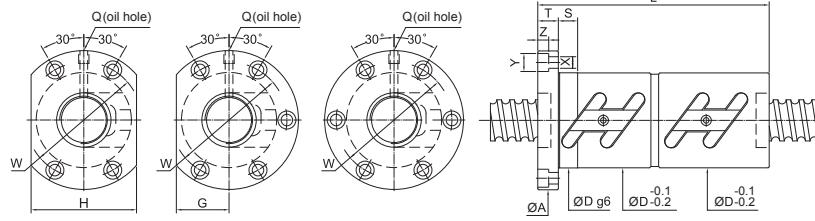
Unit: mm

SCREW SIZE	BALL DIA.	EFFECTIVE TURNS circuit x row	BASIC RATE LOAD(kgf)		NUT		FLANGE				FIT		BOLT			OIL HOLE	STIFFNESS
			Dynamic (1×10 <sup>6</sup> REV.) Ca	Static Co	Dg6	L	A	T	W	G	H	S	X	Y	Z	Q	kgf/mm
32	4 2.381	2.5x1	565	1750	54	68	81	12	67	32	64	15	6.6	11	6.5	M6×1P	52 101
		2.5x2	1020	3500	90												
	5 3.175	1.5x2	1180	3410		82											69
		2.5x1	1010	2840		78											58
	6 3.969	2.5x2	1830	5680	58	105	85	12	71	32	64	15	6.6	11	6.5	M8×1P	112 164 80
		2.5x3	2590	8520													1350 3980
	8 4.762	3.5x1	1350	3980													82
		1.5x2	1560	4135		100											70
	10 6.35	2.5x1	1330	3450	62	87	88	12	75	34	68	15	6.6	11	6.5	M8×1P	59 114 81
		2.5x2	2410	6900		123											100
36	5 3.175	2.5x1	1720	4180	66	106	98	15	82	38	76	15	9	14	8.5	M8×1P	76 64 123 88
		2.5x2	3120	8360		152											113
	6 3.969	3.5x1	2300	5850													5850
		1.5x2	3000	6530		138											76
	8 4.762	2.5x1	2570	5440	74	118	108	15	90	41	82	15	9	14	8.5	M8×1P	76 64 123 88
		2.5x2	4660	10880		177											148
	10 6.35	3.5x1	3430	7620													7620
		1.5x2	3000	6530		160											76
	12 6.35	2.5x1	2570	5440	74	137	108	18	90	41	82	15	9	14	8.5	M8×1P	76 64 124 88
		2.5x2	4660	10880		208											160
38	5 3.175	1.5x2	1240	3850		91											75
		2.5x2	1920	6420	65	110	98	15	82	38	76	15	9	14	8.5	M8×1P	123 181 87
	6 3.969	2.5x3	2720	9630		139											90
		3.5x1	1410	4490													90
	8 4.762	2.5x2	2600	7900	65	123	98	15	82	38	76	15	9	14	8.5	M8×1P	126 187
		2.5x3	3680	11850		159											151
	10 6.35	2.5x2	3265	9450	70	153	114	18	92	46	92	20	11	17.5	11	M8×1P	129
		2.5x1	3180	7410													141
	12 6.35	2.5x2	2720	6180	75	131	118	18	98	45	90	15	11	17.5	11	M8×1P	83 70 136 96
		3.5x1	3630	8650													151



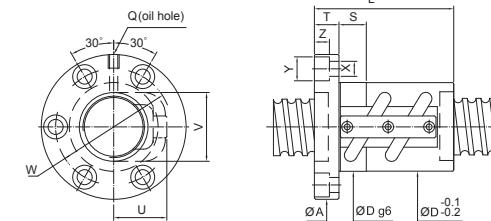
Unit: mm

SCREW SIZE	BALL DIA.	EFFECTIVE TURNS circuit x row	BASIC RATE LOAD(kgf)		NUT		FLANGE				FIT		BOLT			OIL HOLE	STIFFNESS
			Dynamic (1×10 <sup>6</sup> REV.) Ca	Static Co	Dg6	L	A	T	W	G	H	S	X	Y	Z	Q	kgf/mm
40	5 3.175	1.5x2	1280	4275		88											82
		2.5x1	1090	3560		84											69
	6 3.969	2.5x2	1980	7120	67	108	101	15	83	39	78	15	9	14	8.5	M8×1P	133
		2.5x3	2800	10680		139											196
	8 4.762	3.5x1	1450	4980													95
		1.5x2	1750	5300		103											85
	10 6.35	2.5x1	1500	4420		90											71
		2.5x2	2720	8840	70	123	104	15	86	40	80	15	9	14	8.5	PT1/8"	138
	12 6.35	2.5x3	3850	13260		159											202
		3.5x1	2000	6190													98
45	6 3.969	1.5x2	2220	6320		124											86
		2.5x1	1900	5270	74	108	15	90	41	82	15	9	14	8.5	PT1/8"	73	
	8 4.762	2.5x2	3450	10540		152											141
		3.5x1	2540	7380													100
	10 6.35	1.5x2	3370	8335		141											91
		2.5x1	2880	6950	82	131	124	18	102	47	94	20	11	17.5	11	PT1/8"	71
	12 6.35	2.5x2	5220	13900		180											148
		3.5x1	3840	9730													105
	12 7.144	2.5x1	2880	6950		137											76
		2.5x2	5220	13900	86	208	128	18	106	48	96	20	11	17.5	11	PT1/8"	148
	10 6.35	3.5x1	3840	9730		161											105
		1.5x2	2850	9870	80	123	114	15	96	48	96	15	9	14	8.5	PT1/8"	151
	8 4.762	2.5x3	4035	14800		159											222
		2.5x2	3650	11780	85	158	127	18	105	52	104	20	11	17.5	11	PT1/8"	155
	10 6.35	2.5x3	5175	17670		206											228
		2.5x2	5480	15700		180											163
	12 7.144	2.5x1	3550	8950	90	140	132	18	110	50	100	20	11	17.5	11	PT1/8"	239
		2.5x2	6440	17900		210											85
		3.5x1	3630	8650		161											165

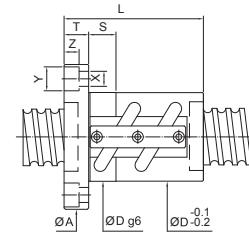
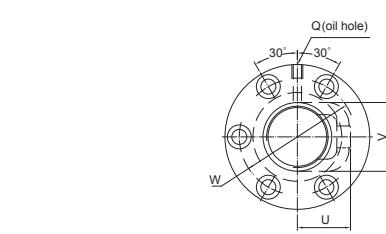


Unit: mm

SCREW SIZE	BALL DIA.	EFFECTIVE TURNS circuit x row	BASIC RATE LOAD(kgf)		NUT		FLANGE			FIT		BOLT		OIL HOLE	STIFFNESS	kgf/ $\mu$ m		
			Dynamic ( $1 \times 10^6$ REV.) Ca	Static Co	Dg6	L	A	T	W	G	H	S	X	Y	Z	Q		
50	5 3.175	1.5x2	1410	5305	80	108										98		
		1.5x3	2000	7960	113	128	114	15	96	43	86	15	9	14	8.5	PT1/8"	144	
		2.5x2	2190	8840		108										159		
		3.5x1	1610	6190												114		
	6 3.969	1.5x2	1920	6600	84	111										101		
		2.5x2	2980	11000	123	128	118	15	100	45	90	15	9	14	8.5	PT1/8"	164	
		2.5x3	4220	16500	159	118	118	15	100	45	90	15	9	14	8.5	PT1/8"	242	
		3.5x1	2190	7700		107											117	
	8 4.762	1.5x2	2515	7810	87	127										104		
		2.5x2	3900	13020	156	128	128	18	107	49	98	20	11	17.5	11	PT1/8"	170	
		2.5x3	5520	19530	208	128	118	15	107	49	98	20	11	17.5	11	PT1/8"	250	
		3.5x1	2870	9110		127											121	
	10 6.35	1.5x2	3725	10450	151											108		
		2.5x1	3190	8710	132											91		
		2.5x2	5790	17420	93	180	135	18	113	51	102	20	11	17.5	11	PT1/8"	177	
		2.5x3	8200	26130		243											261	
	12 7.144	3.5x1	4260	12190	151												126	
		2.5x1	3700	10050	100	140	146	18	122	55	110	20	14	20	13	PT1/8"	92	
		2.5x2	6710	20100	210	146	146	18	122	55	110	20	14	20	13	PT1/8"	179	
		2.5x3	10 6.35	6005	19540	102	181	144	18	122	54	108	20	11	17.5	11	PT1/8"	191
	63	2.5x3	8510	29310	243												281	
		2.5x1	3510	11200	136												110	
		2.5x2	6370	22400	108	189	154	22	130	58	116	20	14	20	13	PT1/8"	213	
		2.5x3	9020	33600		249											313	
	12 7.938	2.5x1	4760	13820	115	144	161	22	137	61	122	20	14	20	13	PT1/8"	112	
		2.5x2	8650	27560	214	144	161	22	137	61	122	20	14	20	13	PT1/8"	218	
		2.5x1	16 9.525	8050	23100	122	200	178	28	150	69	138	20	18	26	17.5	PT1/8"	144
		2.5x2	14600	46200	296												280	
	10 6.35	2.5x2	7130	28500	130	189	176	22	152	66	132	20	14	20	13	PT1/8"	258	
		2.5x3	10100	42750	249												380	
		2.5x2	12 7.938	9710	35560	136	220	182	22	158	68	136	20	14	20	13	PT1/8"	265
		2.5x3	13760	53340	292												391	
	16 9.525	2.5x2	16450	59280	143	290	204	28	172	77	154	30	18	26	17.5	PT1/8"	339	
		2.5x3	23300	88920	386												500	

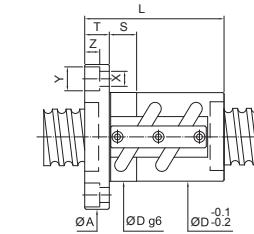
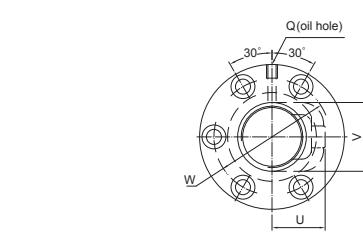


SCREW SIZE	BALL DIA.	EFFECTIVE TURNS circuit x row	BASIC RATE LOAD(kgf)		NUT		FLANGE			FIT		BOLT		RETURN TUBE	OIL HOLE	STIFFNESS	kgf/ $\mu$ m
			Dynamic ( $1 \times 10^6$ REV.) Ca	Static Co	Dg6	L	A	T	W	S	X	Y	Z	U	V	Q	
14	4 2.381	1.5x2	410	750	25	40	45	10	35	10	5.5	9.5	5.5	19	21	M6x1P	14
		2.5x1	675	1145	25	42	45	10	35	10	5.5	9.5	5.5	19	21	M6x1P	15
	5 3.175	1.5x2	420	800	28.5	40	48	10	38	10	5.5	9.5	5.5	17	22	M6x1P	14
		2.5x1	680	1210	28.5	42	48	10	38	10	5.5	9.5	5.5	17	22	M6x1P	15
15	4 2.381	1.5x2	805	1525	50												19
		2.5x1	690	1270	45												16
	5 3.175	1.5x2	1250	2540	31	60	54	12	41	15	5.5	9.5	5.5	20	23	M6x1P	31
		2.5x1	920	1780	50												22
16	5 3.175	1.5x2	965	2070	50												24
		2.5x1	830	1730	45												20
	6 3.969	1.5x2	1510	3460	35	60	58	12	46	10	5.5	9.5	5.5	22	27	M6x1P	39
		2.5x1	1110	2420	50												26
20	5 3.175	1.5x2	1285	2545	66												24
		2.5x1	1100	2120	36	48	60	12	47	10	5.5	9.5	5.5	23	28	M6x1P	20
	6 3.969	1.5x2	1470	2970	66												28
		2.5x1	1110	2960	65												29
25	6 3.969	1.5x2	1420	3215	65												24
		2.5x1	1210	2680	42	68	68	12	55	15	5.5	9.5	5.5	28	33	M6x1P	47
	5 3.175	1.5x2	2190	5360	68	60	68	12	55	15	5.5	9.5	5.5	28	33	M6x1P	34
		2.5x1	1610	3750	65												34
28	10 4.762	1.5x2	1820	3840	75												30
		2.5x1	1560	3200	45	65	72	16	58	15	6.6	11	6.5	29	34	M6x1P	25
	5 3.175	1.5x2	2080	4480	75												35
		2.5x1	1110	2960	50												31
36	6 3.969	1.5x2	1270	3460	44	60	70	12	56	15	6.6	11	6.5	28	34	M6x1P	50
		2.5x1	1270	3460	50												36
	6 3.969	1.5x2	1480	3605	55												32
		2.5x1	1270	3000	44	68	70	12	56	15	6.6	11	6.5	28	36	M6x1P	51
		2.5x2	2300	6000	68												37

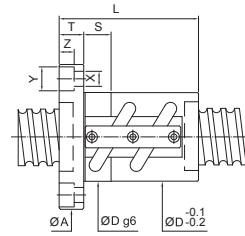
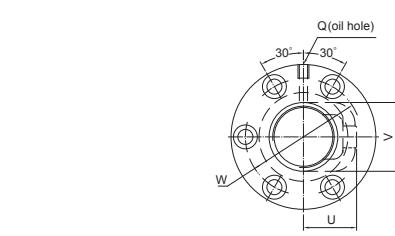


Unit: mm

SCREW SIZE		BALL DIA.	EFFECTIVE TURNS circuit x row	BASIC RATE LOAD(kgf)		NUT		FLANGE		FIT		BOLT		RETURN TUBE		OIL HOLE	STIFFNESS
O.D.	LEAD			Dynamic (1x10 <sup>6</sup> REV.) Ca	Static Co	Dg6	L	A	T	W	S	X	Y	Z	U	V	Q
32	5 3.175	1.5x2	1180	3410	50												34
		2.5x1	1010	2840	45												29
		2.5x2	1830	5680	50	60	76	12	63	15	6.6	11	6.5	30	38	M6x1P	56
		2.5x3	2590	8520	75												82
		3.5x1	1350	3980	50												40
	6 3.969	1.5x2	1560	4135	55												35
		2.5x1	1330	3450	52	50	78	12	65	15	6.6	11	6.5	32	39	M6x1P	29
		2.5x2	2410	6900	68	68											57
		3.5x1	1770	4830	55												40
	8 4.762	1.5x2	2010	5010	70												36
		2.5x1	1720	4180	54	62	88	16	70	15	9	14	8.5	33	40	M6x1P	30
		2.5x2	3120	8360	86	86											59
		3.5x1	2300	5850	70												42
	10 6.35	1.5x2	3000	6530	78												38
		2.5x1	2570	5440	57	68	91	16	73	15	9	14	8.5	37	44	M8x1P	32
		2.5x2	4660	10880	98	98											61
		3.5x1	3430	7620	78												44
36	6 3.969	2.5x1	1430	3950	55	50	82	12	68	15	6.6	11	6.5	32	42	M6x1P	33
		2.5x2	2600	7900	68	68											63
	10 6.35	1.5x2	3180	7410	82												41
		2.5x1	2720	6180	62	72	104	18	82	20	11	17.5	11	40	49	M6x1P	35
		2.5x2	4930	12360	102	102											68
	12 7.144	3.5x1	3630	8650	82												48

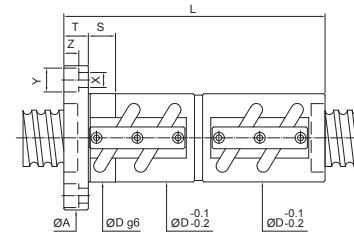
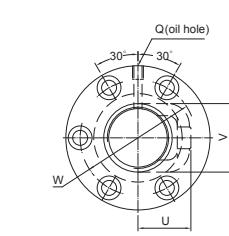


SCREW SIZE		BALL DIA.	EFFECTIVE TURNS circuit x row	BASIC RATE LOAD(kgf)		NUT		FLANGE		FIT		BOLT		RETURN TUBE		OIL HOLE	STIFFNESS
O.D.	LEAD			Dynamic (1x10 <sup>6</sup> REV.) Ca	Static Co	Dg6	L	A	T	W	S	X	Y	Z	U	V	Q
40	5 3.175	1.5x2	1280	4270	55												41
		2.5x1	1090	3560	50												34
		2.5x2	1980	7120	58	65	92	16	72	15	9	14	8.5	34	46	M8x1P	66
		2.5x3	2800	10680	80												98
		3.5x1	1450	4980	55												47
40	6 3.969	1.5x2	1750	5300	60												42
		2.5x1	1500	4420	54												35
		2.5x2	2720	8840	60	72	94	16	76	15	9	14	8.5	36	47	PT1/8"	69
		2.5x3	3850	13260	90												101
		3.5x1	2000	6190	60												49
45	8 4.762	1.5x2	2220	6320	70												43
		2.5x1	1900	5270	62	62											36
		2.5x2	3450	10540	86	86	96	16	78	15	9	14	8.5	38	48	PT1/8"	70
		3.5x1	2540	7380	70												50
		1.5x2	3370	8335	82												45
45	10 6.35	2.5x1	2880	6950	72	65	102	18	85	20	11	17.5	11	42	52	PT1/8"	74
		2.5x2	5220	13900	102												52
		3.5x1	3840	9730	82												52
		2.5x1	3020	7850	70	74	112	18	90	20	11	17.5	11	48	58	PT1/8"	42
		2.5x2	5480	15700	104												81
45	12 7.144	2.5x1	3550	8950	74	87	122	18	97	20	14	20	13	49	60	PT1/8"	43
		2.5x2	6440	17900	123												82

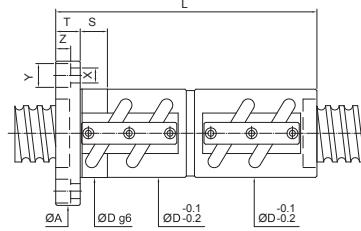
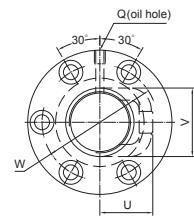


Unit: mm

SCREW SIZE	BALL	EFFECTIVE TURNS circuit x row	BASIC RATE LOAD(kgf)		NUT		FLANGE		FIT		BOLT		RETURN TUBE		OIL HOLE	STIFFNESS	
			Dynamic (1×10 <sup>6</sup> REV.) Ca	Static Co	Dg6	L	A	T	W	S	X	Y	Z	U	V	Q	kgf/μm
50	5	1.5×2	1410	5305	63											49	
		1.5×3	2000	7960	70	73	104	16	86	15	9	14	8.5	40	56	PT1/8"	72
		3.5×1	1610	6190	63											57	
	6	2.5×2	2980	11000	72	75										82	
		2.5×3	4220	16500	93	106	16	88	15	9	14	8.5	43	57	PT1/8"	121	
	8	2.5×2	3900	13020	75	88										85	
		2.5×3	5520	19530	112	116	18	95	20	11	17.5	11	45	59	PT1/8"	125	
	10	1.5×2	3725	10450	84											54	
		2.5×1	3190	8710	74											45	
		2.5×2	5790	17420	78	104	119	18	98	20	11	17.5	11	48	62	PT1/8"	88
		2.5×3	8200	26130	134											130	
		3.5×1	4260	12190	84											63	
55	12	2.5×1	3700	10050	82	87										46	
		2.5×2	6710	20100	123	128	22	105	20	14	20	13	52	64	PT1/8"	89	
	10	2.5×2	6005	19540	84	100										95	
		2.5×3	8150	29310	130	125	18	103	20	11	17.5	11	54	68	PT1/8"	140	
		2.5×1	3510	11200	77											55	
63	10	2.5×2	6370	22400	90	107	132	20	110	20	11	17.5	11	53	74	PT1/8"	106
		2.5×3	9020	33600	137											156	
		2.5×1	4770	13780	88											59	
	12	2.5×2	8650	27560	94	124	142	22	117	20	14	20	13	57	76	PT1/8"	113
		2.5×3	12250	41340	160											167	
80	16	2.5×1	8050	23100	100	105										72	
		2.5×2	14600	46200	153	150	22	123	20	14	20	13	62	78	PT1/8"	140	
	10	2.5×2	7130	28500	115	109	163	22	137	20	14	20	13	64	91	PT1/8"	129
		2.5×3	10100	42750	139											190	
		2.5×2	9710	35560	120	125										137	
12	12	2.5×3	13760	53340	159	169	22	143	25	14	20	13	67	93	PT1/8"	202	
		2.5×2	16450	59280	125	156	190	28	154	25	18	26	17.5	70	94	PT1/8"	170
	16	2.5×3	23300	88920	204											250	

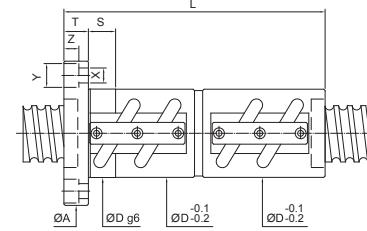
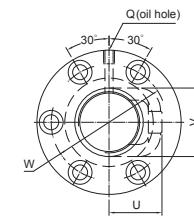


SCREW SIZE	BALL	EFFECTIVE TURNS circuit x row	BASIC RATE LOAD(kgf)		NUT		FLANGE		FIT		BOLT		RETURN TUBE		OIL HOLE	STIFFNESS	
			Dynamic (1×10 <sup>6</sup> REV.) Ca	Static Co	Dg6	L	A	T	W	S	X	Y	Z	U	V	Q	kgf/μm
16	5	1.5×2	805	1525	90											39	
		2.5×1	690	1270	31	80	54	12	41	15	5.5	9.5	5.5	20	23	M6×1P	33
		2.5×2	1250	2540	110	90										63	
		3.5×1	920	1780												45	
	5	1.5×2	965	2070	90											47	
		2.5×1	830	1730	35	80	58	12	46	10	5.5	9.5	5.5	22	27	M6×1P	40
		2.5×2	1510	3460	110	90										77	
	20	3.5×1	1110	2420	90											55	
		1.5×2	1285	2545	104											49	
		2.5×1	1100	2120	36	92	60	12	47	10	5.5	9.5	5.5	23	28	M6×1P	41
25	5	3.5×1	1470	2970	104											56	
		1.5×2	1065	2575	90											57	
		2.5×1	910	2150	40	80	64	12	52	15	5.5	9.5	5.5	26	31	M6×1P	48
		2.5×2	1650	4300	110	90										92	
	3.5×1	1210	3010													65	
28	6	1.5×2	1420	3215	104											58	
		2.5×1	1210	2680	42	92	68	12	55	15	5.5	9.5	5.5	28	33	M6×1P	49
		2.5×2	2190	5360	128	104										94	
		3.5×1	1610	3750												67	
	10	1.5×2	1820	3840	136											60	
		2.5×1	1560	3200	45	122	72	16	58	15	6.6	11	6.5	29	34	M6×1P	50
		3.5×1	2080	4480	136											69	
5	3.175	1.5×2	1110	2960	90											62	
		2.5×1	950	2470	44	80	70	12	56	15	6.6	11	6.5	28	34	M6×1P	52
		2.5×2	1720	4940	110	90										101	
	3.5×1	1270	3460													72	
6	3.969	1.5×2	1480	3605	110											63	
		2.5×1	1270	3000	44	98	70	12	56	15	6.6	11	6.5	28	36	M6×1P	53
		2.5×2	2300	6000	134	104										103	
	3.5×1	1690	4200	110												73	

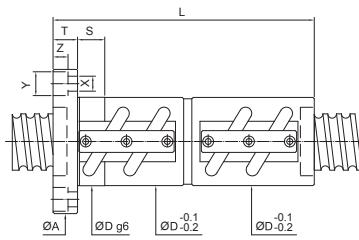
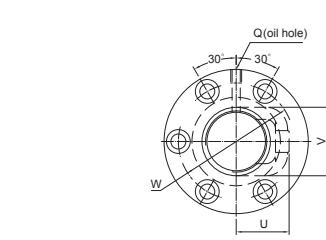


Unit: mm

SCREW SIZE	BALL DIA.	EFFECTIVE TURNS circuit x row	BASIC RATE LOAD(kgf)		NUT		FLANGE		FIT		BOLT		RETURN TUBE		OIL HOLE	STIFFNESS	
			Dynamic (1×10 <sup>6</sup> REV.) Ca	Static Co	Dg6	L	A	T	W	S	X	Y	Z	U	V	Q	kgf/μm
32	5 3.175	1.5×2	1180	3410	90											69	
		2.5×1	1010	2840	80											58	
		2.5×2	1830	5680	50	110	76	12	63	15	6.6	11	6.5	30	38	M6×1P	112
		2.5×3	2590	8520		140										164	
		3.5×1	1350	3980		90										80	
	6 3.969	1.5×2	1560	4135	104											70	
		2.5×1	1330	3450	52	92	78	12	65	15	6.6	11	6.5	32	39	M6×1P	59
		2.5×2	2410	6900		128										114	
		3.5×1	1770	4830		104										81	
	8 4.762	1.5×2	2010	5010	126											73	
		2.5×1	1720	4180	54	110	88	16	70	15	9	14	8.5	33	40	M6×1P	61
		2.5×2	3120	8360		158										118	
		3.5×1	2300	5850		126										84	
36	10 6.35	1.5×2	3000	6530	142											76	
		2.5×1	2570	5440	57	122	91	16	73	15	9	14	8.5	37	44	M8×1P	64
		2.5×2	4660	10880		182										123	
		3.5×1	3430	7620		142										88	
	6 3.969	2.5×1	1430	3950	55	92	82	12	68	15	6.6	11	6.5	32	42	M6×1P	65
		2.5×2	2600	7900		128										126	
		1.5×2	3180	7410		144										83	
		2.5×1	2720	6180	62	124	104	18	82	20	11	17.5	11	40	49	M6×1P	70
		2.5×2	4930	12360		184										136	
	10 6.35	3.5×1	3630	8650		144										90	

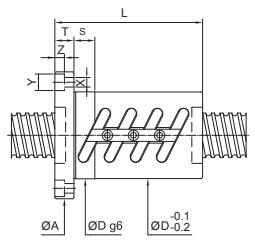
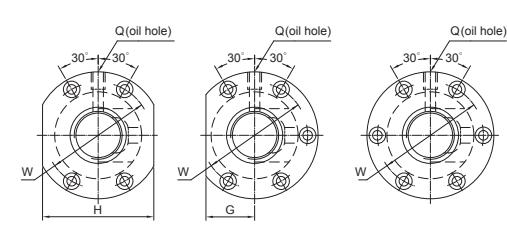


SCREW SIZE	BALL DIA.	EFFECTIVE TURNS circuit x row	BASIC RATE LOAD(kgf)		NUT		FLANGE		FIT		BOLT		RETURN TUBE		OIL HOLE	STIFFNESS	
			Dynamic (1×10 <sup>6</sup> REV.) Ca	Static Co	Dg6	L	A	T	W	S	X	Y	Z	U	V	Q	kgf/μm
40	5 3.175	1.5×2	1280	4275	94											82	
		2.5×1	1090	3560	84											69	
		2.5×2	1980	7120	58	114	92	16	72	15	9	14	8.5	34	46	M8×1P	133
		2.5×3	2800	10680		144										196	
		3.5×1	1450	4980		94										95	
	6 3.969	1.5×2	1750	5300	108											85	
		2.5×1	1500	4420	96											71	
		2.5×2	2720	8840	60	132	94	16	76	15	9	14	8.5	36	47	PT1/8"	138
		2.5×3	3850	13260		168										202	
	8 4.762	1.5×2	2000	6190		108										98	
		2.5×1	2220	6320		126										86	
		2.5×2	1900	5270	62	110	96	16	78	15	9	14	8.5	38	48	PT1/8"	141
		3.5×1	3450	10540		158										100	
45	10 6.35	1.5×2	3370	8335	152											91	
		2.5×1	2880	6950	132											71	
		2.5×2	5220	13900	65	192	106	18	85	20	11	17.5	11	42	52	PT1/8"	148
		3.5×1	3840	9730		152										105	
		2.5×1	3020	7850	70	134	112	18	90	20	11	17.5	11	48	58	PT1/8"	84
	12 7.144	2.5×2	5480	15700		194										163	
		2.5×1	3550	8950	74	158	122	18	97	20	14	20	13	49	60	PT1/8"	85
		2.5×2	6440	17900		230										165	



Unit: mm

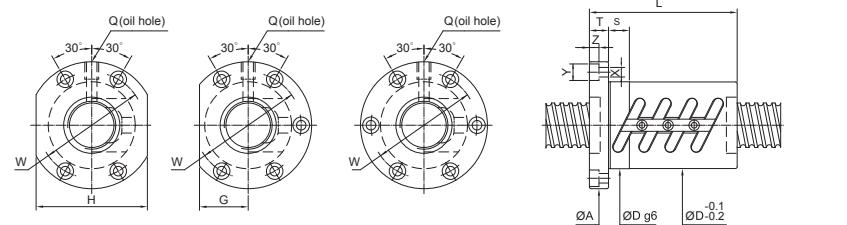
SCREW SIZE	BALL DIA.	EFFECTIVE TURNS circuit × row	BASIC RATE LOAD(kgf)		NUT		FLANGE		FIT		BOLT		RETURN TUBE		OIL HOLE	STIFFNESS	
			Dynamic (1×10 <sup>6</sup> REV.) Ca	Static Co	Dg6	L	A	T	W	S	X	Y	Z	U	V	Q	kgf/μm
50	5	1.5×2	1410	5305	107											98	
		1.5×3	2000	7960	70	127	104	16	86	15	9	14	8.5	40	56	PT1/8"	144
		3.5×1	1610	6190	107												114
	6	2.5×2	2980	11000	72	134	106	16	88	15	9	14	8.5	43	57	PT1/8"	164
		2.5×3	4220	16500	170												242
	8	2.5×2	3900	13020	75	160	116	18	95	20	11	17.5	11	45	59	PT1/8"	170
		2.5×3	5520	19530	208												250
	10	1.5×2	3725	10450	154												119
		2.5×1	3190	8710	134												91
		2.5×2	5790	17420	78	194	119	18	98	20	11	17.5	11	48	62	PT1/8"	177
		2.5×3	8200	26130	254												261
		3.5×1	4260	12190	154												126
	12	2.5×1	3700	10050	82	160	128	22	105	20	14	20	13	52	64	PT1/8"	92
		2.5×2	6710	20100	232												179
55	10	2.5×2	6005	19540	84	194	125	18	103	20	11	17.5	11	54	68	PT1/8"	191
		2.5×3	8510	29310	254												281
63	10	2.5×1	3510	11200	136												110
		2.5×2	6370	22400	90	196	132	20	110	20	11	17.5	11	53	74	PT1/8"	213
		2.5×3	9020	33600	256												313
	12	2.5×1	4760	13820	160												112
		2.5×2	8650	27560	94	232	142	22	117	20	14	20	13	57	76	PT1/8"	218
80	16	2.5×3	12250	41340	304												322
		2.5×1	8050	23100	100	200	150	22	123	20	14	20	13	62	78	PT1/8"	144
		2.5×2	14600	46200	296												280
	10	2.5×2	7130	28500	115	200	163	22	137	20	14	20	13	64	91	PT1/8"	258
		2.5×3	10100	42750	260												380
	12	2.5×2	9710	35560	120	232	169	22	143	25	14	20	13	67	93	PT1/8"	265
		2.5×3	13760	53340	302												391
	16	2.5×2	16450	59280	125	302	190	28	154	25	18	26	17.5	70	94	PT1/8"	339
		2.5×3	23300	88920	398												500



Unit: mm

SCREW SIZE	BALL DIA.	EFFECTIVE TURNS circuit × row	BASIC RATE LOAD(kgf)		NUT		FLANGE		FIT		BOLT		OIL HOLE	STIFFNESS			
			Dynamic (1×10 <sup>6</sup> REV.) Ca	Static Co	Dg6	L	A	T	W	G	H	S	X	Y	Z	Q	kgf/μm
20	4	2.5×1×(2)	450	1060	40	50	63.5	11	51	21	42	10	5.5	9.5	5.5	M6×1P	32
		3.5×1×(2)	600	1480	60	60											49
	5	2.5×1×(2)	830	1730	44	56	67	11	55	26	52	15	5.5	9.5	5.5	M6×1P	40
		3.5×1×(2)	1110	2420	65	65											55
	6	3.969 2.5×1×(2)	1100	2120	48	67	71	11	59	27	54	15	5.5	9.5	5.5	M6×1P	41
		2.5×1×(2)	1100	2120	48	78	75	13	61	27	54	15	6.6	11	6.5	M6×1P	41
	4	2.5×1×(2)	510	1355	46	50	69	11	57	26	52	15	5.5	9.5	5.5	M6×1P	43
		2.5×2×(2)	930	2710	74	74											84
	5	2.5×1×(2)	910	2150	50	55	73	11	61	28	56	15	5.5	9.5	5.5	M6×1P	48
		2.5×2×(2)	1650	4300	85	85											92
	6	2.5×1×(2)	1210	2680	53	62	76	11	64	29	58	15	5.5	9.5	5.5	M6×1P	49
		2.5×2×(2)	2190	5360	98	98											94
25	8	4.762 2.5×1×(2)	1560	3200	58	77	85	13	71	32	64	15	6.6	11	6.5	M6×1P	50
		2.5×1×(2)	1560	3200	58	100	85	15	71	32	64	15	6.6	11	6.5	M6×1P	50
	10	4.762 2.5×1×(2)	1045	2120	60	74	93	15	76	36	72	15	9	14	8.5	M8×1P	34
		2.5×1×(2)	950	2470	55	86	83	12	69	31	62	15	6.6	11	6.5	M8×1P	52
	12	5.3175 2.5×2×(2)	1720	4940	86	86											101
		2.5×1×(2)	1270	3000	63	100	83	12	69	31	62	15	6.6	11	6.5	M8×1P	53
		2.5×2×(2)	2300	6000	100	100											103
32	10	4.762 1.5×1×(2)	1045	2120	60	74	93	15	76	36	72	15	9	14	8.5	M8×1P	34
		2.5×1×(2)	565	1750	50	76	81	12	67	32	64	15	6.6	11	6.5	M6×1P	52
	4	2.5×2×(2)	1020	3500	54	76											101
		2.5×1×(2)	1010	2840	58	87	85	12	71	32	64	15	6.6	11	6.5	M8×1P	58
	6	3.969 2.5×2×(2)	1830	5680	62	99	88	12	75	34	68	15	6.6	11	6.5	M8×1P	112
		2.5×1×(2)	1330	3450	62	99											114
	8	4.762 1.5×1×(2)	1110	2510	64	80	100	15	82	38	76	15	9	14	8.5	M8×1P	37
		2.5×1×(2)	1720	4180	64	80											61
	10	6.335 2.5×1×(2)	1660	3260	74	97	108	15	90	41	82	15	9	14	8.5	M6×1P	39
		2.5×1×(2)	2570	5440	74	97											64
	12	6.335 1.5×1×(2)	1660	3260	74	110	108	18	90	41	82	15	9	14	8.5	M8×1P	39
		2.5×1×(2)	2570	5440	88	110											64

## FOWC



Unit: mm

SCREW SIZE	BALL DIA.	EFFECTIVE TURNS circuit x row	BASIC RATE LOAD(kgf)		NUT		FLANGE			FIT		BOLT			OIL HOLE	STIFFNESS	
			Dynamic (1×10 <sup>6</sup> REV) Ca	Static Co	Dg6	L	A	T	W	G	H	S	X	Y	Z	Q	kgf/μm
36	5	3.175	2.5×1×(2)	1060	3210	65	60	98	15	82	38	76	15	9	14	8.5 M8×1P	64 123
			2.5×2×(2)	1920	6420	90											
	6	3.969	2.5×1×(2)	1430	3950	65	66	98	15	82	38	76	15	9	14	8.5 M8×1P	65 126
			2.5×2×(2)	2600	7900	102											
	10	6.35	1.5×1×(2)	1750	3710	75	81	118	18	98	45	90	15	11	17.5	11 M8×1P	43 70
			2.5×1×(2)	2720	6180	103											
40	5	3.175	2.5×1×(2)	1090	3560	67	60	101	15	83	39	78	15	9	14	8.5 M8×1P	69 133
			2.5×2×(2)	1980	7120	90											
	6	3.969	2.5×1×(2)	1500	4420	70	66	104	15	86	40	80	15	9	14	8.5 PT1/8"	71 138
			2.5×2×(2)	2720	8840	102											
	8	4.762	2.5×1×(2)	1900	5270	74	83	108	15	90	41	82	15	9	14	8.5 PT1/8"	73 141
			2.5×2×(2)	3450	10540	131											
45			1.5×1×(2)	1860	4710		81										47
	10	6.35	2.5×1×(2)	2880	6950	82	103	124	18	102	47	94	20	11	17.5	11 PT1/8"	76
			3.5×1×(2)	3850	9730		121										105
	12	6.35	2.5×1×(2)	2880	6950	86	112	128	18	106	48	96	20	11	17.5	11 PT1/8"	76
			2.5×2×(2)	3020	7850	88	101	132	18	110	50	100	20	11	17.5	11 PT1/8"	84
	12	7.144	2.5×1×(2)	3550	8950	90	112	132	18	110	50	100	20	11	17.5	11 PT1/8"	85
50	5	3.175	2.5×1×(2)	1210	4420	80	60	114	15	96	43	86	15	9	14	8.5 PT1/8"	83
			2.5×2×(2)	2980	11000	84	103	118	15	100	45	90	15	9	14	8.5 PT1/8"	164
	6	3.969	2.5×2×(2)	3900	13020	87	134	129	18	107	49	98	20	11	17.5	11 PT1/8"	170
			2.5×1×(2)	3190	8710		101										91
	10	6.35	2.5×2×(2)	5790	17420	93	161	135	18	113	51	102	20	11	17.5	11 PT1/8"	177
			3.5×1×(2)	4260	12190		121										126
55	12	7.144	2.5×1×(2)	3700	10050	100	116	146	22	122	55	110	20	14	20	13 PT1/8"	92
			2.5×1×(2)	3310	9770	102	101	144	18	122	54	108	20	11	17.5	11 PT1/8"	98
	10	6.35	2.5×2×(2)	6005	19540	161											191
			2.5×1×(2)	3510	11200	108	105	154	22	130	58	116	20	14	20	13 PT1/8"	110
			2.5×2×(2)	6370	22400	165											213
	12	7.938	2.5×1×(2)	4770	13780	115	124	161	22	137	61	122	20	14	20	13 PT1/8"	113

## PMI Precision Ground BallScrew

## 13.4 High Lead Ballscrews

High-lead Ballscrews are essential elements and parts for high-speed machine tools of next century.

## Features:

It is important for a High-lead Ballscrew to be with characteristics of high rigidity, low noise and thermal control. PMI's designs and treatments are taken for following:

## High DN Value

The DN value can be 130,000 in normal case. For some special cases, for example in a fixed ends case, the DN value can be as high as 140,000. Please contact our engineers for this special application.

## High Speed

PMI's High-speed Ballscrews provide 100 m/min and even higher traverse speed for machine tools for high performance cutting.

## High Rigidity

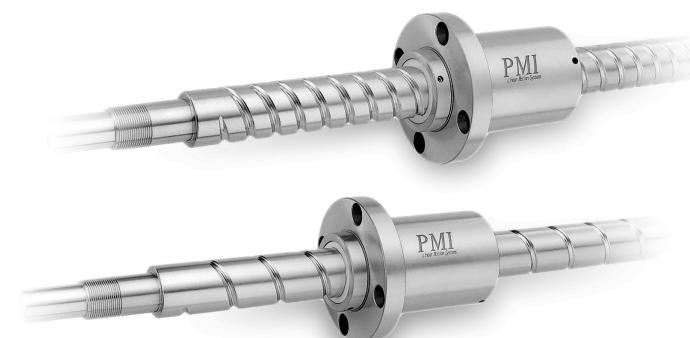
Both the screw and ballnut are surface hardened to a specific hardness and case depth to maintain high rigidity and durability.

Multiple thread starts are available to make more steel balls loaded in the ballnut for higher rigidity and durability.

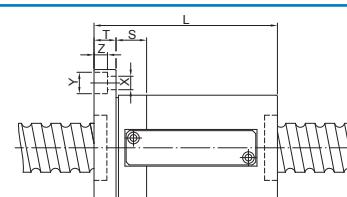
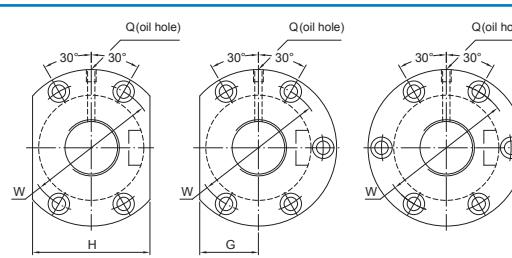
## Low Noise

Special design of ball circulation tubes offer smooth ball circulation inside the ballnut. It also makes safe ball fast running into the tubes without damaging the tubes.

Accurate ball circle diameter (BCD) through whole threads for consistent drag torque and low noise.

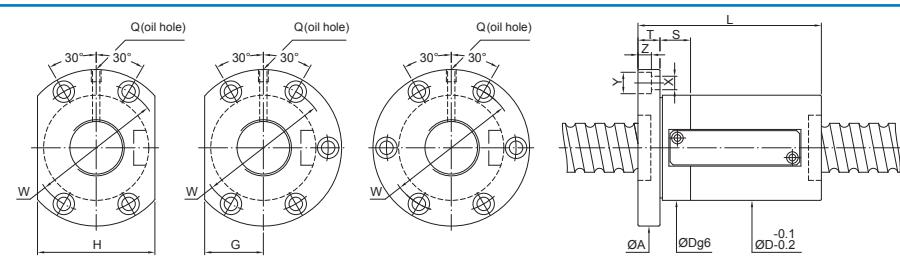


## FSWE



Unit: mm

SCREW SIZE	BALL DIA.	EFFECTIVE TURNS circuit x row	BASIC RATE LOAD(kgf)		NUT		FLANGE			FIT		BOLT		OIL HOLE	STIFFNESS	
			Dynamic (1×10 <sup>6</sup> REV.) Ca	Static Co	Dg6	L	A	T	W	G	H	S	X	Y	Z	kgf/μm
12	10	2.381	2.5×1	420	720	30	50	50	10	40	16	32	10	4.5	8	4.4 M6×1P 20
	10	3.969	2.5×1 3.5×1	1210 1580	2380 3230	63 73	73.5	13	59	25	50	10	5.5	9.5	5.5	M6×1P 34 45
20	16	3.969	1.5×1 2.5×1	830 1210	1530 2380	63 79	73.5	13	59	25	50	10	5.5	9.5	5.5	M6×1P 24 34
	20	3.969	1.5×1	830	1530	46	70	73	13	59	25	50	10	5.5	9.5	5.5 M6×1P 24
25	16	3.969	1.5×1 2.5×1	920 1340	1930 3000	62 78	76	15	64	32	64	15	6.6	11	6.5	M6×1P 28 40
	20	4.762	1.5×1 2.5×1 3.5×1	1170 1710 2220	2300 3580 4860	74 58 114										29 42 55
32	16	3.969	1.5×1 2.5×1 3.5×1 5×1	1010 1470 1910 2340	2480 3860 5240 6620	63 79 95 111										33 48 63 77
	16	6.35	3.5×1 5×1	2830 3680	6090 8270	92 74	108	108	18	90	41	82	15	11	17.5	11 M8×1P 54 69
40	20	3.969	1.5×1 2.5×1 3.5×1 5×1	1010 1470 1910 2350	2480 3860 5240 6610	70 90 110 130										33 48 63 77
	20	6.35	3.5×1 5×1	2830 3680	6090 8270	104 74	124	108	18	90	41	82	15	11	17.5	11 M8×1P 69 85

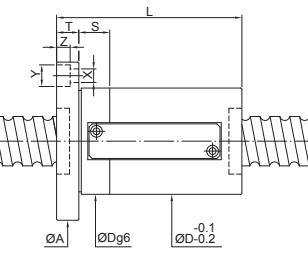
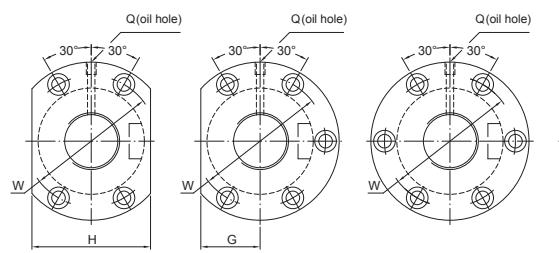


Unit: mm

SCREW SIZE	BALL DIA.	EFFECTIVE TURNS circuit x row	BASIC RATE LOAD(kgf)		NUT		FLANGE			FIT		BOLT		OIL HOLE	STIFFNESS	
			Dynamic (1×10 <sup>6</sup> REV.) Ca	Static Co	Dg6	L	A	T	W	G	H	S	X	Y	Z	kgf/μm
36	10	6.35	3.5×1 5×1	3890 4750	9390 11860	75	84 94	118	18	98	45	90	15	11	17.5	11 M8×1P 76 93
	12	6.35	3.5×1 5×1	3890 4750	9390 11860	75	97 109	118	18	98	45	90	15	11	17.5	11 M8×1P 58 76
36	16	6.35	3.5×1 5×1	3890 4750	9390 11860	75	91 107	118	18	98	45	90	15	11	17.5	11 M8×1P 58 76
	20	6.35	1.5×1 2.5×1 3.5×1 5×1	2990 2990 3890 4750	6920 6920 9390 11860	75	91 111 111 123	118	18	98	45 45	90 90	15 15	11 11	17.5 17.5	11 PT1/8" 41 58 76 93
40	10	6.35	3.5×1 5×1	4130 5050	10560 13340	86	86 96	128	18	106	49	98	15	11	17.5	11 PT1/8" 82 101
	12	6.35	3.5×1 5×1	4130 5050	10560 13340	86	91 110	128	18	106	49	98	15	11	17.5	11 PT1/8" 63 82
40	16	6.35	3.5×1 5×1	4130 5050	10560 13340	86	93 125	128	18	106	49	98	15	11	17.5	11 PT1/8" 63 82
	20	6.35	2.5×1 3.5×1 5×1	3740 4870	8790 11930	86	92 108	128	18	106	49	98	15	11	17.5	11 PT1/8" 65 84
40	20	6.35	1.5×1 2.5×1 3.5×1 5×1	2180 3180 4130 5050	5000 7780 10560 15070	86	84 104 128 124	128	18	106	49 49	98 98	15 15	11 11	17.5 17.5	11 PT1/8" 43 63 82 101
	40	6.35	1.5×1	2180	5000	86	84 104	130	128	18	106	49 49	98 98	15 15	11 11	17.5 17.5

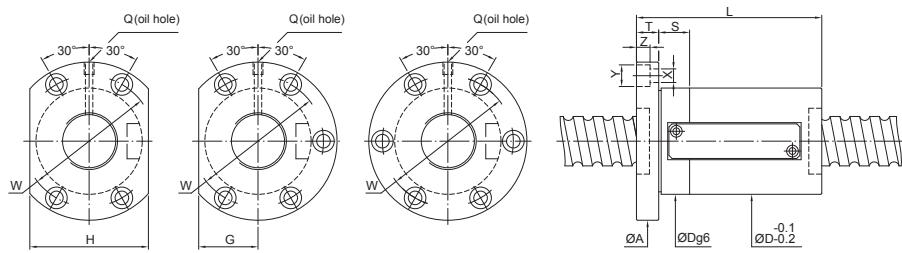
## FSWE

## FSWE



Unit: mm

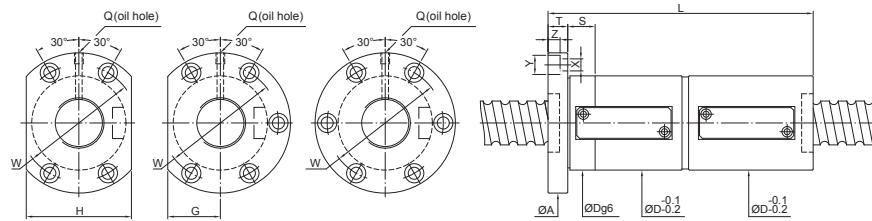
SCREW SIZE	BALL DIA.	EFFECTIVE TURNS circuit x row	BASIC RATE LOAD(kgf)		NUT		FLANGE				FIT		BOLT		OIL HOLE	STIFFNESS	
			Dynamic (1x10 <sup>6</sup> REV.) Ca	Static Co	Dg6	L	A	T	W	G	H	S	X	Y	Z	Q	kgf/μm
50	10 6.35	3.5x1 5x1	4560	13230	93	85	135	18	113	51	102	20	11	17.5	11	PT1/8"	97 119
		2.5x1	3510	9750	80												74
		3.5x1 5x1	4560	13230	93	92	135	18	113	51	102	20	11	17.5	11	PT1/8"	97 119
	12 6.35	2.5x1	4080	11260	93												75
		3.5x1 5x1	5300	15280	100	105	146	25	122	55	110	20	14	20	13	PT1/8"	99 121
		2.5x1	6480	19300	117												121
	16 6.35	3.5x1 5x1	3510	9750	94												74
		2.5x1	4560	13230	93	110	135	18	113	51	102	20	11	17.5	11	PT1/8"	97
		3.5x1 5x1	5580	16710	126												119
	16 7.144	2.5x1	4080	11260	100												75
		3.5x1 5x1	5300	15280	100	116	146	25	122	55	110	20	14	20	13	PT1/8"	99 121
		2.5x1	6480	19300	132												121
20	7.144	1.5x1	2790	7240	98												52
		2.5x1	4080	11260	100	118	146	25	122	55	110	20	14	20	13	PT1/8"	75 99
		3.5x1 5x1	5300	15280	138												121
	7.938	2.5x1 5x1	4750	12090	119												78
		3.5x1 5x1	6180	16400	105	139	152	25	128	58	116	20	14	20	13	PT1/8"	101 124
		2.5x1 5x1	7550	20720	159												124
	9.525	1.5x1	3250	7770	105	157	152	25	128	58	116	20	14	20	13	PT1/8"	53



Unit: mm

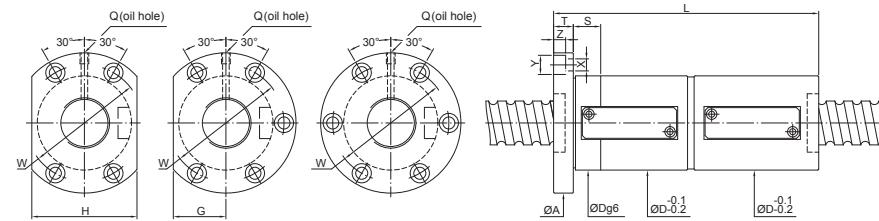
SCREW SIZE	BALL DIA.	EFFECTIVE TURNS circuit x row	BASIC RATE LOAD(kgf)		NUT		FLANGE				FIT		BOLT		OIL HOLE	STIFFNESS	
			Dynamic (1x10 <sup>6</sup> REV.) Ca	Static Co	Dg6	L	A	T	W	G	H	S	X	Y	Z	Q	kgf/μm
63	10 6.35	3.5x1 5x1	5030	17020	86	96	154	22	130	58	116	20	14	20	13	PT1/8"	115 141
		2.5x1	3870	12540	84												87
		3.5x1 5x1	5030	17020	108	96	154	22	130	58	116	20	14	20	13	PT1/8"	115 141
	12 7.144	2.5x1	4540	14460	90												89
		3.5x1 5x1	5900	19620	115	102	161	22	137	61	122	20	14	20	13	PT1/8"	117 145
		2.5x1	7210	24780	114												89
	16 7.144	3.5x1 5x1	4540	14460	97												117 145
		2.5x1	5900	19620	115	113	161	22	137	61	122	20	14	20	13	PT1/8"	120 147
		3.5x1 5x1	7210	24780	129												91
	16 7.938	2.5x1	5260	15430	112												120 147
		3.5x1 5x1	6840	20940	120	128	180	28	150	72	144	25	18	26	17.5	PT1/8"	120 147
		2.5x1	3870	12540	104												87
80	20 6.35	3.5x1 5x1	5030	17020	108	124	154	22	130	58	116	20	14	20	13	PT1/8"	115 141
		2.5x1	6150	21500	144												115 141
		3.5x1 5x1	5260	15430	112												91
	20 9.525	2.5x1	6840	20940	120												105
		3.5x1 5x1	8360	26450	144												136 167
		2.5x1	3870	12540	104												87
	10 9.525	3.5x1 5x1	5630	21660	90	100	176	22	152	66	132	20	14	20	13	PT1/8"	133 164
		2.5x1	6880	27360	130												133 164
		3.5x1 5x1	7670	27030	101	113	182	22	158	68	136	20	14	20	13	PT1/8"	143 177
100	12 9.525	2.5x1	9900	33200	108												124
		3.5x1 5x1	12990	45050	143	140	204	28	172	77	154	30	18	26	17.5	PT1/8"	162 201
		2.5x1	15880	56910	140												124
	20 9.525	3.5x1 5x1	9900	33200	120												162 201
		2.5x1	12990	45050	143	140	204	28	172	77	154	30	18	26	17.5	PT1/8"	124 162
		3.5x1 5x1	15880	56910	160												124 162
	16 9.525	2.5x1	11320	41820	115												139
		3.5x1 5x1	14720	56750	170	131	243	32	205	91	182	30	22	32	21.5	PT1/8"	182 226
		2.5x1	17990	71690	147												139
	20 9.525	2.5x1	11320	41820	128												182 226
		3.5x1 5x1	14720	56750	170	148	243	32	205	91	182	30	22	32	21.5	PT1/8"	182 226
		2.5x1	17990	71690	168												182 226

## FDWE



Unit: mm

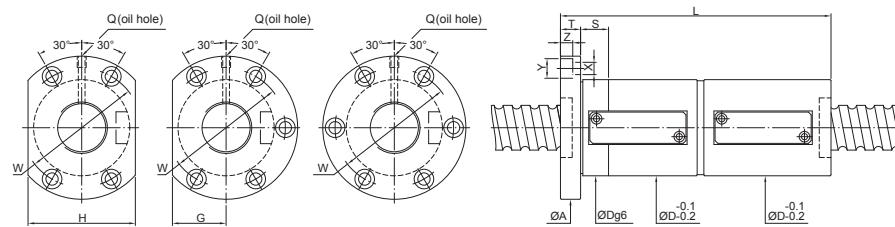
SCREW SIZE	BALL DIA.	EFFECTIVE TURNS circuit x row	BASIC RATE LOAD(kgf)		NUT		FLANGE			FIT		BOLT			OIL HOLE	STIFFNESS		
			Dynamic (1×10 <sup>6</sup> REV.) Ca	Static Co	Dg6	L	A	T	W	G	H	S	X	Y	Z	Q	kgf/μm	
12	10	2.381	2.5×1	420	720	30	102	50	10	40	16	32	10	4.5	8	4.4	M6×1P	30
	10	3.969	2.5×1 3.5×1	1210 1580	2380 3230	46	113 133	73.5	13	59	25	50	10	5.5	9.5	5.5	M6×1P	51 68
20	16	3.969	1.5×1 2.5×1	830 1210	1530 2380	46	128 160	73.5	13	59	25	50	10	5.5	9.5	5.5	M6×1P	35 51
	20	3.969	1.5×1	830	1530	46	130	73	13	59	25	50	10	5.5	9.5	5.5	M6×1P	35
25	16	3.969	1.5×1 2.5×1	920 1340	1930 3000	54	126 158	76	15	64	32	64	15	6.6	11	6.5	M6×1P	41 61
	20	4.762	1.5×1 2.5×1 3.5×1	1170 1710 2220	2300 3580 4860	154 58 234											43 63 83	
32	16	3.969	1.5×1 2.5×1 3.5×1 5×1	1010 1470 1910 2340	2480 3860 5240 6620	130 162 194 226											49 73 96 120	
	16	6.35	2.5×1 3.5×1 5×1	2830 3680 4490	6090 8270 10450	173 74 237											80 105 131	
20	16	3.969	1.5×1 2.5×1 3.5×1 5×1	1010 1470 1910 2350	2480 3860 5240 6610	93 133 173 213											49 73 96 120	
	20	6.35	2.5×1 3.5×1 5×1	2830 3680 4490	6090 8270 10450	204 74 284											80 105 131	



Unit: mm

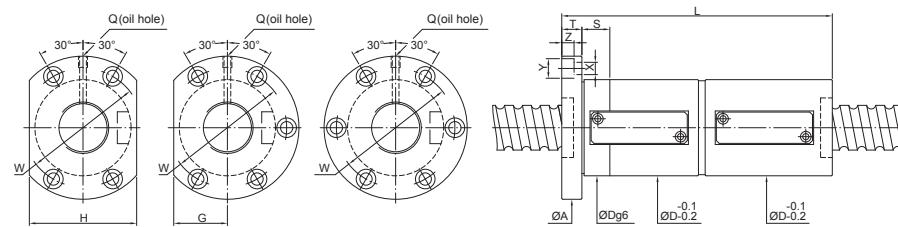
SCREW SIZE	BALL DIA.	EFFECTIVE TURNS circuit x row	BASIC RATE LOAD(kgf)		NUT		FLANGE			FIT		BOLT			OIL HOLE	STIFFNESS	
			Dynamic (1×10 <sup>6</sup> REV.) Ca	Static Co	Dg6	L	A	T	W	G	H	S	X	Y	Z	Q	kgf/μm
36	10	6.35	3.5×1 5×1	3890 4750	9390 11860	75	155 175	118	18	98	45	90	15	11	17.5	11	M8×1P 115 143
	12	6.35	2.5×1 3.5×1 5×1	2990 3890 4750	6920 9390 11860	75	140 164 188	118	18	98	45	90	15	11	17.5	11	M8×1P 88 115 143
36	16	6.35	2.5×1 3.5×1 5×1	2990 3890 4750	6920 9390 11860	75	171 203 235	118	18	98	45	90	15	11	17.5	11	M8×1P 88 115 143
	20	6.35	1.5×1 2.5×1 3.5×1 5×1	2050 2990 3890 4750	4450 6920 9390 11860	75	164 204 244 284	118	18	98	45	90	15	11	17.5	11	PT1/8" 59 88 115 143
40	10	6.35	3.5×1 5×1	4130 5050	10560 13340	86	155 175	128	18	106	49	98	15	11	17.5	11	PT1/8" 125 155
	12	6.35	2.5×1 3.5×1 5×1	3180 4130 5050	7780 10560 13340	86	141 165 189	118	18	106	49	98	15	11	17.5	11	PT1/8" 95 125 155
40	16	6.35	2.5×1 3.5×1 5×1	3180 4130 5050	7780 10560 13340	86	173 205 237	118	18	106	49	98	15	11	17.5	11	PT1/8" 95 125 155
	20	6.35	2.5×1 3.5×1 5×1	3740 4870 5950	8790 11930 15070	86	173 205 237	118	18	106	49	98	15	11	17.5	11	PT1/8" 98 128 159
40	20	6.35	1.5×1 2.5×1 3.5×1 5×1	2180 3180 4130 5050	5000 7780 10560 13340	86	164 204 244 284	128	18	106	49	98	15	11	17.5	11	PT1/8" 64 95 125 155
	40	6.35	1.5×1	2180	5000	86	242 242 242	128	18	106	49	98	15	11	17.5	11	PT1/8" 64

## FDWE



Unit: mm

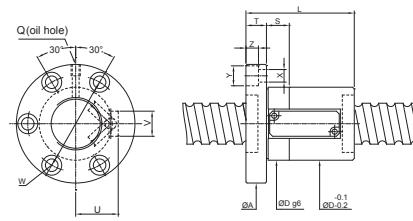
SCREW SIZE	BALL	EFFECTIVE TURNS circuit x row	BASIC RATE LOAD(kgf)		NUT		FLANGE			FIT		BOLT		OIL HOLE	STIFFNESS		
			Dynamic (1×10 <sup>6</sup> REV.) Ca	Static Co	Dg6	L	A	T	W	G	H	S	X	Y	Z	kgf/ $\mu$ m	
50	10	6.35	3.5×1 5×1	4560 5580	13230 16710	93 175	155 135	18	113 113	51	102 20	20	11	17.5 11	PT1/8"	149 185	
			2.5×1	3510	9750	141										112	
	12	6.35	3.5×1 5×1	4560 5580	13230 16710	93 189	165 189	135	18	113 113	51	102 20	20	11 11	17.5 11	PT1/8"	149 185
			2.5×1	4080	11260	161										114	
	12	7.144	3.5×1 5×1	5300 6480	15280 19300	100 209	185 19300	146	25	122 209	55	110 209	20	14 14	20 13	PT1/8"	151 187
			2.5×1	3510	9750	174										112	
	16	6.35	3.5×1 5×1	4560 5580	13230 16710	93 238	206 238	135	18	113 113	51	102 20	20	11 11	17.5 11	PT1/8"	149 185
			2.5×1	4080	11260	180										114	
	16	7.144	3.5×1 5×1	5300 6480	15280 19300	100 244	212 19300	146	25	122 244	55	110 20	20	14 14	20 13	PT1/8"	151 187
			1.5×1	2790	7240	179										77	
20	7.144	2.5×1 3.5×1 5×1	4080 5300 6480	11260 15280 19300	100 100 299	219 259	146 146	25	122 122	55	110 20	20	14 14	20 13	PT1/8"	114 151 187	
			2.5×1	4750	12090	219										117	
	7.938	3.5×1 5×1	6180	16400	105 20720	259 299	152	25	128 128	58	116 20	20	14 14	20 20	PT1/8"	154 191	
			1.5×1	3250	7770	105 105	305 305	152	25	128 128	58	116 20	20	14 14	20 20	PT1/8"	79



Unit: mm

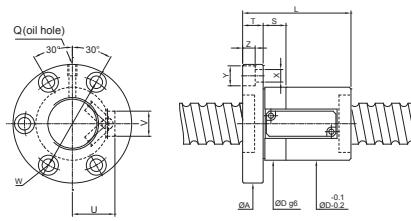
SCREW SIZE	BALL	EFFECTIVE TURNS circuit x row	BASIC RATE LOAD(kgf)		NUT		FLANGE			FIT		BOLT		OIL HOLE	STIFFNESS		
			Dynamic (1×10 <sup>6</sup> REV.) Ca	Static Co	Dg6	L	A	T	W	G	H	S	X	Y	Z	kgf/ $\mu$ m	
63	10	6.35	3.5×1 5×1	5030 6150	17020 21500	108 154	155 154	154	22	130 130	58 116	20 20	14 14	20 20	13 13	PT1/8" 178 220	
			2.5×1	3870	12540		153									134	
	12	6.35	3.5×1 5×1	5030 6150	17020 21500	108 154	177 201	154	22	130 130	58 116	20 20	14 14	20 20	13 13	PT1/8" 178 220	
			2.5×1	4540	14460		158									136	
	12	7.144	3.5×1 5×1	5900 7210	19620 24780	115 22	182 137	161 61	22	137 137	61 122	20 20	14 14	20 20	13 13	PT1/8" 180 224	
			2.5×1	4540	14460		177									136	
	16	7.144	3.5×1 5×1	5900 7210	19620 24780	115 22	209 209	161 161	22	137 137	61 122	20 20	14 14	20 20	13 13	PT1/8" 180 224	
			2.5×1	5260	15430		207									139	
	16	7.938	3.5×1 5×1	6840 8360	20940 26450	120 28	239 271	180 271	28	150 150	72 72	144 144	25 25	18 18	26 26	17.5 PT1/8" 184 228	
			2.5×1	3870	12540		205									134	
80	20	6.35	3.5×1 5×1	5030 6150	17020 21500	108 154	245 285	154 285	22	130 130	58 116	20 20	14 14	20 20	13 13	PT1/8" 178 220	
			2.5×1	8870	25870		219									158	
	20	9.525	3.5×1 5×1	11530 14090	35110 44350	122 28	259 299	182 299	28	150 150	72 72	144 144	25 25	18 18	26 26	17.5 PT1/8" 208 258	
			2.5×1	5630 6880	21660 27360	130 130	159 179	176 176	22	152 152	66 66	132 132	20 20	14 14	20 20	13 13	PT1/8" 207 256
	10	6.35	3.5×1 5×1	7670 9380	27030 34140	136 182	184 208	182 182	22	158 158	68 68	136 136	20 20	14 14	20 20	13 13	PT1/8" 222 275
100	16	7.938	3.5×1 5×1	9400 14940	33100 56740		188 252									189	
			2.5×1	12220 14940	44920 56740	143 28	220 172	204 77	28	172 172	77 77	154 154	30 30	18 18	26 26	17.5 PT1/8" 251 311	
	20	9.525	3.5×1 5×1	12220 14940	44920 56740	143 28	260 243	204 32	28	172 172	77 77	154 154	30 30	18 18	26 26	17.5 PT1/8" 251 311	
			2.5×1	9990 15880	33200 71320		211 259									213	
	16	9.525	3.5×1 5×1	12990 15880	45050 71320	170 170	243 308	243 308	32	205 205	91 91	182 182	30 30	22 22	32 32	21.5 PT1/8" 283 351	
100	20	9.525	3.5×1 5×1	12990 15880	45050 71320	170 170	268 308	243 308	32	205 205	91 91	182 182	30 30	22 22	32 32	21.5 PT1/8" 283 351	

SCREW SIZE		BALL DIA.	EFFECTIVE TURNS circuit x row	BASIC RATE LOAD(kgf)		NUT		FLANGE		FIT	BOLT		RETURN TUBE		OIL HOLE	STIFFNESS		
O.D.	LEAD	DIA.		Dynamic (1x10 <sup>6</sup> REV.) Ca	Static Co	Dg6	L	A	T	W	S	X	Y	Z	U	V	Q	kgf/μm
12	10	2.381	2.5x1	420	720	25	50	48	10	36	10	4.5	8	4.4	14	12	M6x1P	20
	10	3.969	2.5x1 3.5x1	1210	2380	63	38	62	13	50	10	5.5	9.5	5.5	23	15	M6x1P	34 45
20	16	3.969	1.5x1 2.5x1	830	1530	63	38	62	13	50	10	5.5	9.5	5.5	23	15	M6x1P	24 34
	20	3.969	1.5x1	830	1530	38	70	62	13	50	10	5.5	9.5	5.5	23	15	M6x1P	24
25	16	3.969	1.5x1 2.5x1	920	1930	42	62	68	15	55	15	6.6	11	6.6	26	14	M6x1P	28 40
	20	4.762	2.5x1 3.5x1	1170	2300	74												29
32	16	3.969	1.5x1 2.5x1 3.5x1 5x1	1010	2480	63												33 48 63 77
	16	6.35	2.5x1 3.5x1 5x1	1470	3860	49	79	78	15	63	15	6.6	11	6.6	29	15	M8x1P	101
40	20	3.969	1.5x1 2.5x1 3.5x1 5x1	1910	5240	90	95											63 85
	20	6.35	2.5x1 3.5x1 5x1	2340	6610	111												63 85
40	16	3.969	2.5x1 3.5x1 5x1	2830	8200	92												54 69
	16	6.35	3.5x1 5x1	3680	11120	57	108	98	18	77	20	11	17.5	11	34	22	M8x1P	69 85
40	20	3.969	1.5x1 2.5x1 3.5x1 5x1	1010	2480	70												33 48 63 77
	20	6.35	2.5x1 3.5x1 5x1	1470	3860	49	90	78	15	63	15	6.6	11	6.6	29	15	M8x1P	101
40	20	7.144	2.5x1 3.5x1 5x1	1910	5240	110												65 84
	20	6.35	3.5x1 5x1	2350	6610	130												103
40	20	6.35	2.5x1 3.5x1 5x1	2830	8200	104												43 63
	20	6.35	3.5x1 5x1	3680	11120	57	124	98	18	77	20	11	17.5	11	34	22	M8x1P	69 85

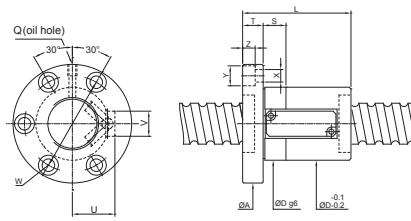


Unit: mm

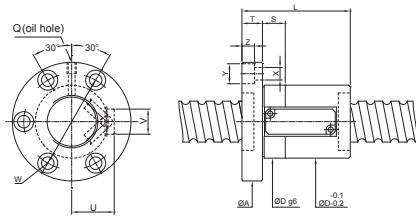
SCREW SIZE		BALL DIA.	EFFECTIVE TURNS circuit x row	BASIC RATE LOAD(kgf)		NUT		FLANGE		FIT	BOLT		RETURN TUBE		OIL HOLE	STIFFNESS		
O.D.	LEAD	DIA.		Dynamic (1x10 <sup>6</sup> REV.) Ca	Static Co	Dg6	L	A	T	W	S	X	Y	Z	U	V	Q	kgf/μm
12	10	2.381	2.5x1	420	720	25	50	48	10	36	10	4.5	8	4.4	14	12	M6x1P	20
	10	3.969	2.5x1 3.5x1	1210	2380	63	38	62	13	50	10	5.5	9.5	5.5	23	15	M6x1P	34 45
20	16	3.969	1.5x1 2.5x1	830	1530	63	38	62	13	50	10	5.5	9.5	5.5	23	15	M6x1P	24 34
	20	3.969	1.5x1	830	1530	38	70	62	13	50	10	5.5	9.5	5.5	23	15	M6x1P	24
25	16	3.969	1.5x1 2.5x1	920	1930	42	62	68	15	55	15	6.6	11	6.6	26	14	M6x1P	28 40
	20	4.762	2.5x1 3.5x1	1340	3000	42	78	68	15	55	15	6.6	11	6.6	26	14	M6x1P	28 40
32	16	3.969	1.5x1 2.5x1 3.5x1 5x1	1010	2480	63												33 48 63 77
	16	6.35	2.5x1 3.5x1 5x1	1470	3860	49	79	78	15	63	15	6.6	11	6.6	29	15	M8x1P	101
40	20	3.969	2.5x1 3.5x1 5x1	1910	5240	90	95											63 85
	20	6.35	3.5x1 5x1	2340	6610	111												63 85
40	16	3.969	2.5x1 3.5x1 5x1	2830	8200	92												54 69
	16	6.35	3.5x1 5x1	3680	11120	57	108	98	18	77	20	11	17.5	11	34	22	M8x1P	69 85
40	20	3.969	1.5x1 2.5x1 3.5x1 5x1	1010	2480	70												33 48 63 77
	20	6.35	2.5x1 3.5x1 5x1	1470	3860	49	90	78	15	63	15	6.6	11	6.6	29	15	M8x1P	101
40	20	7.144	2.5x1 3.5x1 5x1	1910	5240	110												65 84
	20	6.35	3.5x1 5x1	2350	6610	130												103
40	20	6.35	2.5x1 3.5x1 5x1	2830	8200	104												43 63
	20	6.35	3.5x1 5x1	3680	11120	57	124	98	18	77	20	11	17.5	11	34	22	M8x1P	69 85



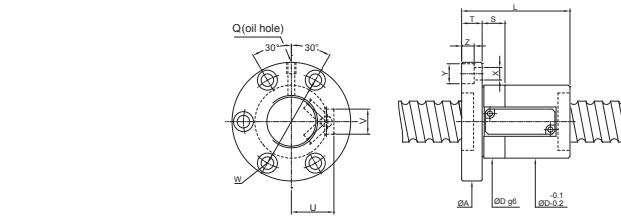
SCREW SIZE		BALL DIA.	EFFECTIVE TURNS circuit x row	BASIC RATE LOAD(kgf)		NUT		FLANGE		FIT	BOLT		RETURN TUBE		OIL HOLE	STIFFNESS		
O.D.	LEAD	DIA.		Dynamic (1x10 <sup>6</sup> REV.) Ca	Static Co	Dg6	L	A	T	W	S	X	Y	Z	U	V	Q	kgf/μm
36	10	6.35	3.5x1 5x1	3890	9390	60	84	100	18	80	20	11	17.5	11	36	22	M8x1P	76 93
	12	6.35	3.5x1 5x1	2990	6920	60	97	100	18	80	20	11	17.5	11	36	22	M8x1P	58 76
40	16	6.35	3.5x1 5x1	3890	9390	60	97	100	18	80	20	11	17.5	11	36	22	M8x1P	93 101
	20	6.35	2.5x1 3.5x1 5x1	2990	6920	60	111	100	18	80	20	11	17.5	11	36	22	M8x1P	58 76
40	10	6.35	3.5x1 5x1	4130	10560	64	84	104	18	84	20	11	17.5	11	38	22	PT1/8"	82 101
	12	6.35	3.5x1 5x1	3180	7780	64	86											63
40	16	6.35	3.5x1 5x1	4130	10560	64	98	104	18	84	20	11	17.5	11	38	22	PT1/8"	82 101
	20	6.35	3.5x1 5x1	3180	7780	64	93											63 82
40	16	6.35	3.5x1 5x1	4130	10560	64	109	104	18	84	20	11	17.5	11	38	22	PT1/8"	82 101
	20	7.144	3.5x1 5x1	3740	8790	64	92											65
40	16	7.144	3.5x1 5x1	4870	11930	64	108	104	18	84	15	11	17.5	11	38	22	PT1/8"	84 103
	20	6.35	3.5x1 5x1	5950	15070	64	124											103
40	20	6.35	1.5x1	2180	5000	64	84											43 63
	20	6.35	2.5x1 3.5x1 5x1	3180	7780	64	104	18	84	20	11	17.5	11	38	22	PT1/8"	63 82	
40	20	6.35	3.5x1 5x1	4130	10560	64	124	104	18	84	20	11	17.5	11	38	22	PT1/8"	82 101
	40	6.35	1.5x1	2180	5000	64	130	104	18	84	20	11	17.5	11	38	22	PT1/8"	43



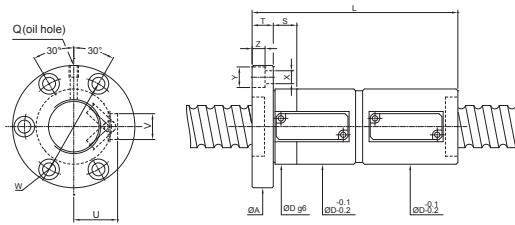
SCREW SIZE		BALL DIA.	EFFECTIVE TURNS circuit x row	BASIC RATE LOAD(kgf)		NUT		FLANGE		FIT	BOLT		RETURN TUBE		OIL HOLE	STIFFNESS		
O.D.	LEAD	DIA.		Dynamic (1×10 <sup>6</sup> REV.) Ca	Static Co	Dg6	L	A	T	W	S	X	Y	Z	U	V	Q	kgf/μm
50	10	6.35	3.5×1 5×1	4560 5580	13230 16710	73 95	85 118	18 118	96 18	20 20	11 11	17.5 17.5	11 11	43 43	22 22	PT1/8"	97 119	
			2.5×1	3510	9750	82											74	
	12	6.35	3.5×1 5×1	4560 5580	13230 16710	73 106											97 119	
			2.5×1	4080	11260	93											75	
	12	7.144	3.5×1 5×1	5300 6480	15280 19300	75 117	105 117	122 118	20 18	98 96	15 20	14 13	20 44	24 24	PT1/8"	99 121		
			2.5×1	3510	9750	94											74	
	16	6.35	3.5×1 5×1	4560 5580	13230 16710	73 126											97 119	
			2.5×1	4080	11260	100											75	
	16	7.144	3.5×1 5×1	5300 6480	15280 19300	75 132											99 121	
			1.5×1	2790	7240	98											52	
	20	7.144	2.5×1 3.5×1 5×1	4080 5300 6480	11260 15280 19300	75 118 138	122 122 138	20 20	98 15	14	20	13 44	44	20 20	PT1/8"	75 99 121		
			2.5×1	4750	12090	119											78	
50	20	7.938	3.5×1 5×1	6180 7550	16400 20720	76 159	139 139	123 123	25 25	99 20	20 14	14 20	13 46	46	25 25	PT1/8"	101 124	
			1.5×1	3250	7770	76	157	123	25	99	20	14	20	13	46	25 25	PT1/8"	53



Unit: mm

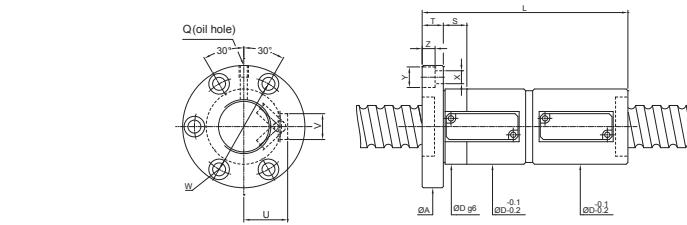


SCREW SIZE		BALL DIA.	EFFECTIVE TURNS circuit x row	BASIC RATE LOAD(kgf)		NUT		FLANGE		FIT	BOLT		RETURN TUBE		OIL HOLE	STIFFNESS		
O.D.	LEAD	DIA.		Dynamic (1×10 <sup>6</sup> REV.) Ca	Static Co	Dg6	L	A	T	W	S	X	Y	Z	U	V	Q	kgf/μm
63	10	6.35	3.5×1 5×1	5030 6150	17020 21500	86 86	86 96	133 133	22 22	108 108	20 20	14 14	20 20	13 13	49 49	24 24	PT1/8"	115 141
			2.5×1	3870	12540												87	
	12	6.35	3.5×1 5×1	5030 6150	17020 21500	86 108	96 133	133 134	22 22	110 110	20 20	14 14	20 20	13 13	50 50	25 25	PT1/8"	115 141
			2.5×1	4540	14460												89	
	12	7.144	3.5×1 5×1	5900 7210	19620 24780	87 114											117 145	
			2.5×1	4540	14460												89	
	16	7.144	3.5×1 5×1	5900 7210	19620 24780	87 129	113 134	134 22	110 110	20 20	14 14	20 20	13 13	50 50	25 25	PT1/8"	117 145	
			2.5×1	5260	15430												91	
	16	7.938	3.5×1 5×1	6840 8360	20940 26450	89 144	128 136	148 26450	28 160	118 118	25 25	18 18	26 26	17.5 17.5	52 52	25 25	PT1/8"	120 147
			2.5×1	3870	12540												87	
	20	6.35	3.5×1 5×1	5030 6150	17020 21500	86 144	124 124	133 133	22 22	108 108	20 20	14 14	20 20	13 13	49 49	24 24	PT1/8"	115 141
80	20	7.938	3.5×1 5×1	6840 8360	20940 26450	89 160	140 140	148 160	28 28	118 118	25 25	18 18	26 26	17.5 17.5	52 52	25 25	PT1/8"	120 147
			2.5×1	5260	15430												91	
			2.5×1	8870	25870												105	
	20	9.525	3.5×1 5×1	11530 14090	35110 44350	93 160	140 140	152 140	28 28	122 122	25 25	18 18	26 26	17.5 17.5	54 54	28 28	PT1/8"	136 167
100	10	6.35	3.5×1 5×1	5630 6880	21660 27360	90 100	150 100	22 22	126 126	20 20	14 14	20 20	13 13	58 58	25 25	PT1/8"	133 164	
			2.5×1	7670	27030	101 123	170 113	22 22	146 146	20 20	14 14	20 20	13 13	66 66	28 28	PT1/8"	143 177	
			2.5×1	9400	33100												124	
	16	9.525	3.5×1 5×1	12220 14940	44920 56740	126 140	124 140	185 140	28 28	155 155	30 30	18 18	26 26	17.5 17.5	70 70	28 28	PT1/8"	162 201
100	20	9.525	3.5×1 5×1	14940	56740												124	
			2.5×1	9990	33200												162	
	16	9.525	3.5×1 5×1	12990 15880	45050 71320	146 147	131 131	217 181	32 30	181 181	30 30	22 22	32 32	21.5 21.5	82 82	35 35	PT1/8"	182 226
			2.5×1	9990	33200												139	
100	20	9.525	3.5×1 5×1	12990 15880	45050 71320	146 168	148 168	217 181	32 30	181 181	30 30	22 22	32 32	21.5 21.5	82 82	35 35	PT1/8"	182 226
			2.5×1	9990	33200												139	



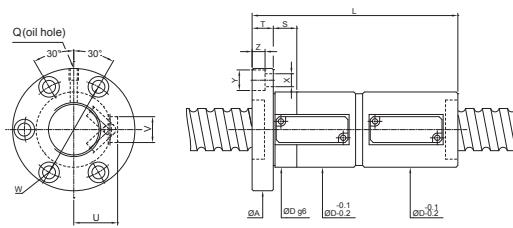
Unit: mm

SCREW SIZE		BALL	EFFECTIVE TURNS circuit x row	BASIC RATE LOAD(kgf)		NUT		FLANGE		FIT		BOLT		RETURN TUBE		OIL HOLE	STIFFNESS	
O.D.	LEAD	DIA.		Dynamic (1x10 <sup>6</sup> REV.) Ca	Static Co	Dg6	L	A	T	W	S	X	Y	Z	U	V	kgf/μm	
12	10	2.381	2.5x1	420	720	25	102	48	10	36	10	4.5	8	4.4	14	12	M6x1P 30	
	10	3.969	2.5x1	1210	2380	38	113	62	13	50	10	5.5	9.5	5.5	23	15	M6x1P 51	
20	10	3.969	3.5x1	1580	3230	133	133	62	13	50	10	5.5	9.5	5.5	23	15	M6x1P 68	
	16	3.969	1.5x1	830	1530	38	128	62	13	50	10	5.5	9.5	5.5	23	15	M6x1P 35	
25	16	3.969	2.5x1	1210	2380	160	160	62	13	50	10	5.5	9.5	5.5	23	15	M6x1P 51	
	16	3.969	1.5x1	830	1530	38	130	62	13	50	10	5.5	9.5	5.5	23	15	M6x1P 35	
32	16	3.969	2.5x1	920	1930	42	126	68	15	55	15	6.6	11	6.6	26	14	M6x1P 41	
	16	3.969	2.5x1	1340	3000	158	158	68	15	55	15	6.6	11	6.6	26	14	M6x1P 61	
40	16	6.35	1.5x1	1170	2300	44	194	72	15	59	15	6.6	11	6.5	27	16	M6x1P 43	
	20	4.762	2.5x1	1710	3580	44	194	72	15	59	15	6.6	11	6.5	27	16	M6x1P 63	
40	20	6.35	3.5x1	2220	4860	234												83
	16	3.969	1.5x1	1010	2480	130												49
40	16	3.969	2.5x1	1470	3860	49	162	78	15	63	15	6.6	11	6.6	29	15	M8x1P 73	
	16	3.969	3.5x1	1910	5240	194												96
40	16	6.35	5x1	2340	6610	226												120
	16	6.35	2.5x1	2830	8200	173												80
40	16	6.35	3.5x1	3680	11120	57	205	98	18	77	20	11	17.5	11	34	22	M8x1P 105	
	16	6.35	5x1	4490	14050	237												131
40	16	3.969	1.5x1	1010	2480	133												49
	20	3.969	2.5x1	1470	3860	49	173	78	15	63	15	6.6	11	6.6	29	15	M8x1P 73	
40	20	3.969	3.5x1	1910	5240	213												96
	20	3.969	5x1	2350	6610	253												120
40	20	6.35	2.5x1	2830	8200	204												80
	20	6.35	3.5x1	3680	11120	57	244	98	18	77	20	11	17.5	11	34	22	M8x1P 105	
	20	6.35	5x1	4490	14050	284												131



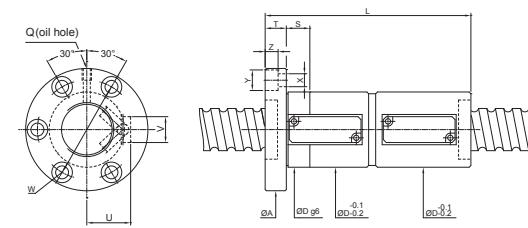
SCREW SIZE		BALL	EFFECTIVE TURNS circuit x row	BASIC RATE LOAD(kgf)		NUT		FLANGE		FIT		BOLT		RETURN TUBE		OIL HOLE	STIFFNESS
O.D.	LEAD	DIA.		Dynamic (1x10 <sup>6</sup> REV.) Ca	Static Co	Dg6	L	A	T	W	S	X	Y	Z	U	V	kgf/μm
36	10	6.35	3.5x1	3890	9390	60	155	100	18	80	20	11	17.5	11	36	22	M8x1P 115
	10	6.35	5x1	4750	11860	60	175										143
36	12	6.35	2.5x1	2990	6920	152											88
	12	6.35	3.5x1	3890	9390	60	176	100	18	80	20	11	17.5	11	36	22	M8x1P 115
36	16	6.35	2.5x1	2990	6920	173											143
	16	6.35	3.5x1	3890	9390	60	205	100	18	80	20	11	17.5	11	36	22	M8x1P 115
36	20	6.35	1.5x1	2050	4450	164											59
	20	6.35	2.5x1	2990	6920	204	100	18	80	20	11	17.5	11	36	22	M8x1P 115	
40	10	6.35	3.5x1	4130	10560	64	155	104	18	84	20	11	17.5	11	38	22	PT1/8" 125
	10	6.35	5x1	5050	13340	64	175										155
40	12	6.35	2.5x1	3180	7780	141											95
	12	6.35	3.5x1	4130	10560	64	165	104	18	84	20	11	17.5	11	38	22	PT1/8" 125
40	16	6.35	2.5x1	3180	7780	173											95
	16	6.35	3.5x1	4130	10560	64	205	104	18	84	20	11	17.5	11	38	22	PT1/8" 125
40	16	7.144	3.5x1	3740	8790	173											98
	16	7.144	5x1	4870	11930	64	205	104	18	84	20	11	17.5	11	38	22	PT1/8" 128
40	20	6.35	1.5x1	2180	5000	164											159
	20	6.35	2.5x1	3180	7780	204	104	18	84	20	11	17.5	11	38	22	PT1/8" 125	
40	20	6.35	3.5x1	4130	10560	64	244										155
	20	6.35	5x1	5050	13340	284											155
40	40	6.35	1.5x1	2180	5000	64	242	104	18	84	20	11	17.5	11	38	22	PT1/8" 64

## FDVE



Unit: mm

SCREW SIZE		BALL DIA.	EFFECTIVE TURNS circuit x row	BASIC RATE LOAD(kgf)		NUT		FLANGE		FIT		BOLT		RETURN TUBE		OIL HOLE	STIFFNESS
O.D.	LEAD			Dynamic (1×10 <sup>6</sup> REV.) Ca	Static Co	Dg6	L	A	T	W	S	X	Y	Z	U	V	Q
50	10 6.35	3.5×1 5×1	4560 13230	73 155 5580 16710	175	118 18 152	96 20 11 11	11 17.5 17.5 11	11 43 43 22	22	PT1/8"	149 185					
	12 6.35	3.5×1 5×1	4560 13230	73 176 118 18 5580 16710	200	96 20 11 11	11 17.5 17.5 11	11 43 43 22	22	PT1/8"	149 185						
	12 7.144	3.5×1 5×1	4080 11260	75 185 122 20 6480 19300	161	98 15 15 14	14 20 20 13	13 44 44 24	24	PT1/8"	114 151						
	12 7.144	3.5×1 5×1	5300 15280	75 185 122 20 6480 19300	209	98 15 15 14	14 20 20 13	13 44 44 24	24	PT1/8"	187 151						
	16 6.35	3.5×1 5×1	3510 9750	73 206 118 18 5580 16710	174	96 20 11 11	11 17.5 17.5 11	11 43 43 22	22	PT1/8"	112 149						
	16 7.144	3.5×1 5×1	4560 13230	73 212 122 20 6480 19300	238	98 15 15 14	14 20 20 13	13 44 44 24	24	PT1/8"	185 149						
	16 7.144	3.5×1 5×1	4080 11260	75 212 122 20 6480 19300	180	98 15 15 14	14 20 20 13	13 44 44 24	24	PT1/8"	114 151						
	20 7.144	3.5×1 5×1	2790 7240	75 219 122 20 5300 15280	179	259 15 15 14	14 20 20 13	13 44 44 20	20	PT1/8"	77 114						
	20 7.144	3.5×1 5×1	4080 11260	75 219 122 20 5300 15280	11260	259 15 15 14	14 20 20 13	13 44 44 20	20	PT1/8"	151 151						
	20 7.938	3.5×1 5×1	4750 12090	76 259 123 25 7550 20720	219	99 20 20 14	14 20 20 13	13 46 46 25	25	PT1/8"	117 154						
	50 7.938	1.5×1	6180 16400	76 259 123 25 7550 20720	299	99 20 20 14	14 20 20 13	13 46 46 25	25	PT1/8"	191 79						

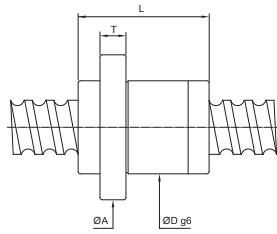
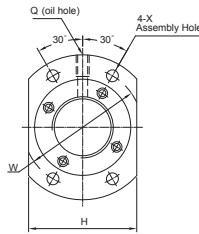


## FDVE

SCREW SIZE		BALL DIA.	EFFECTIVE TURNS circuit x row	BASIC RATE LOAD(kgf)		NUT		FLANGE		FIT		BOLT		RETURN TUBE		OIL HOLE	STIFFNESS
O.D.	LEAD			Dynamic (1×10 <sup>6</sup> REV.) Ca	Static Co	Dg6	L	A	T	W	S	X	Y	Z	U	V	Q
63	10 6.35	3.5×1 5×1	5030 17020	86 155 6150 21500	175	133 22 12540 153	108 20 177 133	14 20 22 108	20 14 20 13	13 49 49 24	24	PT1/8"	178 220				
	12 6.35	3.5×1 5×1	5030 17020	86 177 6150 21500	201	182 134 14460 158	110 20 134 206	14 20 22 110	20 13 20 13	13 50 50 25	25	PT1/8"	134 178				
	12 7.144	3.5×1 5×1	5900 19620	87 14460 7210 24780	206	134 22 19620 177	110 20 206 241	14 20 20 13	20 13 20 13	13 50 50 25	25	PT1/8"	136 180				
	16 7.144	3.5×1 5×1	5900 19620	87 14460 7210 24780	241	134 22 19620 207	110 20 206 241	14 20 20 13	20 13 20 13	13 50 50 25	25	PT1/8"	139 184				
	16 7.938	3.5×1 5×1	5260 15430	89 15430 8360 26450	207 271	239 148 26450 271	118 25 26450 271	18 26 271 301	26 17.5 271 301	52 25 52 25	25	PT1/8"	134 178				
	20 6.35	3.5×1 5×1	5030 17020	86 12540 6150 21500	205 285	245 133 17020 205	108 20 21500 205	14 20 205 285	20 13 20 13	13 49 49 24	24	PT1/8"	134 178				
	20 7.938	3.5×1 5×1	6840 20940	89 15430 8360 26450	221 301	261 148 26450 301	118 25 301 221	18 26 221 301	26 17.5 221 301	52 25 52 25	25	PT1/8"	139 184				
	20 9.525	3.5×1 5×1	11530 35110	93 259 152 14090 44350	289	259 152 44350 289	122 25 44350 289	18 26 28 122	25 18 25 122	17.5 54 54 28	28	PT1/8"	158 208				
	10 6.35	3.5×1 5×1	5630 21660	103 159 6880 27360	179	150 22 27360 179	126 20 179 150	14 20 150 22	20 13 20 13	13 58 58 25	25	PT1/8"	207 256				
	12 7.938	3.5×1 5×1	7670 27030	123 184 9380 34140	208	170 22 34140 208	146 20 208 170	14 20 20 170	20 13 20 13	13 66 66 28	28	PT1/8"	222 275				
	16 9.525	3.5×1 5×1	9400 33100	188	33100 188	122 20 44920 122 20	185 185	28 155 122 20 185	30 18 122 20 185	26 17.5 18 26	28	PT1/8"	189 251				
80	16 9.525	3.5×1 5×1	12220 44920	14940 56740	252	14940 56740 56740 252	220 220	185 185	28 155 122 20 185	30 18 122 20 185	26 17.5 18 26	28	PT1/8"	251 311			
	20 9.525	3.5×1 5×1	12220 44920	14940 56740	300	14940 56740 56740 300	268 268	185 185	28 155 122 20 185	30 18 122 20 185	26 17.5 18 26	28	PT1/8"	189 251			
	100	2.5×1	9990 33200	211												213	
	16 9.525	3.5×1 5×1	12990 45050	146 243 217 15880 71320	259	181 30 71320 259	215 215	82 82	32 32 32 21.5	35 35	35	PT1/8"	213 283				
	20 9.525	3.5×1 5×1	12990 45050	146 268 217 15880 71320	308	181 30 71320 308	215 215	82 82	32 32 32 21.5	35 35	35	PT1/8"	213 351				

## 13.5 End Cap Series

FSKC



Unit: mm

End Cap Series

SCREW SIZE O.D.	LEAD	BALL DIA	EFFECTIVE TURNS circuit x number of thread	BASIC RATE LOAD(kgf)		BALLNUT DIMENSION								
				Dynamic (1×10 <sup>6</sup> REV.) Ca	Static Co	NUT		FLANGE			BOLT	OIL HOLE	STIFFNESS	
						Dg6	L	A	T	H	W	X	Q	kgf/μm
15	10	3.715	2.8×2	1410	2800	34	44	57	10	40	45	5.5	M6×1P	34
16	16	3.175	1.8×2	700	1400	32	38	53	10	38	42	4.5	M6×1P	18
20	20	3.175	1.8×2	1100	2500	39	52	62	10	46	50	5.5	M6×1P	29
25	25	3.969	1.8×2 1.8×4	1650 2830	3900 7800	47	62	74	12	56	60	6.6	M6×1P	35 69
32	32	4.762	1.8×2 1.8×4	2360 4280	5940 11800	58	78	92	15	68	74	9	M6×1P	44 87
36	24	7.144	2.8×2	6450	15220	75	94	115	18	86	94	11	M6×1P	77
40	40	6.35	1.8×2 1.8×4	3860 7000	9900 19880	73	95	114	17	84	93	11	M6×1P	55 108
50	50	7.938	1.8×2 1.8×4	5800 10520	15800 31600	90	120	135	20	104	112	14	M6×1P	68 135

## 13.6 Ballscrews For Heavy Load

### Features

Focused on improvements of contact points of balls and thread grooves, ball diameter and circulation system for new type, FSVH. The rated dynamic load has been increased to as two times as that of conventional type, FSVC.

### Long Life

Structure of the newly developed circulation system is designed to distribute the load uniformly to the load balls and it also increases the life of ballscrews.

On conventional circulation system, FSVC, the returning tube is inserted into the holes on ballnut perpendicularly which forms an advancing angle. While ball moves into returning tube, it will hit tube end area and then move into returning tube.

New circulation system, FSVH, ball will move into returning tube smoothly by tangent line as the same direction as lead angle. It can increase the life of circulation system structure.

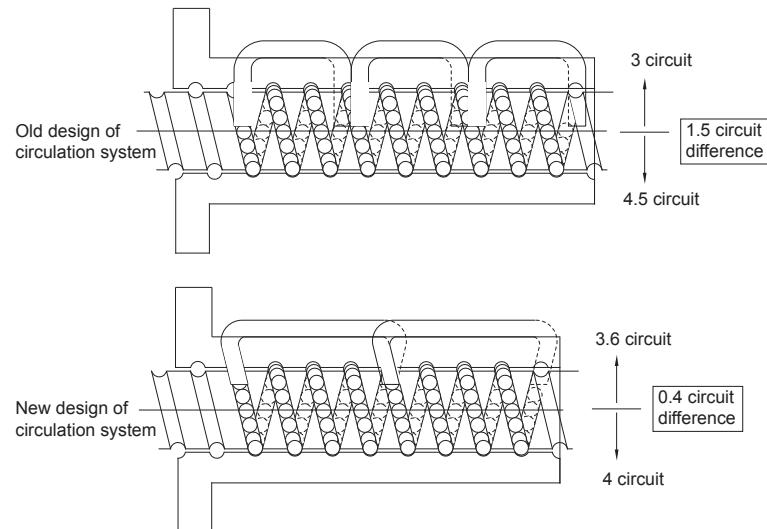


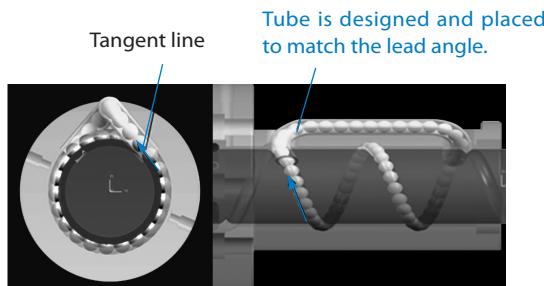
Fig.13.4 Circuit difference for heavy load ballscrew

### High DN Value

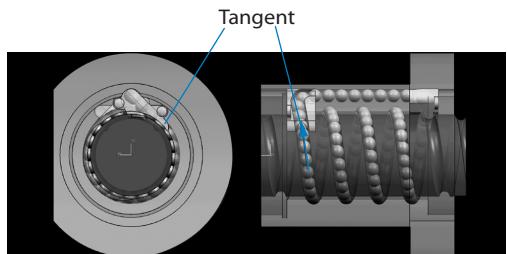
With the newly developed circulation system, ballscrews can meet the demands of high speed running with high DN value.

### Low Noise

To use tangential circulation system structure, it can eliminate the noise while balls run into the returning tube.



**FSVH circulation system structure(NEW)**

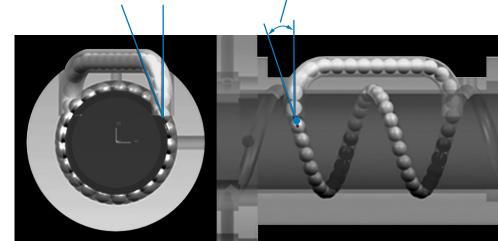


**FSDH circulation system structure (NEW)**

Fig.13.5 Circulation system structure for FSVH and FSDH

Advancing angle exists.

Angle exists due to the tube is placed not to in line with lead angle.



**FSVC circulation system structure**

Fig.13.6 Circulation system structure for FSVC

### Various Specifications Combination

PMI can supply various ballscrews with diameter 40~120mm and lead 10mm to 60mm (Please contact PMI for your specific design requirement)

### Recommend mounting direction of heavy load ball screws

In order to support equal load distribution for shaft and nut, recommend mounting direction of ball screws allow fig. 13.7. This mounting direction can avoid vibration as axial load uneven distribution for ball screws, therefore increase service life efficient.

### Application

Plastic Injection Machines / Press and Forging Machines  
Semi-conductor Equipments / General Machines

## FSVH

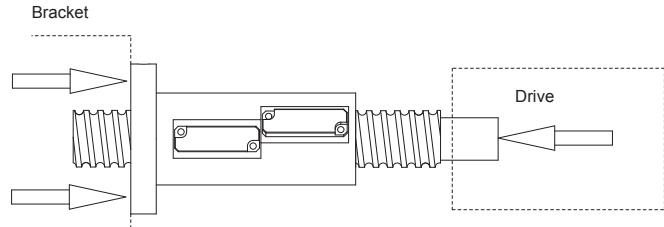


Fig.13.7 Recommend mounting direction of heavy load ballscrew

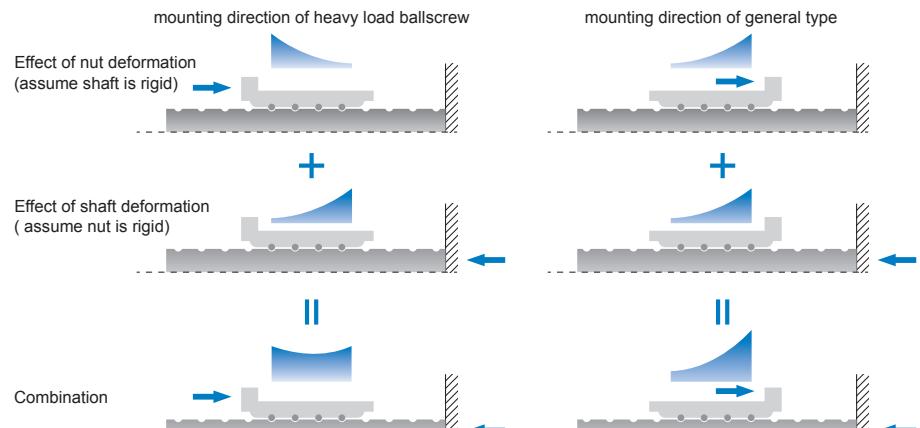
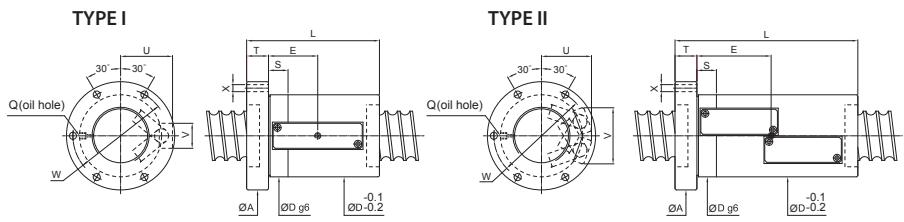
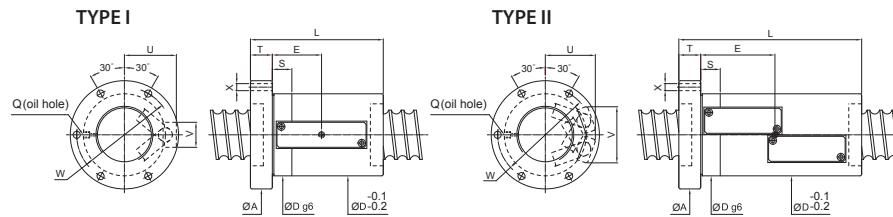


Fig.13.8 Load distribution



SCREW SIZE	BALL DIA.	EFFECTIVE CIRCUIT X ROW	BASIC RATE LOAD(kg)		NUT		FLANGE		FIT		OIL HOLE		BOLT		RETURN TUB		Type
			DYNAMIC (1x10 <sup>6</sup> REV.)	STATIC Ca	Dg6	L	A	T	W	S	Q	E	X	V	U		
40	10	7.938	3.5x2	15000	41800	66	124	98	18	83	20	M6x1P	50.75	9	51	43	II
	12	9.525	3.5x2	18600	48200	70	156	93	18	86	20	M6x1P	58	9	55	45	II
45	10	7.938	3.5x2	15900	47300	70	134	104	18	87	20	M6x1P	54.2	9	54	45	II
	10	7.938	3.5x2	16700	52900	77	133	109	18	92	20	M6x1P	53.7	9	60	48	II
50	12.7	6x1	24800	63700	95	168	128	28	112	20	PT1/8"	70.5	9	32	60	I	
	16	12.7	3.5x2	31200	83500	95	200	128	28	112	20	PT1/8"	86	9	72	62	II
	20	12.7	3.5x2	31200	84800	95	235	128	28	112	20	PT1/8"	97	9	72	62	II
55	10	7.938	3.5x2	17500	58500	80	153	114	28	97	20	PT1/8"	62.1	9	61	49	II
	16	12.7	6x1	25800	71800	100	168	133	28	115	20	PT1/8"	69.5	9	32	63	I
	16	12.7	3.5x2	32600	94000	100	200	133	28	115	20	PT1/8"	84.5	9	77	64	II
63			6x1	27800	81700	105	168	138	28	122	25		65.25	9	32	66	I
	16	12.7	3.5x2	35000	107000	105	202	138	28	122	25	PT1/8"	82.25	9	80	67	II
			6x2	50300	164000	105	266	138	28	122	25		114.25	9	80	67	II
	20	15.875	2.5x2	35900	99300	117	210	157	32	137	25	PT1/8"	96	11	88	74	II
			3.5x2	46600	134700	117	246	157	32	137	25	PT1/8"	105.5	11	88	74	II
80	25	15.875	2.5x2	35900	99300	117	235	157	32	137	25	PT1/8"	91	11	88	75	II
			6x1	30900	104400	120	172	158	32	139	25		66	9	36	73	I
	16	12.7	3.5x2	39000	136700	120	205	158	32	139	25	PT1/8"	84	9	89	74	II
			6x2	56000	208700	120	275	158	32	139	25		122	9	89	74	II
			2.5x2	40100	127000	130	210	168	32	150	25		87.5	11	90	83	II
	20	15.875	3.5x2	52100	172400	130	250	168	32	150	25	PT1/8"	107.5	11	90	83	II
			6x2	75000	263200	130	330	168	32	150	30		147.5	11	90	83	II
	25	19.05	3.5x2	67700	206100	145	305	188	40	165	25	PT1/8"	119	11	108	94	II
			6x2	97200	314600	145	402	188	40	165	30	PT1/8"	169	11	108	94	II

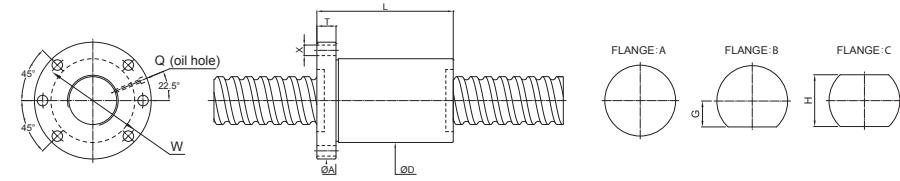


FSVH

PMI Precision Ground BallScrew

## 13.7 Heavy Load Series of End Deflector

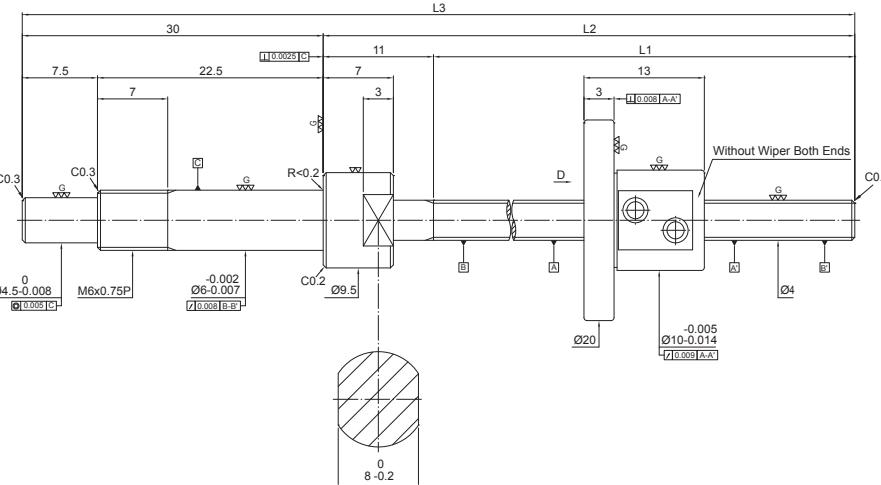
FSDH



Unit: mm

SCREW SIZE	BALL DIA.	EFFECTIVE TURNS circuit x row	BASIC RATE LOAD(kgf)		NUT	FLANGE			FIT	OIL HOLE		BOLT	RETURN TUB	Type		
			Dynamic (1x10 <sup>6</sup> REV.) Ca	Static Co		Dg6	L	A		T	W					
100	16	6x1	34200	133200	145	172	185	32	165	25	PT1/8"	63.5	11	38	85	I
		3.5x2	43200	174500	145	205	185	32	165	25		79.5	11	98	85	II
		6x2	62000	266300	145	275	185	32	165	25		117.5	11	98	85	II
	20	2.5x2	44800	160900	150	205	194	32	172	30	PT1/8"	82	11	107	92	II
		3.5x2	58300	218400	150	245	194	32	172	30		102	11	107	92	II
		6x2	83800	333300	150	330	194	32	172	30		147	11	107	92	II
	25	3.5x2	74900	262000	165	305	218	40	190	30	PT1/8"	122	11	111	102	II
		6x2	107700	397100	165	410	218	40	190	30		177	11	111	102	II
		3.5x2	43000	170700	173	230	213	40	193	30	PT1/8"	84	11	38	93	I
120	16	6x1	34100	130200	173	205	213	40	193	30	PT1/8"	101	11	108	94	II
		3.5x2	43000	170700	173	230	213	40	193	30		116	11	121	104	II
	20	6x1	46000	160800	173	222	213	40	193	30	PT1/8"	95	11	54	100	I
		3.5x2	58100	210700	173	260	213	40	193	30		109.5	11	50	106	I
	25	6x1	59200	194500	183	261	213	40	193	30	PT1/8"	135.5	11	129	109	II
		3.5x2	74700	254800	183	314	213	40	193	30						

## 13.8 Miniature Series

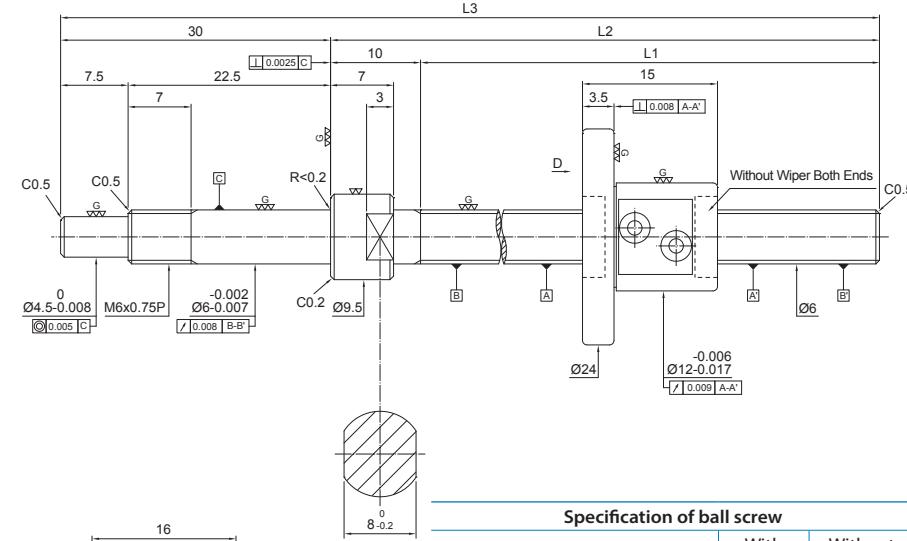
Miniature Ballscrews  
Screw Dia. Ø4 Lead01 **FSMC**

## Specification of ball screw

Production Specification		With Preload	Without Preload
Number of Thread / Thread Direction	BCD	1/Right	
BCD		4.1	
Lead		1	
Ball Dia.		0.8	
Effective Turns (Circuit × Row)		2.5 × 1	
Lead Angle		4.44	
Dynamic Rate Load Ca (kgf)		49	
Static Rate Load Co (kgf)		70	
Axial Play	0	0.005 or less	
Preloading Torque (kgf-cm)	0.01~0.1	0.03 or less	

Unit: mm

Model No.	Screw Spindle (Shaft) Length			Accuracy Grade	Lead Accuracy		
	L1	L2	L3		Specified Travel (T)	Accumulated reference lead deviation E	Lead Deriation in random 300mm e <sub>300</sub>
FSM0401-C3-1R-0085	44	55	85	3	0	0.012	0.008
FSM0401-C3-1R-0105	64	75	105	3	0	0.012	0.008
FSM0401-C3-1R-0135	94	108	138	3	0	0.012	0.008

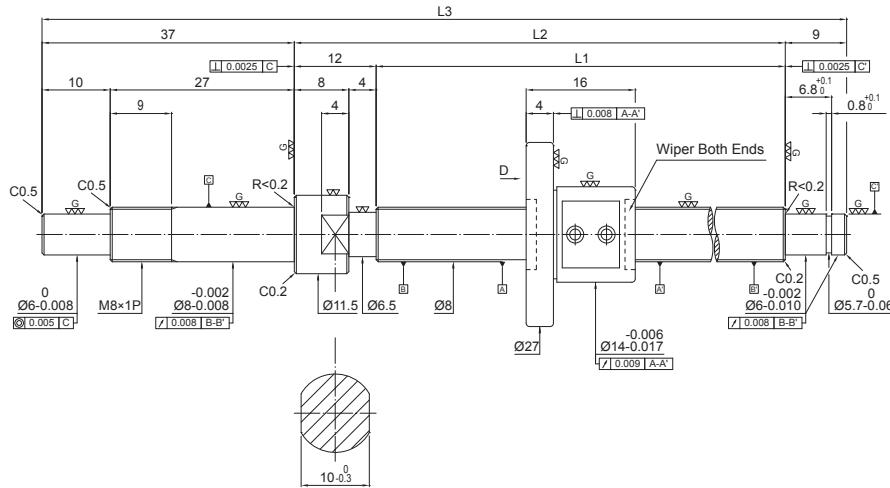
Miniature Ballscrews  
Screw Dia. Ø6 Lead01 **FSMC**

## Specification of ball screw

Production Specification		With Preload	Without Preload
Number of Thread / Thread Direction	BCD	1/Right	
BCD		6.1	
Lead		1	
Ball Dia.		0.8	
Effective Turns (Circuit × Row)		2.5 × 1	
Lead Angle		2.99	
Dynamic Rate Load Ca (kgf)		58	
Static Rate Load Co (kgf)		100	
Axial Play	0	0.005 or less	
Preloading Torque (kgf-cm)	0.01~0.15	0.03 or less	

Unit: mm

Model No.	Screw Spindle (Shaft) Length			Accuracy Grade	Lead Accuracy		
	L1	L2	L3		Specified Travel (T)	Accumulated reference lead deviation E	Lead Deriation in random 300mm e <sub>300</sub>
FSM0601-C3-1R-0105	65	75	105	3	0	0.012	0.008
FSM0601-C3-1R-0135	95	105	135	3	0	0.012	0.008
FSM0601-C3-1R-0165	125	135	165	3	0	0.012	0.008

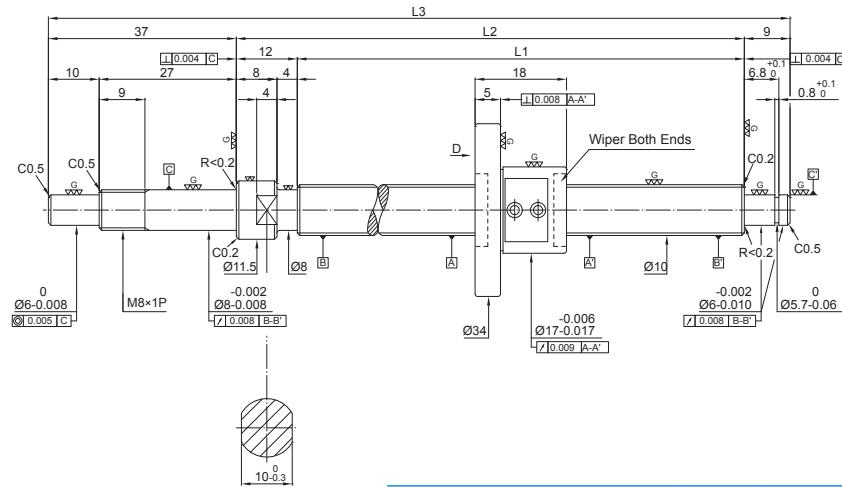


## Specification of ball screw

Production Specification		With Preload	Without Preload
Number of Thread / Thread Direction	BCD	1/Right	
Lead	1		
Ball Dia.	0.8		
Effective Turns (Circuit × Row)	2.5 × 1		
Lead Angle	2.25		
Dynamic Rate Load Ca (kgf)	66		
Static Rate Load Co (kgf)	140		
Axial Play	0	0.005 or less	
Preloading Torque (kgf-cm)	0.01~0.2	0.05 or less	

Unit: mm

Model No.	Screw Spindle (Shaft) Length			Accuracy Grade	Lead Accuracy		
	L1	L2	L3		Specified Travel (T)	Accumulated reference lead deviation E	Lead Deriation in random 300mm e <sub>300</sub>
FSM0801-C3-1R-0138	80	92	138	3	0	0.012	0.008
FSM0801-C3-1R-0168	110	122	168	3	0	0.012	0.008
FSM0801-C3-1R-0198	140	152	198	3	0	0.012	0.008
FSM0801-C3-1R-0248	190	202	248	3	0	0.012	0.008

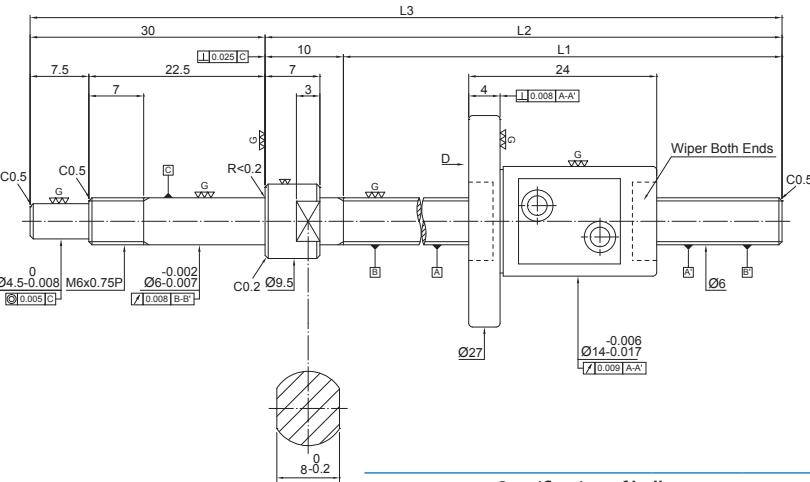


## Specification of ball screw

Production Specification		With Preload	Without Preload
Number of Thread / Thread Direction	BCD	1/Right	
Lead	1		
Ball Dia.	0.8		
Effective Turns (Circuit × Row)	2.5 × 1		
Lead Angle	1.8		
Dynamic Rate Load Ca (kgf)	73		
Static Rate Load Co (kgf)	180		
Axial Play	0	0.005 or less	
Preloading Torque (kgf-cm)	0.01~0.3	0.05 or less	

Unit: mm

Model No.	Screw Spindle (Shaft) Length			Accuracy Grade	Lead Accuracy		
	L1	L2	L3		Specified Travel (T)	Accumulated reference lead deviation E	Lead Deriation in random 300mm e <sub>300</sub>
FSM1001-C3-1R-0168	110	122	168	3	0	0.012	0.008
FSM1001-C3-1R-0218	160	172	218	3	0	0.012	0.008
FSM1001-C3-1R-0268	210	222	268	3	0	0.012	0.008
FSM1001-C3-1R-0318	260	272	318	3	0	0.012	0.008
FSM1001-C3-1R-0368	310	322	368	3	0	0.013	0.008

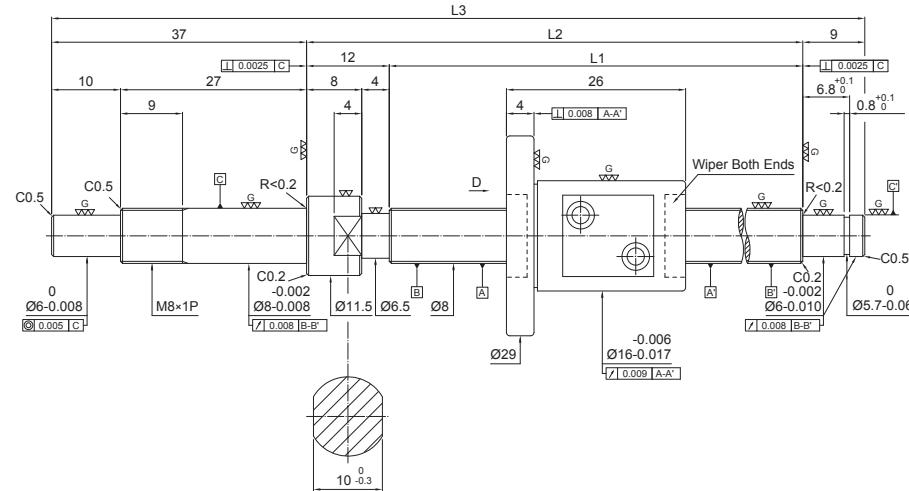
**FSMC** Miniature Ballscrews  
Screw Dia. Ø6 Lead02


Specification of ball screw

Production Specification		With Preload	Without Preload
Number of Thread / Thread Direction	BCD	1/Right	
BCD	6.3		
Lead	2		
Ball Dia.	1.588		
Effective Turns (Circuit × Row)	2.5 × 1		
Lead Angle	5.77		
Dynamic Rate Load Ca (kgf)	160		
Static Rate Load Co (kgf)	210		
Axial Play	0	0.005 or less	
Preloading Torque (kgf-cm)	0.01~0.2	0.05 or less	

Unit: mm

Model No.	Screw Spindle (Shaft) Length			Accuracy Grade	Lead Accuracy		
	L1	L2	L3		Specified Travel (T)	Accumulated reference lead deviation E	Lead Deriation in random 300mm e <sub>300</sub>
FSM0602-C3-1R-0105	65	75	105	3	0	0.012	0.008
FSM0602-C3-1R-0135	95	105	135	3	0	0.012	0.008
FSM0602-C3-1R-0165	125	135	165	3	0	0.012	0.008

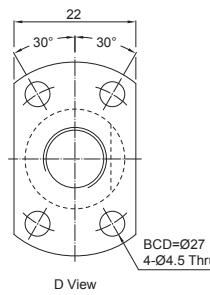
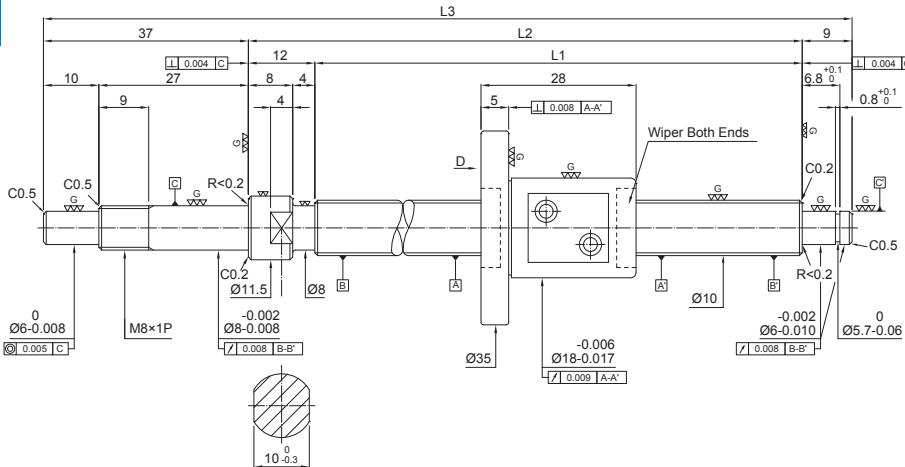
**FSMC** Miniature Ballscrews  
Screw Dia. Ø8 Lead02


Specification of ball screw

Production Specification		With Preload	Without Preload
Number of Thread / Thread Direction	BCD	1/Right	
BCD	8.3		
Lead	2		
Ball Dia.	1.588		
Effective Turns (Circuit × Row)	2.5 × 1		
Lead Angle	4.39		
Dynamic Rate Load Ca (kgf)	190		
Static Rate Load Co (kgf)	290		
Axial Play	0	0.005 or less	
Preloading Torque (kgf-cm)	0.01~0.2	0.05 or less	

Unit: mm

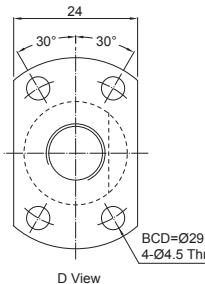
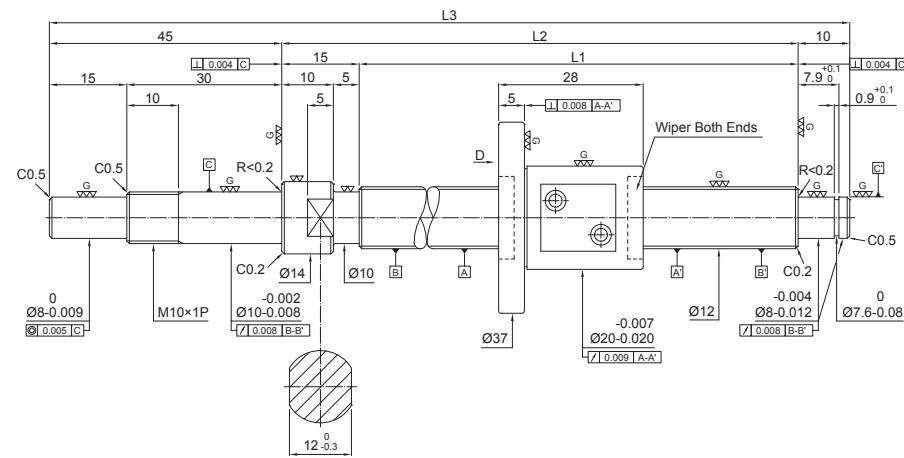
Model No.	Screw Spindle (Shaft) Length			Accuracy Grade	Lead Accuracy		
	L1	L2	L3		Specified Travel (T)	Accumulated reference lead deviation E	Lead Deriation in random 300mm e <sub>300</sub>
FSM0802-C3-1R-0138	80	92	138	3	0	0.012	0.008
FSM0802-C3-1R-0168	110	122	168	3	0	0.012	0.008
FSM0802-C3-1R-0198	140	152	198	3	0	0.012	0.008
FSM0802-C3-1R-0248	190	202	248	3	0	0.012	0.008

**FSMC** Miniature Ballscrews  
Screw Dia.Ø10 Lead02


Production Specification			With Preload	Without Preload
Number of Thread / Thread Direction			1/Right	
BCD			10.3	
Lead			2	
Ball Dia.			1.588	
Effective Turns (Circuit × Row)			2.5 × 1	
Lead Angle			3.54	
Dynamic Rate Load Ca (kgf)			220	
Static Rate Load Co (kgf)			370	
Axial Play	0	0.005 or less		
Preloading Torque (kgf-cm)	0.01~0.3	0.05 or less		

Unit: mm

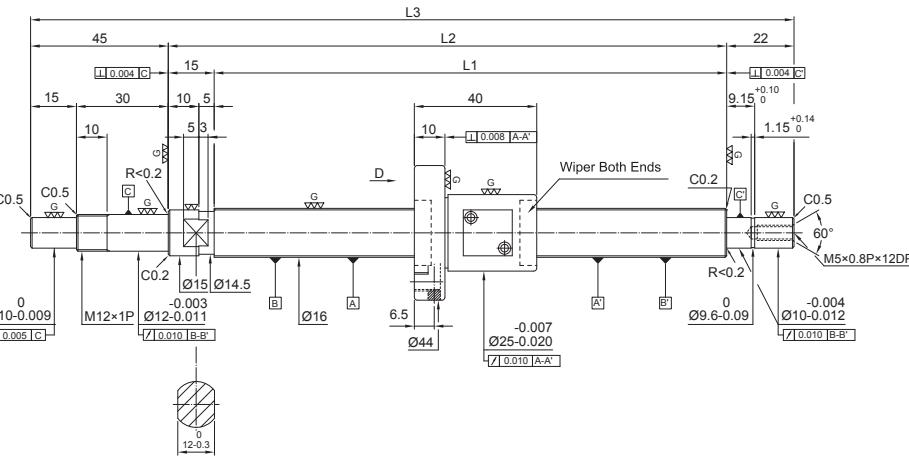
Model No.	Screw Spindle (Shaft) Length			Accuracy Grade	Lead Accuracy		
	L1	L2	L3		Specified Travel (T)	Accumulated reference lead deviation E	Lead Derivation in random 300mm $e_{300}$
FSM1002-C3-1R-0168	110	122	168	3	0	0.012	0.008
FSM1002-C3-1R-0218	160	172	218	3	0	0.012	0.008
FSM1002-C3-1R-0268	210	222	268	3	0	0.012	0.008
FSM1002-C3-1R-0318	260	272	318	3	0	0.012	0.008
FSM1002-C3-1R-0368	310	322	368	3	0	0.012	0.008

**FSMC** Miniature Ballscrews  
Screw Dia.Ø12 Lead02


Production Specification			With Preload	Without Preload
Number of Thread / Thread Direction			1/Right	
BCD			12.3	
Lead			2	
Ball Dia.			1.588	
Effective Turns (Circuit × Row)			2.5 × 1	
Lead Angle			2.96	
Dynamic Rate Load Ca (kgf)			240	
Static Rate Load Co (kgf)			450	
Axial Play	0	0.005 or less		
Preloading Torque (kgf-cm)	0.04~0.4	0.1 or less		

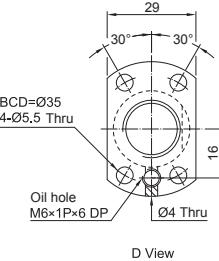
Unit: mm

Model No.	Screw Spindle (Shaft) Length			Accuracy Grade	Lead Accuracy		
	L1	L2	L3		Specified Travel (T)	Accumulated reference lead deviation E	Lead Derivation in random 300mm $e_{300}$
FSM1202-C3-1R-0180	110	125	180	3	0	0.012	0.008
FSM1202-C3-1R-0230	160	175	230	3	0	0.012	0.008
FSM1202-C3-1R-0280	210	225	280	3	0	0.012	0.008
FSM1202-C3-1R-0330	260	275	330	3	0	0.012	0.008
FSM1202-C3-1R-0380	310	325	380	3	0	0.012	0.008



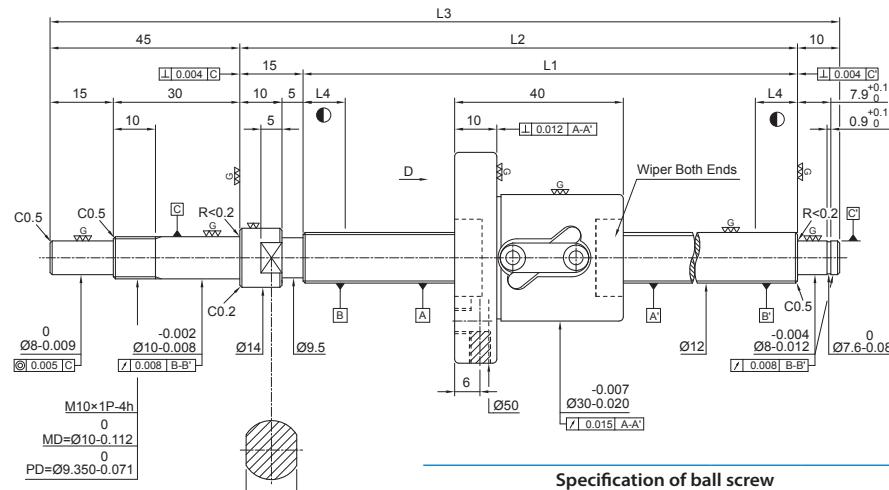
Specification of ball screw		
Production Specification	With Preload	Without Preload
Number of Thread / Thread Direction	1/Right	
BCD	16.3	
Lead	2	
Ball Dia.	1.588	
Effective Turns (Circuit x Row)	3.5 x 1	
Lead Angle	2.24	
Dynamic Rate Load Ca (kgf)	360	
Static Rate Load Co (kgf)	850	
Axial Play	0	0.005 or less
Preloading Torque (kgf-cm)	0.05~0.5	0.15 or less

Unit: mm

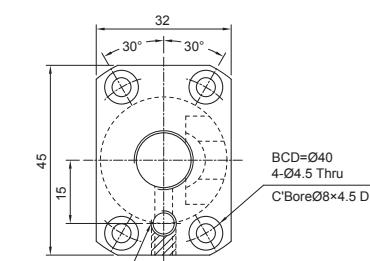


D View

Model No.	Screw Spindle (Shaft) Length			Accuracy Grade	Lead Accuracy		
	L1	L2	L3		Specified Travel (T)	Accumulated reference lead deviation E	Lead Derivation in random 300mm e <sub>300</sub>
FSM1602-C3-1R-0221	139	154	221	3	0	0.012	0.008
FSM1602-C3-1R-0271	189	204	271	3	0	0.012	0.008
FSM1602-C3-1R-0321	239	254	321	3	0	0.012	0.008
FSM1602-C3-1R-0371	289	304	371	3	0	0.012	0.008
FSM1602-C3-1R-0471	389	404	471	3	0	0.013	0.008

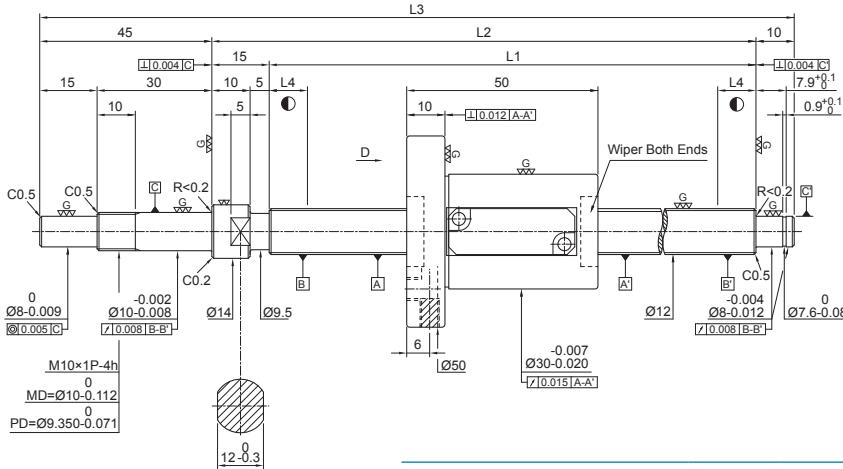


Specification of ball screw		
Production Specification	With Preload	Without Preload
Number of Thread / Thread Direction	1/Right	
BCD	12.4	
Lead	5	
Ball Dia.	2.381	
Effective Turns (Circuit x Row)	2.5 x 1	
Lead Angle	7.31	
Dynamic Rate Load Ca (kgf)	380	
Static Rate Load Co (kgf)	640	
Axial Play	0	0.005 or less
Preloading Torque (kgf-cm)	0.01~0.45	0.1 or less



D View

Model No.	Screw Spindle (Shaft) Length				Accuracy Grade	Lead Accuracy	
	L1	L2	L3	L4		Accumulated reference lead deviation E	Lead Derivation in random 300mm e <sub>300</sub>
1R12-05B1-FSWC-110-180-0.008	110	125	180	10	3	0.012	0.008
1R12-05B1-FSWC-160-230-0.008	160	175	230	10	3	0.012	0.008
1R12-05B1-FSWC-210-280-0.008	210	225	280	10	3	0.012	0.008
1R12-05B1-FSWC-260-330-0.008	260	275	330	10	3	0.012	0.008
1R12-05B1-FSWC-310-380-0.008	310	325	380	10	3	0.012	0.008
1R12-05B1-FSWC-410-480-0.008	410	425	480	15	3	0.013	0.008
1R12-05B1-FSWC-510-580-0.008	510	525	580	15	3	0.015	0.008

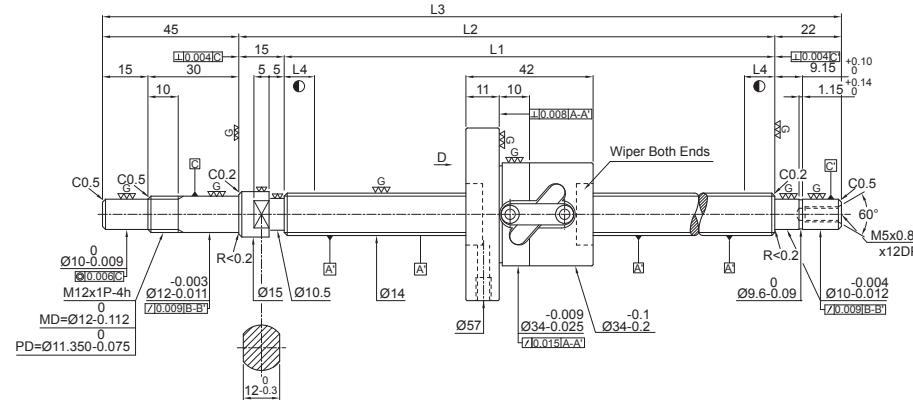


## Specification of ball screw

Production Specification	With Preload	Without Preload
Number of Thread / Thread Direction	1/Right	
BCD	12.4	
Lead	10	
Ball Dia.	2.381	
Effective Turns (Circuit × Row)	2.5 × 1	
Lead Angle	14.4	
Dynamic Rate Load Ca (kgf)	420	
Static Rate Load Co (kgf)	720	
Axial Play	0	0.005 or less
Preloading Torque (kgf-cm)	0.1~0.5	0.1 or less

Unit: mm

Model No.	Screw Spindle (Shaft) Length				Accuracy Grade	Lead Accuracy	
	L1	L2	L3	L4		Accumulated reference lead deviation E	Lead Derivation in random 300mm e <sub>300</sub>
1R12-10B1-FSWE-160-230-0.008	160	175	230	10	3	0.012	0.008
1R12-10B1-FSWE-210-280-0.008	210	225	280	10	3	0.012	0.008
1R12-10B1-FSWE-310-380-0.008	310	325	380	15	3	0.012	0.008
1R12-10B1-FSWE-410-480-0.008	410	425	480	15	3	0.013	0.008
1R12-10B1-FSWE-510-580-0.008	510	525	580	15	3	0.015	0.008

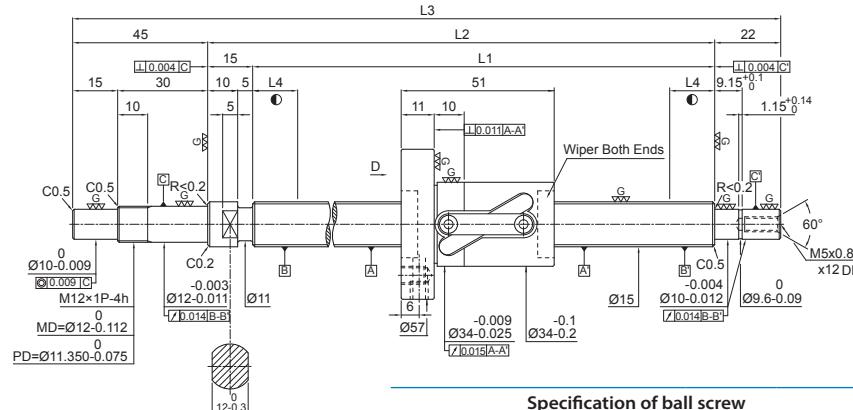


## Specification of ball screw

Production Specification	With Preload	Without Preload
Number of Thread / Thread Direction	1/Right	
BCD	14.6	
Lead	5	
Ball Dia.	3.175	
Effective Turns (Circuit × Row)	2.5 × 1	
Lead Angle	6.22	
Dynamic Rate Load Ca (kgf)	675	
Static Rate Load Co (kgf)	1145	
Axial Play	0	0.005 or less
Preloading Torque (kgf-cm)	0.15~0.7	0.2 or less

Unit: mm

Model No.	Screw Spindle (Shaft) Length				Accuracy Grade	Lead Accuracy	
	L1	L2	L3	L4		Accumulated reference lead deviation E	Lead Derivation in random 300mm e <sub>300</sub>
1R14-05B1-FSWC-189-271-0.008	189	204	271	10	3	0.012	0.008
1R14-05B1-FSWC-239-321-0.008	239	254	321	10	3	0.012	0.008
1R14-05B1-FSWC-339-421-0.008	339	954	421	15	3	0.012	0.008
1R14-05B1-FSWC-439-521-0.008	439	454	521	15	3	0.012	0.008
1R14-05B1-FSWC-539-621-0.008	539	554	621	15	3	0.012	0.008
1R14-05B1-FSWC-689-771-0.008	689	704	771	15	3	0.013	0.008

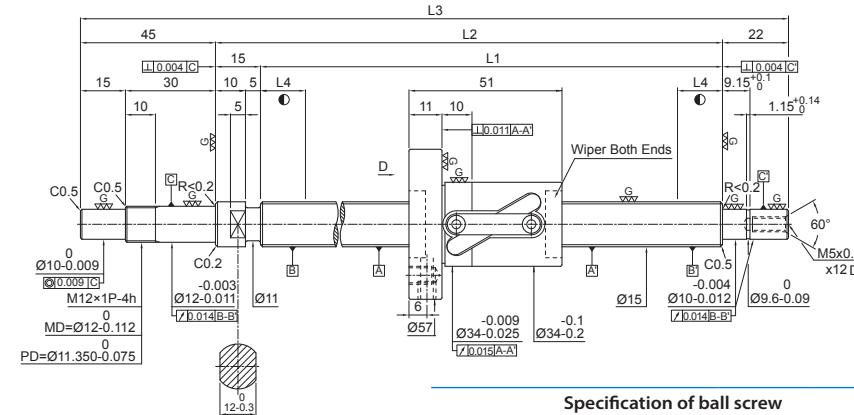


## Specification of ball screw

Production Specification	With Preload	Without Preload
Number of Thread / Thread Direction	1/Right	
BCD	15.6	
Lead	10	
Ball Dia.	3.175	
Effective Turns (Circuit x Row)	2.5 x 1	
Lead Angle	11.53	
Dynamic Rate Load Ca (kgf)	680	
Static Rate Load Co (kgf)	1210	
Axial Play	0	0.005 or less
Preloading Torque (kgf-cm)	0.1~0.79	0.24 or less

Unit: mm

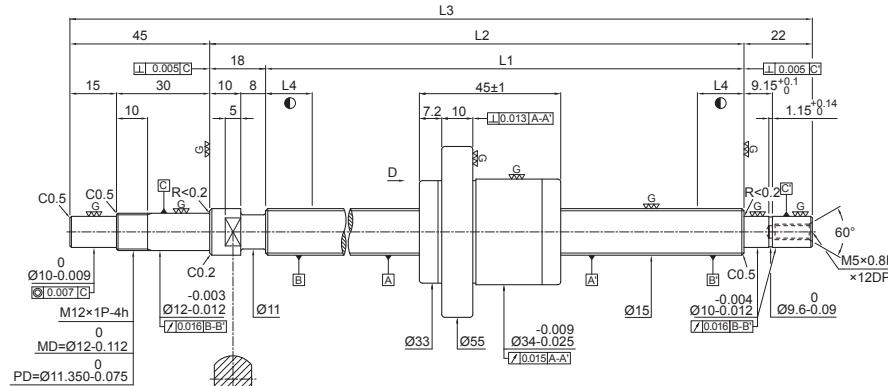
Model No.	Screw Spindle (Shaft) Length				Accuracy Grade	Lead Accuracy	
	L1	L2	L3	L4		Accumulated reference lead deviation E	Lead Derivation in random 300mm $\epsilon_{300}$
1R15-10B1-FSWC-189-271-0.018	189	201	271	10	5	0.023	0.018
1R15-10B1-FSWC-239-321-0.018	239	254	321	10	5	0.023	0.018
1R15-10B1-FSWC-289-371-0.018	289	304	371	15	5	0.023	0.018
1R15-10B1-FSWC-339-421-0.018	339	354	421	15	5	0.023	0.018
1R15-10B1-FSWC-389-471-0.018	289	404	471	15	5	0.025	0.018
1R15-10B1-FSWC-439-521-0.018	439	454	521	15	5	0.025	0.018
1R15-10B1-FSWC-489-571-0.018	489	504	571	15	5	0.027	0.018



Production Specification	With Preload	Without Preload
Number of Thread / Thread Direction	1/Right	
BCD	15.6	
Lead	10	
Ball Dia.	3.175	
Effective Turns (Circuit x Row)	2.5 x 1	
Lead Angle	11.53	
Dynamic Rate Load Ca (kgf)	680	
Static Rate Load Co (kgf)	1210	
Axial Play	0	0.005 or less
Preloading Torque (kgf-cm)	0.1~0.79	0.24 or less

Unit: mm

Model No.	Screw Spindle (Shaft) Length				Accuracy Grade	Lead Accuracy	
	L1	L2	L3	L4		Accumulated reference lead deviation E	Lead Derivation in random 300mm $\epsilon_{300}$
1R15-10B1-FSWC-539-621-0.018	539	554	621	15	5	0.027	0.018
1R15-10B1-FSWC-589-671-0.018	589	604	671	15	5	0.030	0.018
1R15-10B1-FSWC-639-721-0.018	639	654	721	15	5	0.030	0.018
1R15-10B1-FSWC-689-771-0.018	689	704	771	15	5	0.035	0.018
1R15-10B1-FSWC-789-871-0.018	789	804	871	15	5	0.035	0.018
1R15-10B1-FSWC-889-971-0.018	889	904	971	15	5	0.040	0.018
1R15-10B1-FSWC-1089-1171-0.018	1089	1104	1171	15	5	0.046	0.018

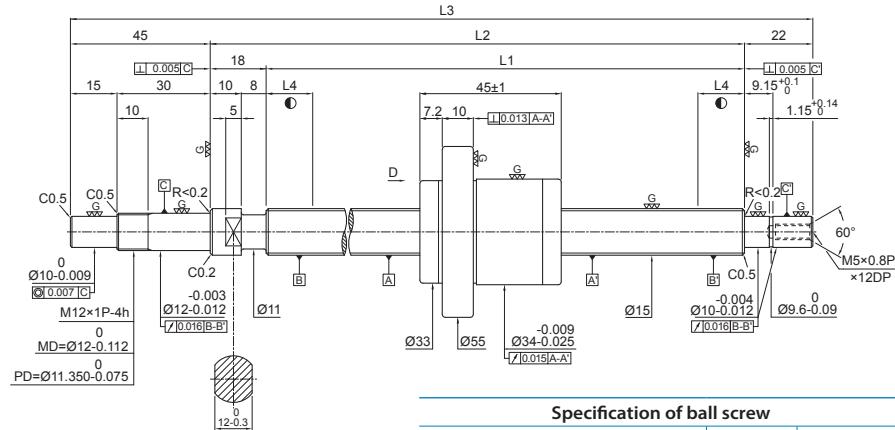


## Specification of ball screw

Production Specification	With Preload	Without Preload
Number of Thread / Thread Direction	1/Right	
BCD	15.6	
Lead	20	
Ball Dia.	3.175	
Effective Turns (Circuit × Row)	1.8 × 1	
Lead Angle	22.2	
Dynamic Rate Load Ca (kgf)	780	
Static Rate Load Co (kgf)	1400	
Axial Play	0	0.005 or less
Preloading Torque (kgf-cm)	0.15~0.8	0.24 or less

Unit: mm

Model No.	Screw Spindle (Shaft) Length				Accuracy Grade	Lead Accuracy	
	L1	L2	L3	L4		Accumulated reference lead deviation E	Lead Deriation in random 300mm e <sub>300</sub>
1R15-20A1-FSKC-186-271-0.018	186	204	271	10	5	0.023	0.018
1R15-20A1-FSKC-236-321-0.018	236	254	321	10	5	0.023	0.018
1R15-20A1-FSKC-286-371-0.018	286	304	371	15	5	0.023	0.018
1R15-20A1-FSKC-336-421-0.018	336	354	421	15	5	0.023	0.018
1R15-20A1-FSKC-386-471-0.018	386	404	471	15	5	0.025	0.018
1R15-20A1-FSKC-436-521-0.018	436	454	521	15	5	0.025	0.018
1R15-20A1-FSKC-486-571-0.018	486	504	571	15	5	0.027	0.018

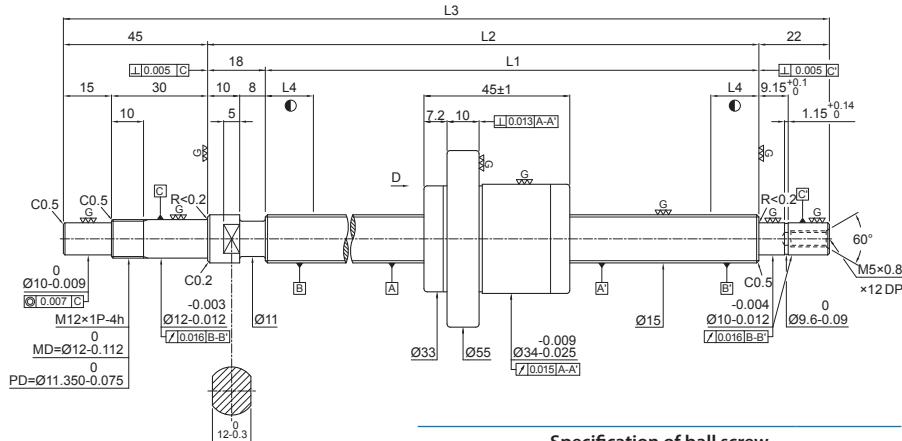


## Specification of ball screw

Production Specification	With Preload	Without Preload
Number of Thread / Thread Direction	1/Right	
BCD	15.6	
Lead	20	
Ball Dia.	3.175	
Effective Turns (Circuit × Row)	1.8 × 1	
Lead Angle	22.2	
Dynamic Rate Load Ca (kgf)	780	
Static Rate Load Co (kgf)	1400	
Axial Play	0	0.005 or less
Preloading Torque (kgf-cm)	0.15~0.8	0.24 or less

Unit: mm

Model No.	Screw Spindle (Shaft) Length				Accuracy Grade	Lead Accuracy	
	L1	L2	L3	L4		Accumulated reference lead deviation E	Lead Deriation in random 300mm e <sub>300</sub>
1R15-20A1-FSKC-536-621-0.018	536	554	621	15	5	0.027	0.018
1R15-20A1-FSKC-586-671-0.018	586	604	671	15	5	0.030	0.018
1R15-20A1-FSKC-636-721-0.018	636	654	721	15	5	0.030	0.018
1R15-20A1-FSKC-686-771-0.018	686	704	771	15	5	0.030	0.018
1R15-20A1-FSKC-786-871-0.018	786	804	871	15	5	0.035	0.018
1R15-20A1-FSKC-886-971-0.018	889	904	971	15	5	0.040	0.018
1R15-20A1-FSKC-1086-1171-0.018	1089	1104	1171	15	5	0.046	0.018

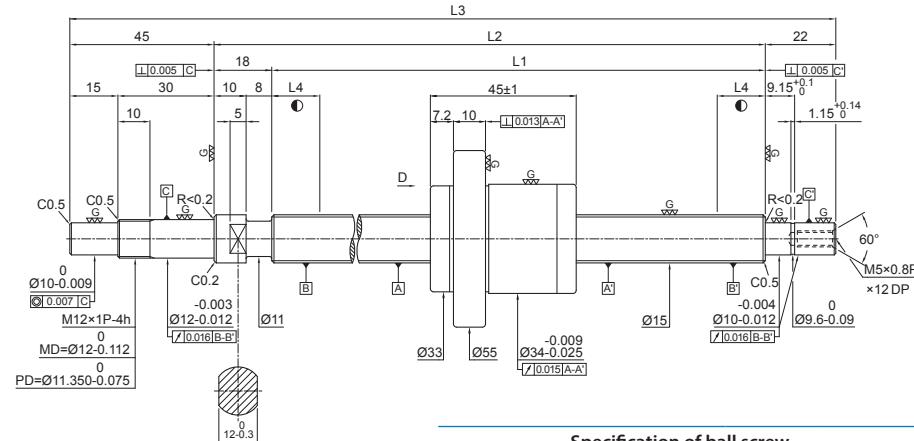


## Specification of ball screw

Production Specification	With Preload	Without Preload
Number of Thread / Thread Direction	2/Right	
BCD	15.6	
Lead	20	
Ball Dia.	3.175	
Effective Turns (Circuit x Row)	1.8 × 2	
Lead Angle	22.2	
Dynamic Rate Load Ca (kgf)	1400	
Static Rate Load Co (kgf)	2800	
Axial Play	0	0.005 or less
Preloading Torque (kgf-cm)	0.2~0.9	-

Unit: mm

Model No.	Screw Spindle (Shaft) Length				Accuracy Grade	Lead Accuracy	
	L1	L2	L3	L4		Accumulated reference lead deviation E	Lead Derivation in random 300mm e <sub>300</sub>
2R15-20A1-FSKC-236-321-0.018	236	254	321	10	5	0.023	0.018
2R15-20A1-FSKC-286-371-0.018	286	304	371	10	5	0.023	0.018
2R15-20A1-FSKC-336-421-0.018	336	354	421	15	5	0.023	0.018
2R15-20A1-FSKC-386-471-0.018	386	404	471	15	5	0.025	0.018
2R15-20A1-FSKC-436-521-0.018	436	454	521	15	5	0.025	0.018
2R15-20A1-FSKC-486-571-0.018	486	504	571	15	5	0.027	0.018

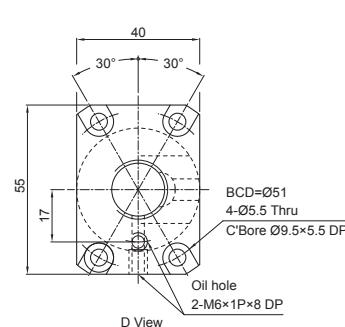
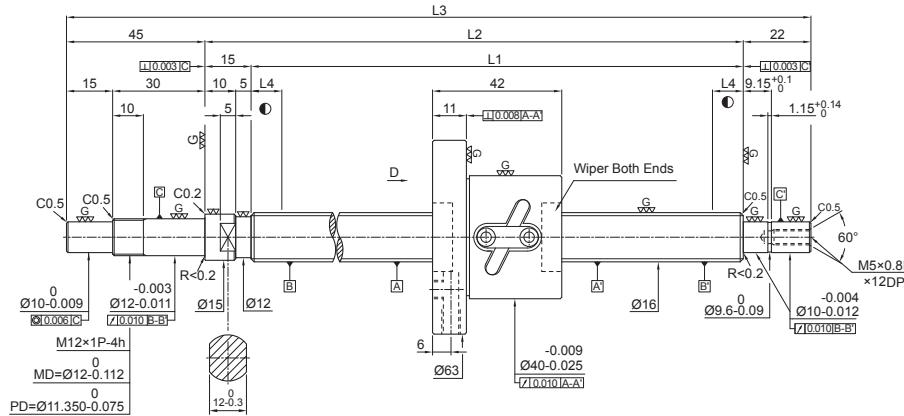


## Specification of ball screw

Production Specification	With Preload	Without Preload
Number of Thread / Thread Direction	2/Right	
BCD	15.6	
Lead	20	
Ball Dia.	3.175	
Effective Turns (Circuit x Row)	1.8 × 2	
Lead Angle	22.2	
Dynamic Rate Load Ca (kgf)	1400	
Static Rate Load Co (kgf)	2800	
Axial Play	0	0.005 or less
Preloading Torque (kgf-cm)	0.2~0.9	-



Model No.	Screw Spindle (Shaft) Length				Accuracy Grade	Lead Accuracy	
	L1	L2	L3	L4		Accumulated reference lead deviation E	Lead Derivation in random 300mm e <sub>300</sub>
2R15-20A1-FSKC-536-621-0.018	536	554	621	15	5	0.027	0.018
2R15-20A1-FSKC-586-671-0.018	586	604	671	15	5	0.030	0.018
2R15-20A1-FSKC-636-721-0.018	636	654	721	15	5	0.030	0.018
2R15-20A1-FSKC-686-771-0.018	686	704	771	15	5	0.030	0.018
2R15-20A1-FSKC-786-871-0.018	786	804	871	15	5	0.035	0.018
2R15-20A1-FSKC-886-971-0.018	886	904	971	15	5	0.040	0.018

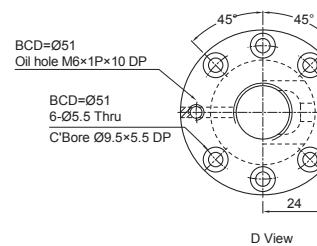
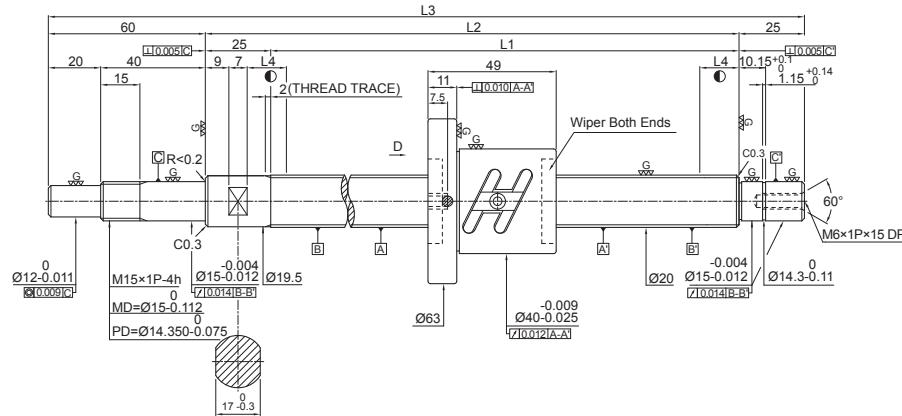


Specification of ball screw

Production Specification	With Preload	Without Preload
Number of Thread / Thread Direction	1/Right	
BCD	16.6	
Lead	5	
Ball Dia.	3.175	
Effective Turns (Circuit x Row)	2.5 x 1	
Lead Angle	5.48	
Dynamic Rate Load Ca (kgf)	690	
Static Rate Load Co (kgf)	1270	
Axial Play	0	0.005 or less
Preloading Torque (kgf-cm)	0.15~0.8	0.2 or less

Unit: mm

Model No.	Screw Spindle (Shaft) Length				Accuracy Grade	Lead Accuracy	
	L1	L2	L3	L4		Accumulated reference lead deviation E	Lead Derivation in random 300mm $e_{300}$
1R16-05B1-FSWC-189-271-0.018	189	204	271	10	5	0.023	0.018
1R16-05B1-FSWC-289-371-0.018	289	304	371	10	5	0.023	0.018
1R16-05B1-FSWC-389-471-0.018	389	404	471	15	5	0.025	0.018
1R16-05B1-FSWC-489-571-0.018	489	504	571	15	5	0.027	0.018
1R16-05B1-FSWC-689-771-0.018	689	704	771	15	5	0.035	0.018
1R16-05B1-FSWC-889-971-0.018	889	904	971	15	5	0.040	0.018

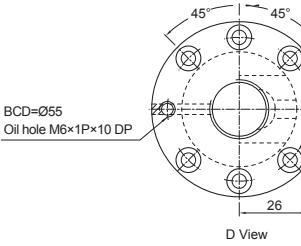
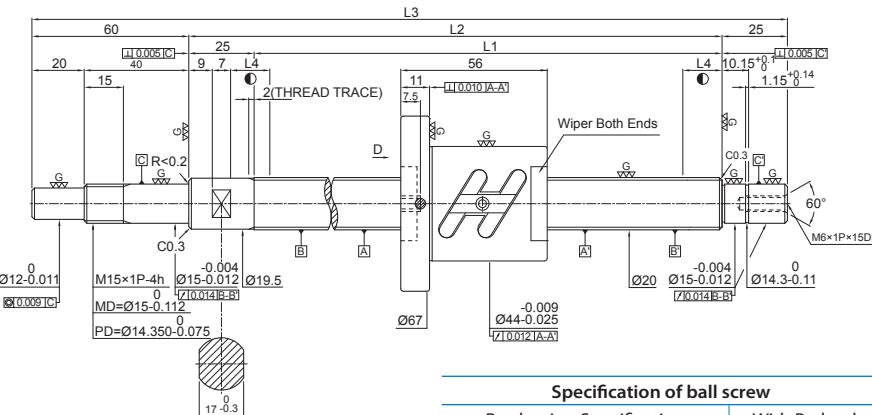


Specification of ball screw

Production Specification	With Preload
Number of Thread / Thread Direction	1/Right
BCD	20.4
Lead	4
Ball Dia.	2.381
Effective Turns (Circuit x Row)	2.5 x 2
Lead Angle	3.57
Dynamic Rate Load Ca (kgf)	820
Static Rate Load Co (kgf)	2110
Axial Play	0
Preloading Torque (kgf-cm)	0.12~0.68

Unit: mm

Model No.	Screw Spindle (Shaft) Length				Accuracy Grade	Lead Accuracy	
	L1	L2	L3	L4		Accumulated reference lead deviation E	Lead Derivation in random 300mm $e_{300}$
1R20-04B2-FSWC-225-335-0.018	225	250	335	10	5	0.023	0.018
1R20-04B2-FSWC-275-385-0.018	275	300	385	10	5	0.023	0.018
1R20-04B2-FSWC-375-485-0.018	375	400	485	15	5	0.025	0.018
1R20-04B2-FSWC-475-585-0.018	475	500	585	15	5	0.027	0.018
1R20-04B2-FSWC-575-685-0.018	575	600	685	15	5	0.030	0.018
1R20-04B2-FSWC-675-785-0.018	675	700	785	15	5	0.035	0.018

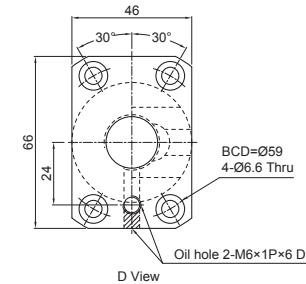
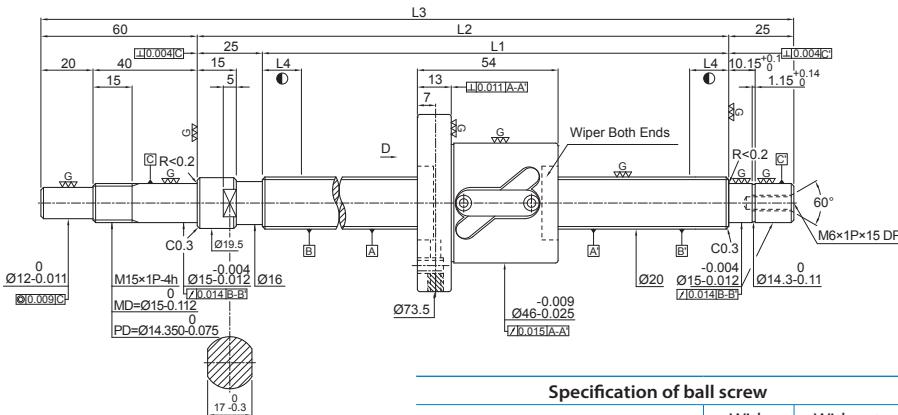


## Specification of ball screw

Production Specification	With Preload
Number of Thread / Thread Direction	1/Right
BCD	20.6
Lead	5
Ball Dia.	3.175
Effective Turns (Circuit × Row)	2.5 × 2
Lead Angle	4.42
Dynamic Rate Load Ca (kgf)	1510
Static Rate Load Co (kgf)	3460
Axial Play	0
Preloading Torque (kgf-cm)	0.28~1.32

Unit: mm

Model No.	Screw Spindle (Shaft) Length				Accuracy Grade	Lead Accuracy	
	L1	L2	L3	L4		Accumulated reference lead deviation E	Lead Derivation in random 300mm $e_{300}$
1R20-05B2-FSWC-225-335-0.018	225	250	335	10	5	0.023	0.018
1R20-05B2-FSWC-275-385-0.018	275	300	385	10	5	0.023	0.018
1R20-05B2-FSWC-375-485-0.018	375	400	485	15	5	0.025	0.018
1R20-05B2-FSWC-475-585-0.018	475	500	585	15	5	0.027	0.018
1R20-05B2-FSWC-575-685-0.018	575	600	685	15	5	0.030	0.018
1R20-05B2-FSWC-775-885-0.018	775	800	885	10	5	0.035	0.018

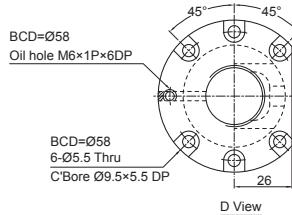
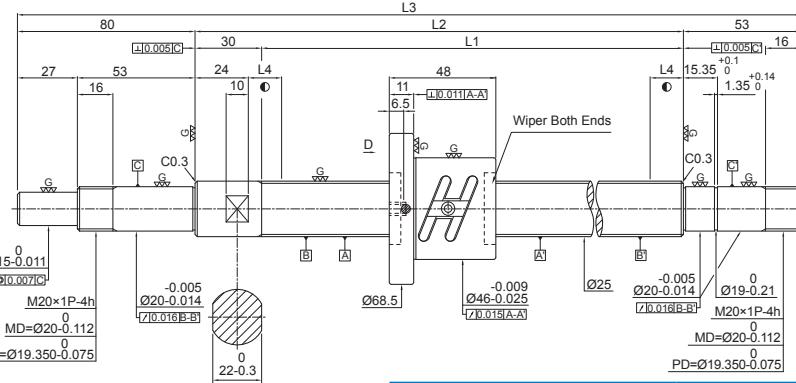


## Specification of ball screw

Production Specification	With Preload	Without Preload
Number of Thread / Thread Direction	1/Right	
BCD	20.7	
Lead	10	
Ball Dia.	3.969	
Effective Turns (Circuit × Row)	2.5 × 1	
Lead Angle	8.74	
Dynamic Rate Load Ca (kgf)	1100	
Static Rate Load Co (kgf)	2120	
Axial Play	0	0.005 or less
Preloading Torque (kgf-cm)	0.36~1.44	0.3 or less

Unit: mm

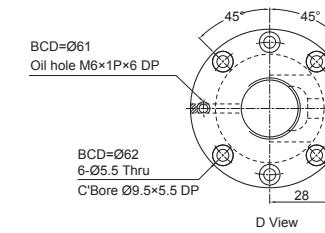
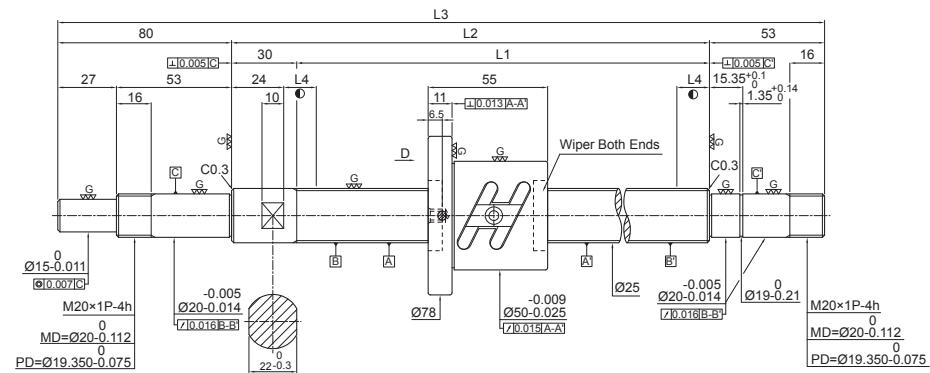
Model No.	Screw Spindle (Shaft) Length				Accuracy Grade	Lead Accuracy	
	L1	L2	L3	L4		Accumulated reference lead deviation E	Lead Derivation in random 300mm $e_{300}$
1R20-10B1-FSWC-289-399-0.018	289	314	399	10	5	0.023	0.018
1R20-10B1-FSWC-389-499-0.018	389	414	499	10	5	0.025	0.018
1R20-10B1-FSWC-489-599-0.018	489	514	599	15	5	0.027	0.018
1R20-10B1-FSWC-589-699-0.018	589	614	699	15	5	0.030	0.018
1R20-10B1-FSWC-689-799-0.018	689	714	799	15	5	0.035	0.018
1R20-10B1-FSWC-789-899-0.018	789	814	899	15	5	0.035	0.018
1R20-10B1-FSWC-889-999-0.018	889	914	999	15	5	0.040	0.018
1R20-10B1-FSWC-989-1099-0.018	989	1014	1099	15	5	0.040	0.018
1R20-10B1-FSWC-1089-1199-0.018	1089	1114	1199	15	5	0.046	0.018
1R20-10B1-FSWC-1189-1299-0.018	1189	1214	1299	15	5	0.046	0.018
1R20-10B1-FSWC-1289-1399-0.018	1289	1314	1399	15	5	0.046	0.018



Specification of ball screw	
Production Specification	With Preload
Number of Thread / Thread Direction	1/Right
BCD	25.4
Lead	4
Ball Dia.	2.381
Effective Turns (Circuit x Row)	2.5 x 2
Lead Angle	2.87
Dynamic Rate Load Ca (kgf)	930
Static Rate Load Co (kgf)	2710
Axial Play	0
Preloading Torque (kgf-cm)	0.15~0.85

Unit: mm

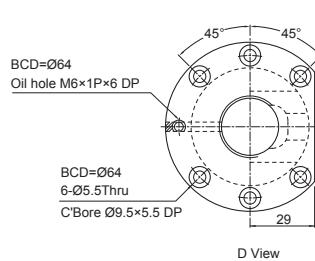
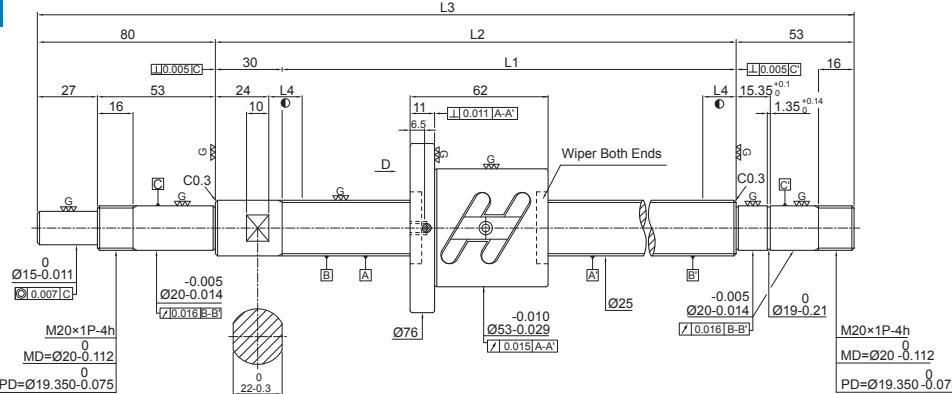
Model No.	Screw Spindle (Shaft) Length				Accuracy Grade	Lead Accuracy	
	L1	L2	L3	L4		Accumulated reference lead deviation E	Lead Derivation in random 300mm e <sub>300</sub>
1R25-04B2-FSWC-220-383-0.018	220	250	383	10	5	0.023	0.018
1R25-04B2-FSWC-270-433-0.018	270	300	433	10	5	0.023	0.018
1R25-04B2-FSWC-370-533-0.018	370	400	533	15	5	0.025	0.018
1R25-04B2-FSWC-470-633-0.018	470	500	633	15	5	0.027	0.018
1R25-04B2-FSWC-570-733-0.018	570	600	733	15	5	0.030	0.018
1R25-04B2-FSWC-770-933-0.018	770	800	933	10	5	0.035	0.018



Specification of ball screw		
Production Specification	With Preload	Without Preload
Number of Thread / Thread Direction	1/Right	1/Right
BCD	25.7	25.7
Lead	5	5
Ball Dia.	3.969	3.969
Effective Turns (Circuit x Row)	2.5 x 2	2.5 x 2
Lead Angle	3.54	3.54
Dynamic Rate Load Ca (kgf)	1100	1100
Static Rate Load Co (kgf)	2120	2120
Axial Play	0	0.005 or less
Preloading Torque (kgf-cm)	0.36~1.44	0.3 or less

Unit: mm

Model No.	Screw Spindle (Shaft) Length				Accuracy Grade	Lead Accuracy	
	L1	L2	L3	L4		Accumulated reference lead deviation E	Lead Derivation in random 300mm e <sub>300</sub>
1R25-05B2-FSWC-220-383-0.018	220	250	383	10	5	0.023	0.018
1R25-05B2-FSWC-270-433-0.018	270	300	433	10	5	0.023	0.018
1R25-05B2-FSWC-370-533-0.018	370	400	533	15	5	0.025	0.018
1R25-05B2-FSWC-470-633-0.018	470	500	633	15	5	0.027	0.018
1R25-05B2-FSWC-570-733-0.018	570	600	733	15	5	0.030	0.018
1R25-05B2-FSWC-670-833-0.018	670	700	833	15	5	0.030	0.018
1R25-05B2-FSWC-770-933-0.018	770	800	933	15	5	0.035	0.018
1R25-05B2-FSWC-970-1133-0.018	970	1000	1133	15	5	0.040	0.018
1R25-05B2-FSWC-1170-1333-0.018	1170	1200	1333	15	5	0.046	0.018

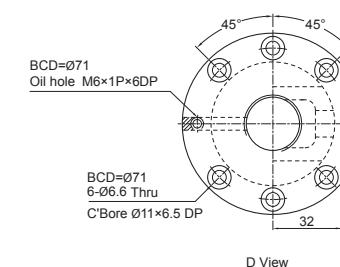
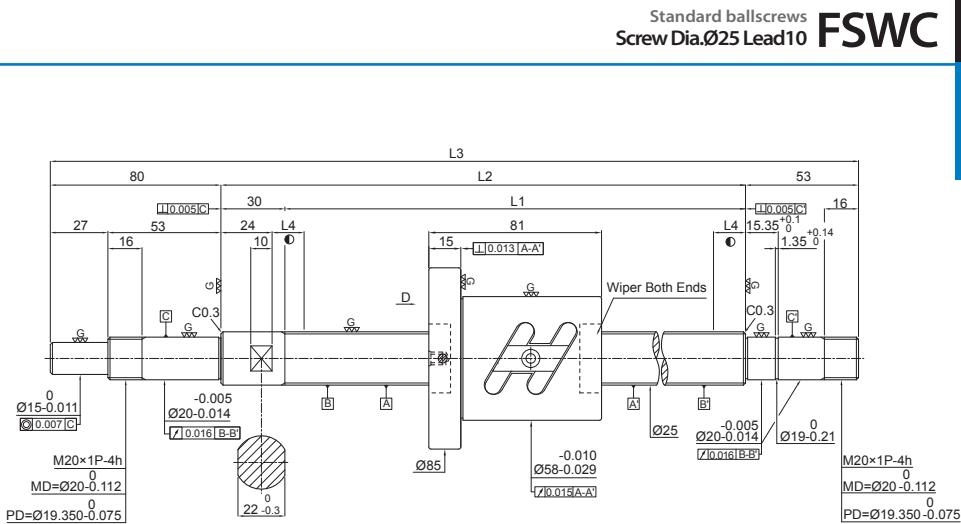
**FSWC** Standard ballscrews  
Screw Dia. Ø25 Lead06


## Specification of ball screw

Production Specification		With Preload
Number of Thread / Thread Direction	1/Right	
BCD	25.7	
Lead	6	
Ball Dia.	3.969	
Effective Turns (Circuit x Row)	2.5 x 2	
Lead Angle	4.25	
Dynamic Rate Load Ca (kgf)	2190	
Static Rate Load Co (kgf)	5360	
Axial Play	0	
Preloading Torque (kgf-cm)	0.42~2.4	

Unit: mm

Model No.	Screw Spindle (Shaft) Length				Accuracy Grade	Lead Accuracy	
	L1	L2	L3	L4		Accumulated reference lead deviation E	Lead Derivation in random 300mm e <sub>300</sub>
1R25-06B2-FSWC-370-533-0.018	370	400	533	15	5	0.025	0.018
1R25-06B2-FSWC-570-733-0.018	570	600	733	15	5	0.030	0.018
1R25-06B2-FSWC-770-933-0.018	770	800	933	15	5	0.035	0.018
1R25-06B2-FSWC-1170-1333-0.018	1170	1200	1333	15	5	0.046	0.018



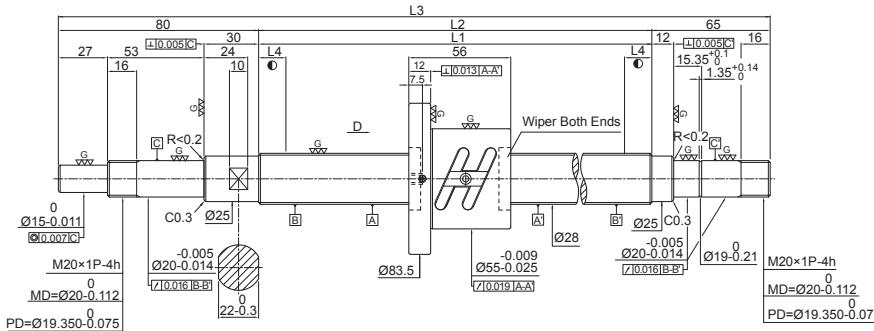
## Specification of ball screw

Production Specification		With Preload
Number of Thread / Thread Direction	1/Right	
BCD	26	
Lead	10	
Ball Dia.	4.762	
Effective Turns (Circuit x Row)	1.5 x 2	
Lead Angle	6.98	
Dynamic Rate Load Ca (kgf)	1820	
Static Rate Load Co (kgf)	3840	
Axial Play	0	
Preloading Torque (kgf-cm)	0.42~2.4	

Unit: mm

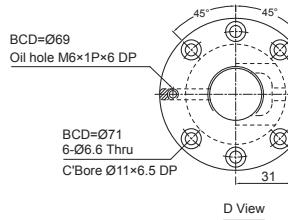
Model No.	Screw Spindle (Shaft) Length				Accuracy Grade	Lead Accuracy	
	L1	L2	L3	L4		Accumulated reference lead deviation E	Lead Derivation in random 300mm e <sub>300</sub>
1R25-10A2-FSWC-370-533-0.018	370	400	533	10	5	0.025	0.018
1R25-10A2-FSWC-570-733-0.018	570	600	733	10	5	0.030	0.018
1R25-10A2-FSWC-770-933-0.018	770	800	933	15	5	0.035	0.018
1R25-10A2-FSWC-970-1133-0.018	970	1000	1133	15	5	0.040	0.018
1R25-10A2-FSWC-1170-1333-0.018	1170	1200	1333	15	5	0.046	0.018
1R25-10A2-FSWC-1470-1600-0.018	1470	1500	1633	15	5	0.054	0.018

**FSWC** Standard ballscrews  
Screw Dia. Ø25 Lead10



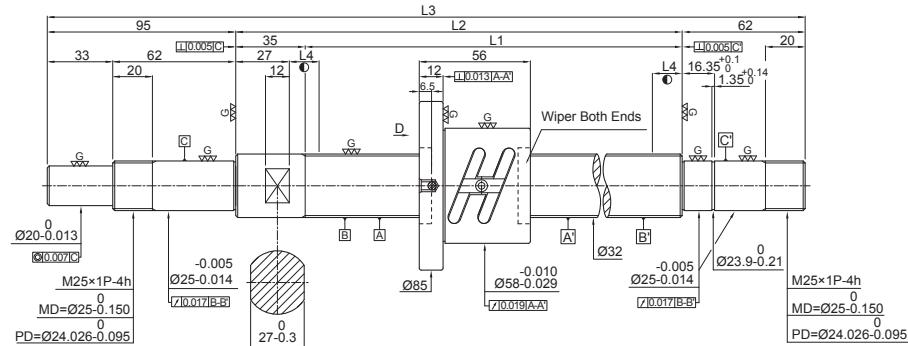
## Specification of ball screw

Production Specification		With Preload
Number of Thread / Thread Direction		1/Right
BCD		28.6
Lead		5
Ball Dia.		3.175
Effective Turns (Circuit × Row)		2.5 × 2
Lead Angle		3.19
Dynamic Rate Load Ca (kgf)		1720
Static Rate Load Co (kgf)		4940
Axial Play		0
Preloading Torque (kgf-cm)		0.3~1.7



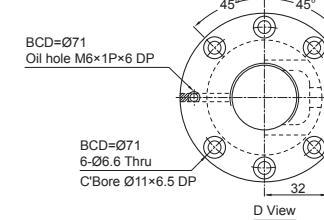
Unit: mm

Model No.	Screw Spindle (Shaft) Length				Accuracy Grade	Lead Accuracy	
	L1	L2	L3	L4		Accumulated reference lead deviation E	Lead Derivation in random 300mm e <sub>300</sub>
1R28-05B2-FSWC-270-445-0.018	270	300	445	10	5	0.023	0.018
1R28-05B2-FSWC-370-545-0.018	370	400	545	15	5	0.023	0.018
1R28-05B2-FSWC-470-645-0.018	470	500	645	15	5	0.023	0.018
1R28-05B2-FSWC-558-733-0.018	558	588	733	15	5	0.023	0.018
1R28-05B2-FSWC-758-933-0.018	758	788	933	15	5	0.025	0.018
1R28-05B2-FSWC-958-1133-0.018	958	988	1133	15	5	0.025	0.018
1R28-05B2-FSWC-1158-1333-0.018	1158	1188	1333	15	5	0.027	0.018



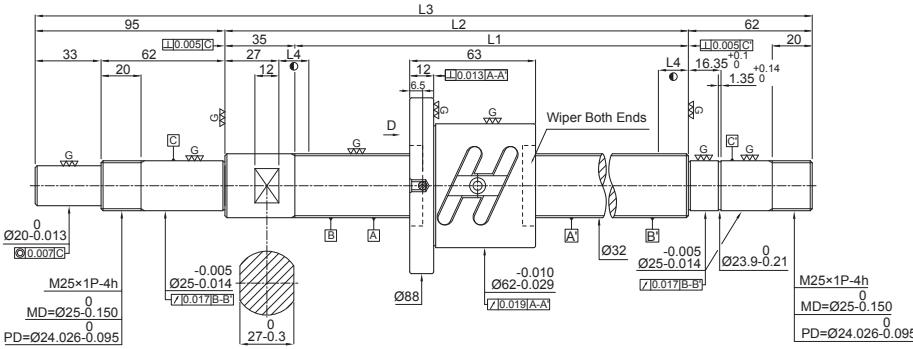
## Specification of ball screw

Production Specification		With Preload
Number of Thread / Thread Direction		1/Right
BCD		32.6
Lead		5
Ball Dia.		3.175
Effective Turns (Circuit × Row)		2.5 × 2
Lead Angle		2.79
Dynamic Rate Load Ca (kgf)		1830
Static Rate Load Co (kgf)		5680
Axial Play		0
Preloading Torque (kgf-cm)		0.48~1.92



Unit: mm

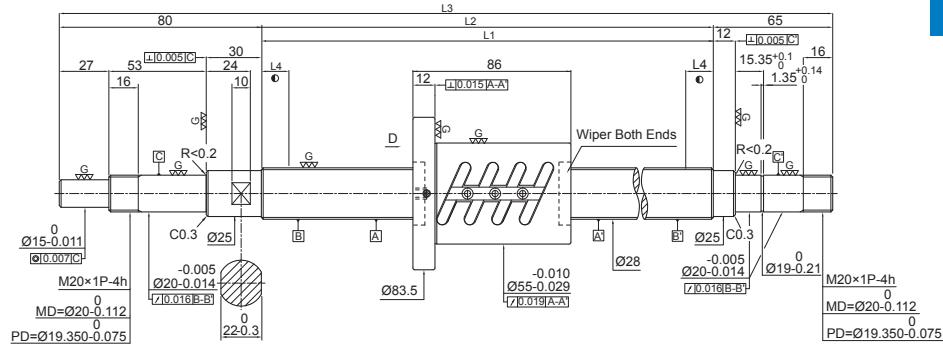
Model No.	Screw Spindle (Shaft) Length				Accuracy Grade	Lead Accuracy	
	L1	L2	L3	L4		Accumulated reference lead deviation E	Lead Derivation in random 300mm e <sub>300</sub>
1R32-05B2-FSWC-265-457-0.018	265	300	457	10	5	0.023	0.018
1R32-05B2-FSWC-365-557-0.018	365	400	557	15	5	0.025	0.018
1R32-05B2-FSWC-465-657-0.018	465	500	657	15	5	0.027	0.018
1R32-05B2-FSWC-565-757-0.018	565	600	757	15	5	0.030	0.018
1R32-05B2-FSWC-665-857-0.018	665	700	857	15	5	0.030	0.018
1R32-05B2-FSWC-765-957-0.018	765	800	957	15	5	0.035	0.018
1R32-05B2-FSWC-965-1157-0.018	965	1000	1157	15	5	0.040	0.018
1R32-05B2-FSWC-1165-1357-0.018	1165	1200	1357	15	5	0.046	0.018
1R32-05B2-FSWC-1465-1657-0.018	1465	1500	1657	15	5	0.054	0.018

**FSWC** Standard ballscrews  
Screw Dia. Ø32 Lead06


Specification of ball screw		
Production Specification		With Preload
Number of Thread / Thread Direction	1/Right	
BCD	32.7	
Lead	6	
Ball Dia.	3.969	
Effective Turns (Circuit x Row)	2.5 x 2	
Lead Angle	3.34	
Dynamic Rate Load Ca (kgf)	2410	
Static Rate Load Co (kgf)	6900	
Axial Play	0	
Preloading Torque (kgf-cm)	0.48~2.72	

Unit: mm

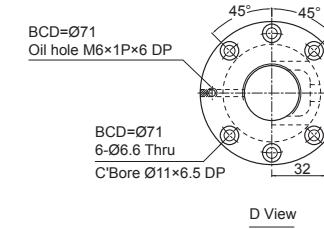
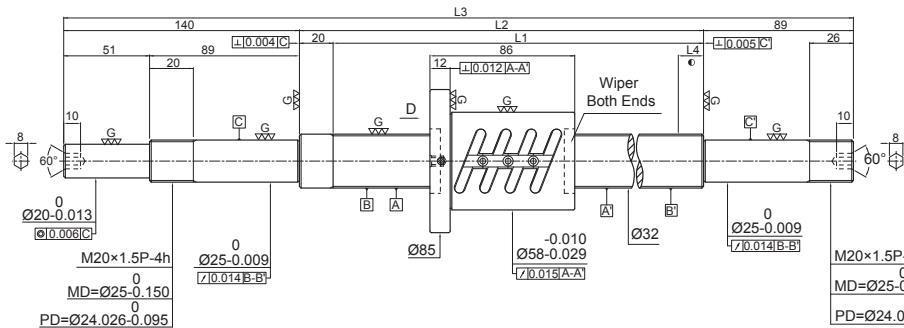
Model No.	Screw Spindle (Shaft) Length				Accuracy Grade	Lead Accuracy	
	L1	L2	L3	L4		Accumulated reference lead deviation E	Lead Derivation in random 300mm $e_{300}$
1R32-06B2-FSWC-365-557-0.018	365	400	557	15	5	0.025	0.018
1R32-06B2-FSWC-565-757-0.018	565	600	757	15	5	0.030	0.018
1R32-06B2-FSWC-765-957-0.018	765	800	957	15	5	0.035	0.018
1R32-06B2-FSWC-965-1157-0.018	965	1000	1157	15	5	0.040	0.018
1R32-06B2-FSWC-1165-1357-0.018	1165	1200	1357	15	5	0.046	0.018
1R32-06B2-FSWC-1465-1657-0.018	1465	1500	1657	15	5	0.054	0.018

**FOWC** Standard ballscrews  
Screw Dia. Ø28 Lead05


Specification of ball screw		
Production Specification		With Preload
Number of Thread / Thread Direction	1/Right	
BCD	28.6	
Lead	5	
Ball Dia.	3.175	
Effective Turns (Circuit x Row)	2.5 x 2(2)	
Lead Angle	3.19	
Dynamic Rate Load Ca (kgf)	1720	
Static Rate Load Co (kgf)	4940	
Axial Play	0	
Preloading Torque (kgf-cm)	1.1~3.3	

Unit: mm

Model No.	Screw Spindle (Shaft) Length				Accuracy Grade	Lead Accuracy	
	L1	L2	L3	L4		Accumulated reference lead deviation E	Lead Derivation in random 300mm $e_{300}$
1R28-05B1-FOWC-270-445-0.018	270	312	445	10	5	0.023	0.018
1R28-05B1-FOWC-370-545-0.018	370	412	545	15	5	0.025	0.018
1R28-05B1-FOWC-470-645-0.018	470	512	645	15	5	0.027	0.018
1R28-05B1-FOWC-558-733-0.018	558	600	733	15	5	0.030	0.018
1R28-05B1-FOWC-758-933-0.018	758	800	933	15	5	0.035	0.018
1R28-05B1-FOWC-958-1133-0.018	958	1000	1133	15	5	0.040	0.018
1R28-05B1-FOWC-1158-1333-0.018	1158	1200	1333	15	5	0.046	0.018

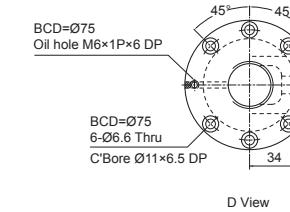
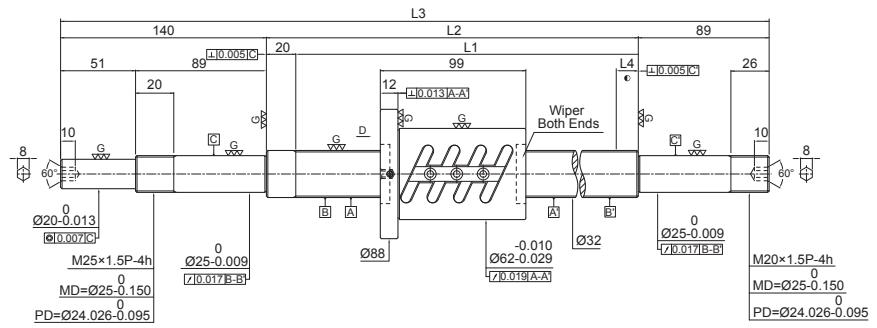
**FOWC** Standard ballscrews  
Screw Dia. Ø32 Lead05


## Specification of ball screw

Production Specification	With Preload
Number of Thread / Thread Direction	1/Right
BCD	32.6
Lead	5
Ball Dia.	3.175
Effective Turns (Circuit × Row)	2.5 × 2(2)
Lead Angle	2.79
Dynamic Rate Load Ca (kgf)	1830
Static Rate Load Co (kgf)	5680
Axial Play	0
Preloading Torque (kgf-cm)	1.2~3.6

Unit: mm

Model No.	Screw Spindle (Shaft) Length				Accuracy Grade	Lead Accuracy	
	L1	L2	L3	L4		Accumulated reference lead deviation E	Lead Deviation in random 300mm e <sub>300</sub>
1R32-05B1-FOWC-280-529-0.018	280	300	529	10	5	0.023	0.018
1R32-05B1-FOWC-380-629-0.018	380	400	629	15	5	0.025	0.018
1R32-05B1-FOWC-480-729-0.018	480	500	729	15	5	0.027	0.018
1R32-05B1-FOWC-580-829-0.018	580	600	829	15	5	0.030	0.018
1R32-05B1-FOWC-680-929-0.018	680	700	929	15	5	0.035	0.018
1R32-05B1-FOWC-780-1029-0.018	780	800	1029	15	5	0.035	0.018
1R32-05B1-FOWC-980-1229-0.018	980	1000	1229	15	5	0.040	0.018
1R32-05B1-FOWC-1180-1429-0.018	1180	1200	1429	15	5	0.046	0.018
1R32-05B1-FOWC-1480-1729-0.018	1480	1500	1729	15	5	0.054	0.018

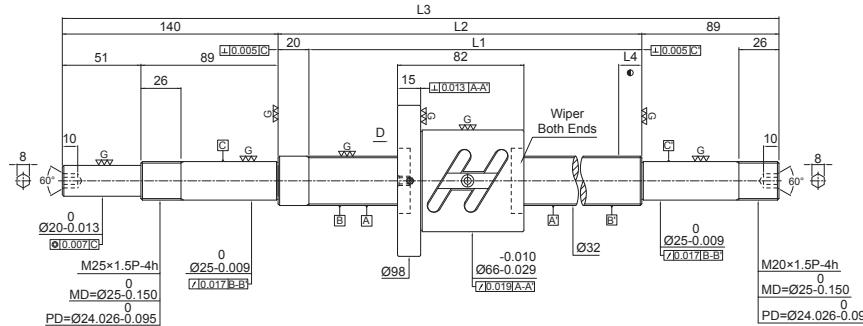
**FOWC** Standard ballscrews  
Screw Dia. Ø32 Lead06


## Specification of ball screw

Production Specification	With Preload
Number of Thread / Thread Direction	1/Right
BCD	32.7
Lead	6
Ball Dia.	3.969
Effective Turns (Circuit × Row)	2.5 × 2(2)
Lead Angle	3.34
Dynamic Rate Load Ca (kgf)	2410
Static Rate Load Co (kgf)	6900
Axial Play	0
Preloading Torque (kgf-cm)	2.32~4.82

Unit: mm

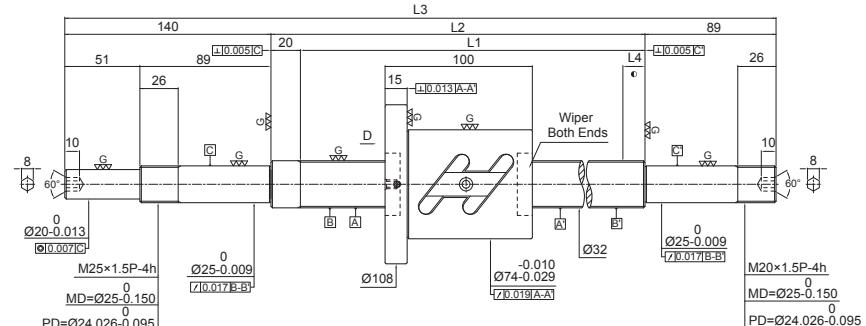
Model No.	Screw Spindle (Shaft) Length				Accuracy Grade	Lead Accuracy	
	L1	L2	L3	L4		Accumulated reference lead deviation E	Lead Deviation in random 300mm e <sub>300</sub>
1R32-06B1-FOWC-380-629-0.018	380	400	629	15	5	0.025	0.018
1R32-06B1-FOWC-580-829-0.018	580	600	829	15	5	0.030	0.018
1R32-06B1-FOWC-780-1029-0.018	780	800	1029	15	5	0.035	0.018
1R32-06B1-FOWC-980-1229-0.018	980	1000	1229	15	5	0.040	0.018
1R32-06B1-FOWC-1180-1429-0.018	1180	1200	1429	15	5	0.046	0.018
1R32-06B1-FOWC-1480-1729-0.018	1480	1500	1729	15	5	0.054	0.018

**FOWC** Standard ballscrews  
Screw Dia. Ø32 Lead8


Specification of ball screw	
Production Specification	With Preload
Number of Thread / Thread Direction	1/Right
BCD	33
Lead	8
Ball Dia.	4.762
Effective Turns (Circuit x Row)	2.5 x 1(2)
Lead Angle	4.41
Dynamic Rate Load Ca (kgf)	1720
Static Rate Load Co (kgf)	4180
Axial Play	0
Preloading Torque (kgf-cm)	1.26~5.06

Unit: mm

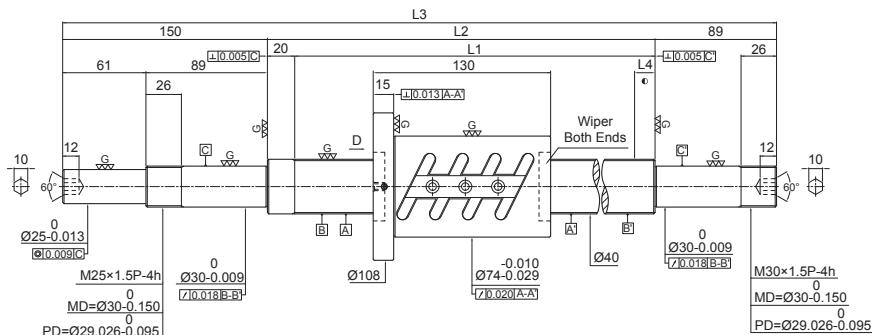
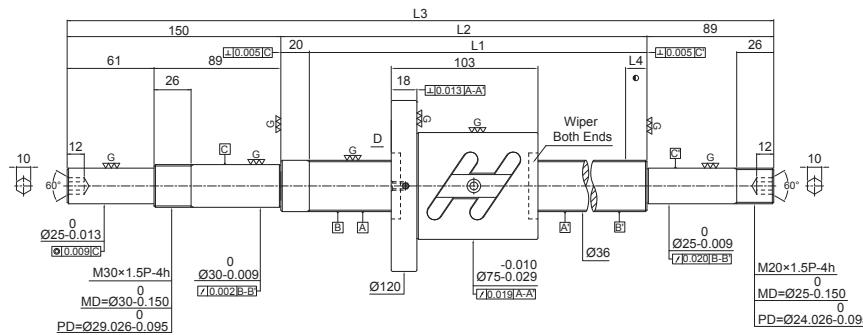
Model No.	Screw Spindle (Shaft) Length				Accuracy Grade	Lead Accuracy	
	L1	L2	L3	L4		Accumulated reference lead deviation E	Lead Derivation in random 300mm $e_{300}$
1R32-08B1-FOWC-380-629-0.018	380	400	629	15	5	0.025	0.018
1R32-08B1-FOWC-580-829-0.018	580	600	829	15	5	0.030	0.018
1R32-08B1-FOWC-780-1029-0.018	780	800	1029	15	5	0.035	0.018
1R32-08B1-FOWC-980-1229-0.018	980	1000	1229	15	5	0.040	0.018
1R32-08B1-FOWC-1480-1729-0.018	1480	1500	1729	15	5	0.054	0.018

**FOWC** Standard ballscrews  
Screw Dia. Ø32 Lead10


Specification of ball screw	
Production Specification	With Preload
Number of Thread / Thread Direction	1/Right
BCD	33.4
Lead	10
Ball Dia.	6.35
Effective Turns (Circuit x Row)	2.5 x 1(2)
Lead Angle	5.44
Dynamic Rate Load Ca (kgf)	2570
Static Rate Load Co (kgf)	5440
Axial Play	0
Preloading Torque (kgf-cm)	3.58~7.44

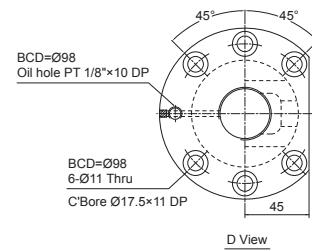
Unit: mm

Model No.	Screw Spindle (Shaft) Length				Accuracy Grade	Lead Accuracy	
	L1	L2	L3	L4		Accumulated reference lead deviation E	Lead Derivation in random 300mm $e_{300}$
1R32-10B1-FOWC-380-629-0.018	380	400	629	15	5	0.025	0.018
1R32-10B1-FOWC-480-729-0.018	480	500	729	15	5	0.027	0.018
1R32-10B1-FOWC-580-829-0.018	580	600	829	15	5	0.030	0.018
1R32-10B1-FOWC-680-929-0.018	680	700	929	15	5	0.030	0.018
1R32-10B1-FOWC-780-1029-0.018	780	800	1029	15	5	0.035	0.018
1R32-10B1-FOWC-980-1229-0.018	980	1000	1229	15	5	0.040	0.018
1R32-10B1-FOWC-1180-1429-0.018	1180	1200	1429	15	5	0.046	0.018
1R32-10B1-FOWC-1480-1729-0.018	1480	1500	1729	15	5	0.054	0.018
1R32-10B1-FOWC-1780-2029-0.018	1780	1800	2029	15	5	0.065	0.018

**FOWC** Standard ballscrews  
Screw Dia. Ø36 Lead10


## Specification of ball screw

Production Specification	With Preload
Number of Thread / Thread Direction	1/Right
BCD	37.4
Lead	10
Ball Dia.	6.35
Effective Turns (Circuit × Row)	2.5 × 1(2)
Lead Angle	4.86
Dynamic Rate Load Ca (kgf)	2720
Static Rate Load Co (kgf)	6180
Axial Play	0
Preloading Torque (kgf-cm)	3.91~8.13

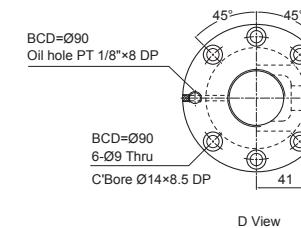


Unit: mm

Model No.	Screw Spindle (Shaft) Length				Accuracy Grade	Lead Accuracy	
	L1	L2	L3	L4		Accumulated reference lead deviation E	Lead Derivation in random 300mm e <sub>300</sub>
1R36-10B1-FOWC-480-739-0.018	480	500	739	15	5	0.027	0.018
1R36-10B1-FOWC-680-939-0.018	680	700	939	15	5	0.030	0.018
1R36-10B1-FOWC-980-1239-0.018	980	1000	1239	15	5	0.040	0.018
1R36-10B1-FOWC-1380-1639-0.018	1380	1400	1639	15	5	0.054	0.018
1R36-10B1-FOWC-1780-2039-0.018	1780	1800	2039	15	5	0.065	0.018

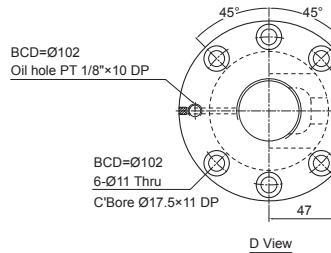
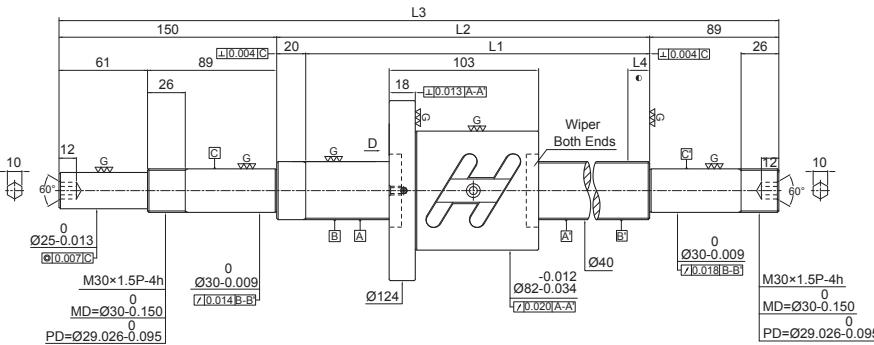
**FOWC** Standard ballscrews  
Screw Dia. Ø40 Lead08

Production Specification	With Preload
Number of Thread / Thread Direction	1/Right
BCD	41
Lead	8
Ball Dia.	4.762
Effective Turns (Circuit × Row)	2.5 × 2(2)
Lead Angle	3.55
Dynamic Rate Load Ca (kgf)	3450
Static Rate Load Co (kgf)	10540
Axial Play	0
Preloading Torque (kgf-cm)	4.24~8.82



Unit: mm

Model No.	Screw Spindle (Shaft) Length				Accuracy Grade	Lead Accuracy	
	L1	L2	L3	L4		Accumulated reference lead deviation E	Lead Derivation in random 300mm e <sub>300</sub>
1R40-8B2-FOWC-380-639-0.018	380	400	639	15	5	0.025	0.018
1R40-8B2-FOWC-580-839-0.018	580	600	839	15	5	0.030	0.018
1R40-8B2-FOWC-780-1039-0.018	780	800	1039	15	5	0.035	0.018
1R40-8B2-FOWC-980-1239-0.018	980	1000	1239	15	5	0.040	0.018
1R40-8B2-FOWC-1180-1439-0.018	1180	1200	1439	15	5	0.046	0.018
1R40-8B2-FOWC-1580-1839-0.018	1580	1600	1839	15	5	0.054	0.018

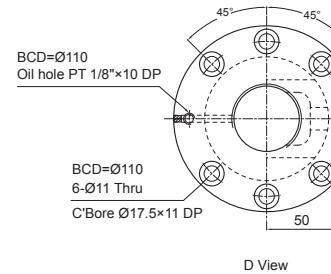
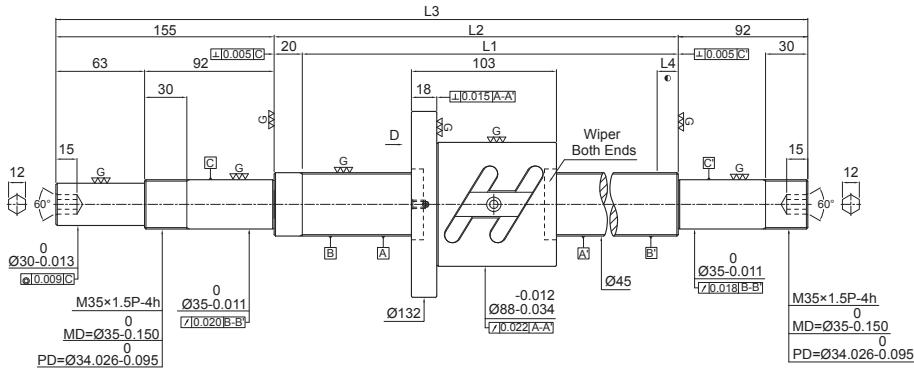
**FOWC** Standard ballscrews  
Screw Dia. Ø40 Lead10


## Specification of ball screw

Production Specification		With Preload
Number of Thread / Thread Direction	1/Right	
BCD	41.4	
Lead	10	
Ball Dia.	6.35	
Effective Turns (Circuit x Row)	2.5 x 1(2)	
Lead Angle	4.4	
Dynamic Rate Load Ca (kgf)	2880	
Static Rate Load Co (kgf)	6950	
Axial Play	0	
Preloading Torque (kgf-cm)	4.57~8.49	

Unit: mm

Model No.	Screw Spindle (Shaft) Length				Accuracy Grade	Lead Accuracy	
	L1	L2	L3	L4		Accumulated reference lead deviation E	Lead Derivation in random 300mm e <sub>300</sub>
1R40-10B1-FOWC-480-739-0.018	480	500	739	15	5	0.027	0.018
1R40-10B1-FOWC-580-839-0.018	580	600	839	15	5	0.030	0.018
1R40-10B1-FOWC-680-939-0.018	680	700	939	15	5	0.030	0.018
1R40-10B1-FOWC-780-1039-0.018	780	800	1039	15	5	0.035	0.018
1R40-10B1-FOWC-980-1239-0.018	980	1000	1239	15	5	0.040	0.018
1R40-10B1-FOWC-1180-1439-0.018	1180	1200	1439	15	5	0.046	0.018
1R40-10B1-FOWC-1380-1639-0.018	1380	1400	1639	15	5	0.054	0.018
1R40-10B1-FOWC-1580-1839-0.018	1580	1600	1839	15	5	0.054	0.018
1R40-10B1-FOWC-1780-2039-0.018	1780	1800	2039	15	5	0.065	0.018
1R40-10B1-FOWC-2380-2639-0.018	2380	2400	2639	15	5	0.077	0.018

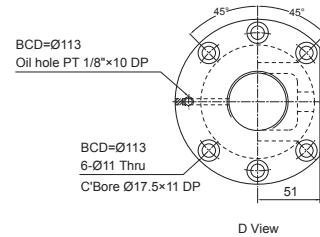
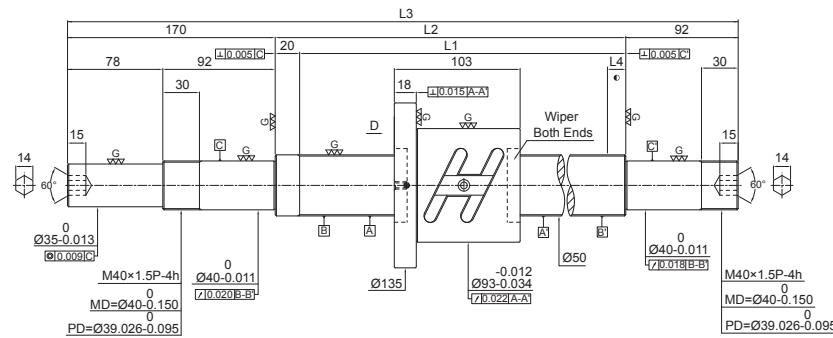

**FOWC** Standard ballscrews  
Screw Dia. Ø45 Lead10

## Specification of ball screw

Production Specification		With Preload
Number of Thread / Thread Direction	1/Right	
BCD	46.4	
Lead	10	
Ball Dia.	6.35	
Effective Turns (Circuit x Row)	2.5 x 1(2)	
Lead Angle	4.4	
Dynamic Rate Load Ca (kgf)	3020	
Static Rate Load Co (kgf)	7850	
Axial Play	0	
Preloading Torque (kgf-cm)	4.58~9.5	

Unit: mm

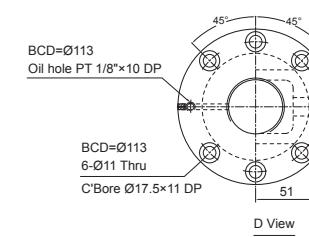
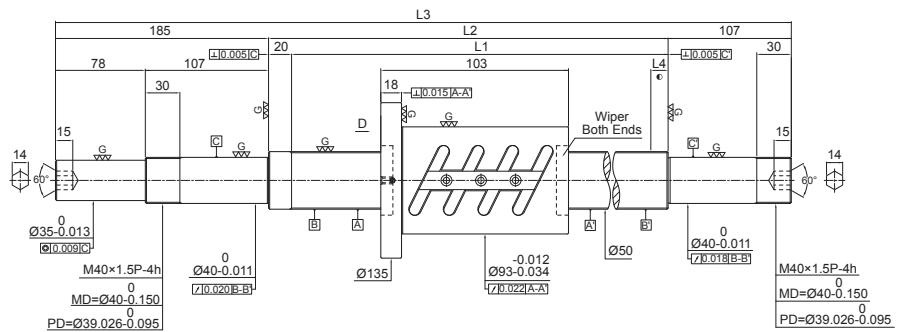
Model No.	Screw Spindle (Shaft) Length				Accuracy Grade	Lead Accuracy	
	L1	L2	L3	L4		Accumulated reference lead deviation E	Lead Derivation in random 300mm e <sub>300</sub>
1R45-10B1-1FOWC-680-947-0.018	680	700	947	15	5	0.035	0.018
1R45-10B1-1FOWC-980-1247-0.018	980	1000	1247	15	5	0.04	0.018
1R45-10B1-1FOWC-1380-1647-0.018	1380	1400	1647	15	5	0.054	0.018
1R45-10B1-1FOWC-1780-2047-0.018	1780	1800	2047	15	5	0.065	0.018
1R45-10B1-1FOWC-2480-2747-0.018	2480	2500	2747	15	5	0.077	0.018



Specification of ball screw	
Production Specification	With Preload
Number of Thread / Thread Direction	1/Right
BCD	51.4
Lead	10
Ball Dia.	6.35
Effective Turns (Circuit × Row)	2.5 × 1(2)
Lead Angle	3.54
Dynamic Rate Load Ca (kgf)	3190
Static Rate Load Co (kgf)	8710
Axial Play	0
Preloading Torque (kgf-cm)	4.84~11.28

Unit: mm

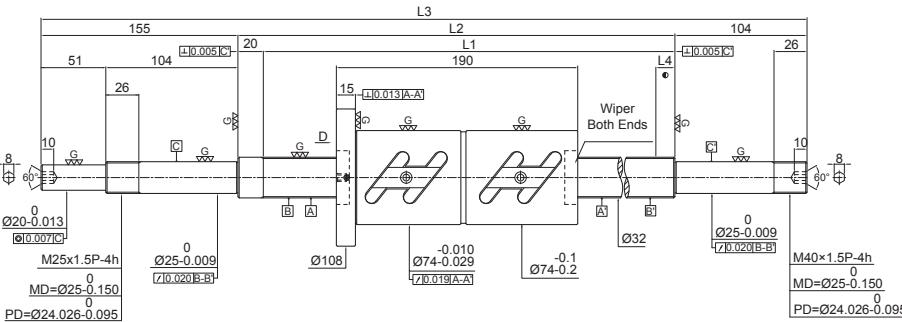
Model No.	Screw Spindle (Shaft) Length				Accuracy Grade	Lead Accuracy	
	L1	L2	L3	L4		Accumulated reference lead deviation E	Lead Deriation in random 300mm $e_{300}$
1R50-10B1-FOWC-580-892-0.018	580	600	892	15	5	0.030	0.018
1R50-10B1-FOWC-780-1092-0.018	780	800	1092	15	5	0.035	0.018
1R50-10B1-FOWC-980-1292-0.018	980	1000	1292	15	5	0.040	0.018
1R50-10B1-FOWC-1180-1492-0.018	1180	1200	1492	15	5	0.046	0.018
1R50-10B1-FOWC-1480-1792-0.018	1480	1500	1792	15	5	0.054	0.018
1R50-10B1-FOWC-1980-2292-0.018	1980	2000	2292	15	5	0.065	0.018
1R50-10B1-FOWC-2580-2892-0.018	2580	2600	2892	15	5	0.093	0.018



Specification of ball screw	
Production Specification	With Preload
Number of Thread / Thread Direction	1/Right
BCD	51.4
Lead	10
Ball Dia.	6.35
Effective Turns (Circuit × Row)	2.5 × 2(2)
Lead Angle	3.54
Dynamic Rate Load Ca (kgf)	5790
Static Rate Load Co (kgf)	17420
Axial Play	0
Preloading Torque (kgf-cm)	10.48~17.48

Unit: mm

Model No.	Screw Spindle (Shaft) Length				Accuracy Grade	Lead Accuracy	
	L1	L2	L3	L4		Accumulated reference lead deviation E	Lead Deriation in random 300mm $e_{300}$
1R50-10B2-FOWC-580-892-0.018	580	600	892	15	5	0.030	0.018
1R50-10B2-FOWC-780-1092-0.018	780	800	1092	15	5	0.035	0.018
1R50-10B2-FOWC-980-1292-0.018	980	1000	1292	15	5	0.040	0.018
1R50-10B2-FOWC-1180-1492-0.018	1180	1200	1492	15	5	0.046	0.018
1R50-10B2-FOWC-1480-1792-0.018	1480	1500	1792	15	5	0.054	0.018
1R50-10B2-FOWC-1980-2292-0.018	1980	2000	2292	15	5	0.065	0.018
1R50-10B2-FOWC-2580-2892-0.018	2580	2600	2892	15	5	0.093	0.018

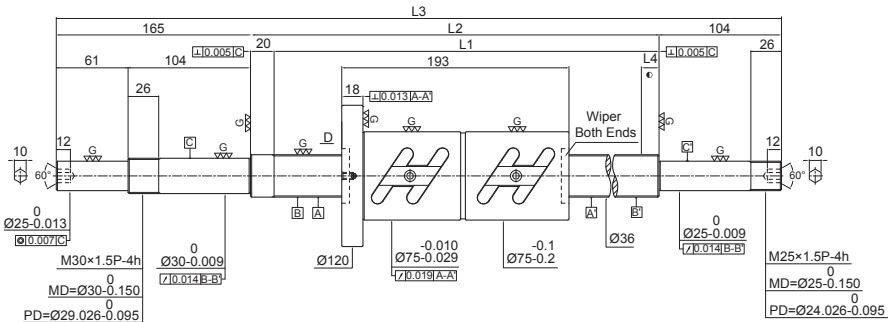
**FDWC** Standard ballscrews  
Screw Dia.Ø32 Lead10


## Specification of ball screw

Production Specification	With Preload
Number of Thread / Thread Direction	1/Right
BCD	33.4
Lead	10
Ball Dia.	6.35
Effective Turns (Circuit × Row)	2.5 × 2
Lead Angle	5.44
Dynamic Rate Load Ca (kgf)	4660
Static Rate Load Co (kgf)	10880
Axial Play	0
Preloading Torque (kgf-cm)	5.51~11.43

Unit: mm

Model No.	Screw Spindle (Shaft) Length				Accuracy Grade	Lead Accuracy	
	L1	L2	L3	L4		Accumulated reference lead deviation E	Lead Derivation in random 300mm e <sub>300</sub>
1R32-10B2-FDWC-380-659-0.018	380	400	659	15	5	0.025	0.018
1R32-10B2-FDWC-480-759-0.018	480	500	759	15	5	0.027	0.018
1R32-10B2-FDWC-580-859-0.018	580	600	859	15	5	0.030	0.018
1R32-10B2-FDWC-680-959-0.018	680	700	959	15	5	0.030	0.018
1R32-10B2-FDWC-780-1059-0.018	780	800	1059	15	5	0.035	0.018
1R32-10B2-FDWC-980-1259-0.018	980	1000	1259	15	5	0.040	0.018
1R32-10B2-FDWC-1180-1459-0.018	1180	1200	1459	15	5	0.046	0.018
1R32-10B2-FDWC-1480-1759-0.018	1480	1500	1759	15	5	0.054	0.018
1R32-10B2-FDWC-1780-2059-0.018	1780	1800	2059	15	5	0.065	0.018

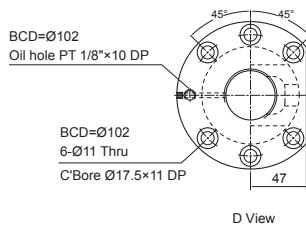
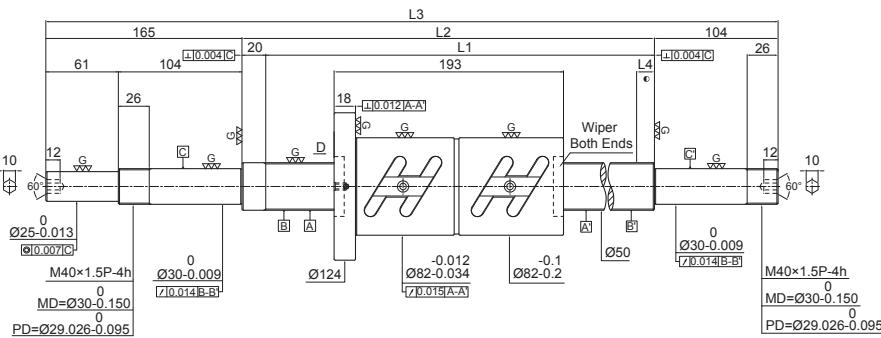
**FDWC** Standard ballscrews  
Screw Dia.Ø36 Lead10


## Specification of ball screw

Production Specification	With Preload
Number of Thread / Thread Direction	1/Right
BCD	37.4
Lead	10
Ball Dia.	6.35
Effective Turns (Circuit × Row)	2.5 × 2
Lead Angle	4.86
Dynamic Rate Load Ca (kgf)	4930
Static Rate Load Co (kgf)	12360
Axial Play	0
Preloading Torque (kgf-cm)	6.64~12.34

Unit: mm

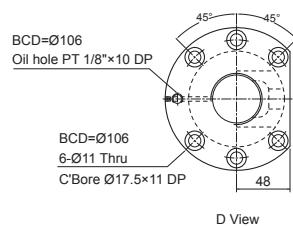
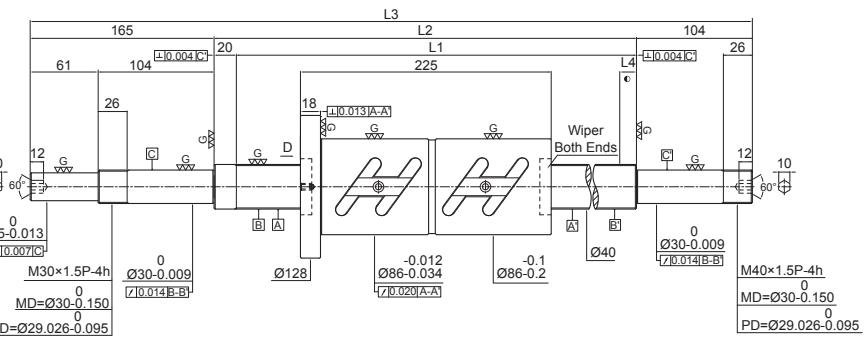
Model No.	Screw Spindle (Shaft) Length				Accuracy Grade	Lead Accuracy	
	L1	L2	L3	L4		Accumulated reference lead deviation E	Lead Derivation in random 300mm e <sub>300</sub>
1R36-10B2-1FDWC-480-769-0.018	480	500	769	15	5	0.027	0.018
1R36-10B2-1FDWC-680-969-0.018	680	700	969	15	5	0.035	0.018
1R36-10B2-1FDWC-980-1269-0.018	980	1000	1269	15	5	0.040	0.018
1R36-10B2-1FDWC-1380-1669-0.018	1380	1400	1669	15	5	0.054	0.018
1R36-10B2-1FDWC-1780-2069-0.018	1780	1800	2069	15	5	0.065	0.018



Specification of ball screw	
Production Specification	
Number of Thread / Thread Direction	1/Right
BCD	41.4
Lead	10
Ball Dia.	6.35
Effective Turns (Circuit × Row)	2.5 × 2
Lead Angle	4.4
Dynamic Rate Load Ca (kgf)	5220
Static Rate Load Co (kgf)	13900
Axial Play	0
Preloading Torque (kgf-cm)	8.26~13.78

Unit: mm

Model No.	Screw Spindle (Shaft) Length				Accuracy Grade	Lead Accuracy	
	L1	L2	L3	L4		Accumulated reference lead deviation E	Lead Derivation in random 300mm e <sub>300</sub>
1R40-10B2-FDWC-480-769-0.018	480	500	769	15	5	0.027	0.018
1R40-10B2-FDWC-580-869-0.018	580	600	869	15	5	0.030	0.018
1R40-10B2-FDWC-680-969-0.018	680	700	969	15	5	0.030	0.018
1R40-10B2-FDWC-780-1069-0.018	780	800	1069	15	5	0.035	0.018
1R40-10B2-FDWC-980-1269-0.018	980	1000	1269	15	5	0.040	0.018
1R40-10B2-FDWC-1180-1469-0.018	1180	1200	1469	15	5	0.046	0.018
1R40-10B2-FDWC-1380-1669-0.018	1380	1400	1669	15	5	0.054	0.018
1R40-10B2-FDWC-1580-1869-0.018	1580	1600	1869	15	5	0.054	0.018
1R40-10B2-FDWC-1780-2069-0.018	1780	1800	2069	15	5	0.065	0.018
1R40-10B2-FDWC-2380-2269-0.018	2380	2400	2269	15	5	0.077	0.018



Specification of ball screw	
Production Specification	
Number of Thread / Thread Direction	1/Right
BCD	41.5
Lead	12
Ball Dia.	7.144
Effective Turns (Circuit × Row)	2.5 × 2
Lead Angle	5.26
Dynamic Rate Load Ca (kgf)	6170
Static Rate Load Co (kgf)	15700
Axial Play	0
Preloading Torque (kgf-cm)	9.79~18.17

Unit: mm

Model No.	Screw Spindle (Shaft) Length				Accuracy Grade	Lead Accuracy	
	L1	L2	L3	L4		Accumulated reference lead deviation E	Lead Derivation in random 300mm e <sub>300</sub>
1R40-12B2-FDWC-680-969-0.018	680	700	969	15	5	0.030	0.018
1R40-12B2-FDWC-980-1269-0.018	980	1000	1269	15	5	0.040	0.018
1R40-12B2-FDWC-1380-1669-0.018	1380	1400	1669	15	5	0.054	0.018
1R40-12B2-FDWC-1780-2069-0.018	1780	1800	2069	15	5	0.065	0.018
1R40-12B2-FDWC-2480-2769-0.018	2480	2500	2769	15	5	0.077	0.018

## 14.1 Introduction to Rolled Ballscrew

The production of the **PMI** rolled ballscrews has adopted a manufacturing process and equipment unlike other manufacturers. Combining advanced skills and the Bad Düben digital electric screw thread rolling machine, we adhere to a strict quality control policy at every stage of production, from the selection of ballscrew material and rolled processing to induction hardening heat treatment and post production. We are committed to providing clients with products of the best quality.

The combination of rolled ballscrews and ground nuts has replaced the traditional ACME screws and trapezoidal screws. This makes for a smoother operation while lowering friction and backlash. Moreover, the new technology has the advantage of faster production speed and lower prices.



We employ the most advanced digital electric screw thread rolling machine. During the manufacturing process, the oil cylinders on the two axes of the thread rolling dies employ a servo hydraulic system for the correction of oil pressure and positioning precision.



We employ Germany-imported Bad Düben roller in order to maintain the stability of the thread rolling machine and the quality of the rolled product.

## 14.2 Features of the **PMI** Rolled Ballscrew

### C7, C8, and C10 Screws have been Standardized

**PMI** C7, C8, and C10 products have been standardized

### High Precision Rolled Nuts

The manufacturing process of rolled nuts is identical to that of ground nuts. Surface hardening treatment and internal thread grinding ensure durability and smoothness.

### Nuts are Interchangeable

Without preload and within the maximum permissible axial play, different types of nuts can be used on the same screw.

## 14.3 Lead Accuracy of Rolled Screws ( $e_{300}$ )

According to JIS B1192:1997, the definition of lead accuracy for **PMI** rolled ballscrews is as follows: Within the effective thread length, the permissible value of accumulated lead deviation in random 300mm. As shown in table 14.1:

Table 14.1 Lead Accuracy

$e_{300}$  (Within the effective thread length, the permissible value of accumulated lead deviation in random 300mm)

Unit:  $\mu\text{m}$

Grade	C5	C6	C7	C8	C10
ISO, DIN	23		52		210
JIS	18		50		210
<b>PMI</b>	18	25	50	100	210

ep(Within the effective thread length, the permissible value of accumulated lead deviation) Unit:  $\mu\text{m}$

Grade	C6	C7	C8	C10
PMI	$\text{ep} = \pm(\text{lu}/300) \times e_{300}$	lu: Effective thread length (Unit: mm)		

e <sub>300</sub> Measured length	Grade	C6	C7	C8	C10
0~100		20	44	84	178
101~200		22	48	92	194
201~315		25	50	100	210

P.S. Please contact us for PMI C5 and C6 requirements.

#### 14.4 Reference Table of the Nominal Outer diameter and Lead of the PMI's Rolled screw shaft

PMI rolled ballscrews offer a variety of specifications, lead accuracies, and maximum rolling length, as shown in table 14.2~14.3:

Table 14.2 Specifications of Rolled Ballscrews

Screw nominal outer diameter Ø	Lead										Maximum rolled ballscrew length
	4	5	5.08	6	10	16	20	25	32	40	
12	●	●									1500
14	●	●									3000
15		●			●	●					3000
16	●	●			●	●					3000
20	●	●			●		●				3000
25	●	●/○	●/○		●			●			6000
28		●		●							6000
32	●/○	●/○			●		●		●		6000
36					●						6000
38					●		●			●	6000
40		●			●		●			●	6000
50					●						6000

● : right-hand thread ○ : left-hand thread

P.S. Rolled ballscrews are limited in length and accuracy, please contact us for other requirements.

Table 14.3 Lead Accuracy and Maximum Rolled Length

Screw nominal outer diameter Ø(mm)	Lead Accuracy Grade (e <sub>300</sub> ) Maximum Rolled Length (mm)			
	ISO5	ISO7	-	ISO10
	C6	C7	C8	C10
12	1500	1500	1500	1500
14	1500	3000	3000	3000
15	2000	3000	3000	3000
16	2000	3000	3000	3000
20				
25				
28				
32		3000	6000	6000
36				
38				
40				
50				

#### 14.5 Axial Play

The maximum axial play under normal non-preload condition, as shown in table 14.4

Table 14.4 Maximum Axial Play

Screw O.D. Ød (mm)	6~32	36~50
Maximum Axial Play (mm)	0.04	0.07

PMI rolled ballscrews can eliminate axial play by preloading. Please contact our sales representatives if preloading is required.

#### 14.6 Materials and Hardness

Standard material and surface hardness for PMI rolled screw, as shown in table 14.5

Table 14.5

Denomination	Material	Heat Treatment	Hardness (HRC)
Rolled screw	S55C/Equivalent	Induction hardening	58~62
Nuts	SCM420H/Equivalent	Carburized hardening	58~62

### 14.7 Types and Dimensions of Rolled screw shaft

						Unit:mm							
SCREW SIZE			Lead Accuracy Grade	Thread Direction L: Left / R: Right	Number of Threads	Maximum Rolling Length	Screw Number						
O.D.	LEAD	BALL DIA.						O.D.	LEAD	BALL DIA.	SCREW SIZE	Lead Accuracy Grade	Thread Direction L: Left / R: Right
<b>12</b>	4	2.381	C6,C7,C8,C10	R	1	1500	R1204A	C6,C7,C8,C10					
	5	2.000		R	1		R1205Z						
<b>14</b>	4	2.381		R	1	3000	R1404A						
	5	3.175		R	1		R1405B						
<b>15</b>	5	3		R	1	3000	R1505V						
	10	3		R	2		2R1510V						
	10	3.175		R	2		2R1510B						
	16	3		R	2		2R1516V						
<b>16</b>	4	2.381		R	1	3000	R1604A						
	5	3.175		R	1		R1605B						
	10	3.175		R	2		2R1610B						
	16	3.175		R	2		2R1616B						
<b>20</b>	4	2.381		R	1	6000	R2004A						
	5	3.175		R	1		R2005B						
	10	4.762		R	1		R2010D						
	20	3.175		R	2		2R2020B						

SCREW SIZE			Lead Accuracy Grade	Thread Direction L: Left / R: Right	Number of Threads	Maximum Rolling Length	Screw Number						
O.D.	LEAD	BALL DIA.						O.D.	LEAD	BALL DIA.	SCREW SIZE	Lead Accuracy Grade	Thread Direction L: Left / R: Right
<b>25</b>	4	2.381	C6,C7,C8,C10										
	5	3.175											
	5.08	3.175											
	10	3.175											
	10	4.762											
	10	6.350											
	25	3.175											
	25	3.969											
<b>28</b>	5	3.175											
	6	3.175											
	5	3.175											
	5.08	3.175											
<b>32</b>	10	3.969	C6,C7,C8,C10										
	10	6.350											
	20	3.969											
	20	6.350											
	32	3.969											
	32	4.762											
	10	6.350											
	20	6.350											
<b>36</b>	10	6.350	C6,C7,C8,C10										
	10	6.350											
	20	6.350											
	40	6.350											
<b>40</b>	5	3.175	C6,C7,C8,C10										
	10	6.350											
	20	6.350											
	40	6.350											
<b>50</b>	10	6.350	C6,C7,C8,C10										
	10	6.350											

**Order Code:****4 R 15 10 A -1500 -C7**

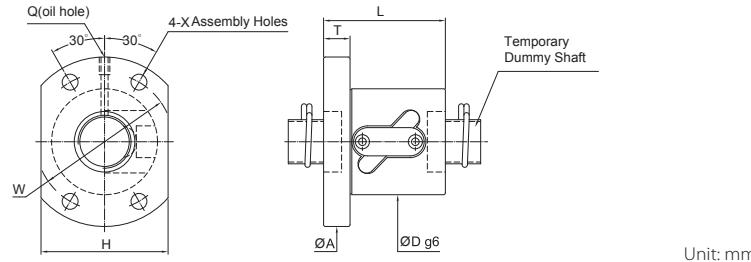
- Lead Accuracy Grade
- Custom Length of Screw (mm)
- Ball Diameter(mm)(A: 2.381 B: 3.175 C: 3.969  
D: 4.762 F: 6.35 Z: 2.0 V: 3.0 )
- Lead (mm)
- Screw Nominal O.D. (mm)
- Thread Direction (R: Right L: Left)
- Number of Threads (N/A for single thread screws)

**Optional Models :****FSWW****FSVW****RSVW****SSVW****FSBW****Order Code:****R F SDN 25 05 A 4T**

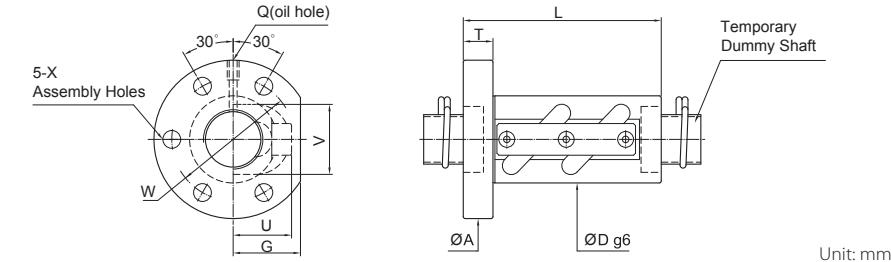
- Effective Turns
- Ball Diameter(mm)(A:2.381 B:3.175 C:3.969 D:4.762 F:6.35  
V:3.0)
- Lead(mm)
- Screw nominal O.D.(mm)
- N:European Standard Model
- Ball Circulation Type D : End Deflector Series  
I : Internal Ball Circulation Nuts  
W : Immersion type  
V : Extrusive type  
K : End Cap Series
- Single Nut
- Type of Nuts(F:with flange R:without flange S:square nut)
- Thread Direction(R: Right L:Left)

**14.8 Nut Types of Rolled Ballscrew****Standard Models:**

## FSWW

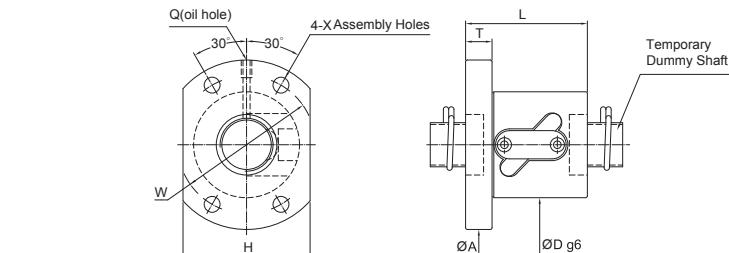


SCREW SIZE	BALL DIA.	EFFECTIVE TURNS circuit × row	BASIC RATE LOAD(kgf)		BALLNUT DIMENSION										Nut Model NO.
			Dynamic (1×10 <sup>6</sup> REV.) Ca	Static Co	O.D. D	Length L	Flange A	Assembly Hole T	Oil Hole W	H	X	Q	STIFFNESS kgf/μm		
12	4	2.381	2.5x1	285	533	30	40	52	10	40	31	4.5	M6x1P	9	FSWW1204A-2.5P
	5	2	2.5x1	270	350	26	40	47	10	37	30	4.5	M6x1P	8.2	FSWW1205Z-2.5P
14	4	2.381	3.5x1	500	1100	35	42	57	10	45	40	4.5	M6x1P	15	FSWW1404A-3.5P
	5	3.175	2.5x1	515	990	40	40	57	10	45	40	4.5	M6x1P	11	FSWW1405B-2.5P
15	10	3.175	2.5x1	440	680	34	55	57	10	45	34	5.5	M6x1P	12	FSWW1510B-2.5P
			1.5x2	540	1260		44					15	FSWW1604A-3.0P		
	4	2.381	2.5x1	460	1050	34	41	57	11	45	34	5.5	M6x1P	13	FSWW1604A-2.5P
			3.5x1	610	1470		42					17	FSWW1604A-3.5P		
16			1.5x2	640	1370		45					15	FSWW1605B-3.0P		
	5	3.175	2.5x1	550	1140	40	41	63	11	51	42	5.5	M6x1P	13	FSWW1605B-2.5P
			2.5x2	1000	2280	40	56					23	FSWW1605B-5.0P		
			3.5x1	730	1600		46					17	FSWW1605B-3.5P		
	10	3.175	2.5x1	550	990	40	56	63	11	51	42	5.5	M6x1P	13	FSWW1610B-2.5P
20			1.5x2	740	1870		45					19	FSWW2004A-3.0P		
	4	2.381	2.5x1	630	1560	40	42	67	11	55	52	5.5	M6x1P	16	FSWW2004A-2.5P
			2.5x2	1140	3120		56					30	FSWW2004A-5.0P		
			3.5x1	840	2180		46					22	FSWW2004A-3.5P		
			1.5x2	730	1740		45					18	FSWW2005B-3.0P		
25	5	3.175	2.5x1	625	1450	44	42	67	11	55	52	5.5	M6x1P	15	FSWW2005B-2.5P
			2.5x2	1130	2900		56					28	FSWW2005B-5.0P		
			3.5x1	830	2030		46					20	FSWW2005B-3.5P		
	10	4.762	2.5x1	1100	2200	52	61	82	12	67	64	6.6	M6x1P	16	FSWW2010D-2.5P



SCREW SIZE	BALL DIA.	EFFECTIVE TURNS circuit × row	BASIC RATE LOAD(kgf)		BALLNUT DIMENSION										Nut Model NO.	
			Dynamic (1×10 <sup>6</sup> REV.) Ca	Static Co	O.D. D	Length L	Flange A	Assembly Hole T	Oil Hole W	H	X	Q	STIFFNESS kgf/μm			
25	4	1.5x2	980	2640		44									24	FSWW2504A-3.0P
		2.5x1	840	2200	46	40									20	FSWW2504A-2.5P
		2.5x2	1520	4400	49	49									38	FSWW2504A-5.0P
		3.5x1	1120	3080		42									27	FSWW2504A-3.5P
25	5	1.5x2	840	2200		45									21	FSWW2505B-3.0P
		2.5x1	720	1830	50	41									18	FSWW2505B-2.5P
		2.5x2	1120	3710	56	56									37	FSWW2505B-5.0P
		3.5x1	960	2560		46									24	FSWW2505B-3.5P
28	10	1.5x2	1490	3340		71									23	FSWW2510D-3.0P
		2.5x1	1270	2780	58	65	85	15	71	64	6.6	M6x1P			20	FSWW2510D-2.5P
		3.5x1	1700	3890		75									27	FSWW2510D-3.5P
		2.5x1	1720	3590	60	69	96	15	78	72	9	M6x1P			21	FSWW2510F-2.5P
32	5	1.5x2	910	2470		46									21	FSWW2805B-3.0P
		2.5x1	780	2060	55	42									18	FSWW2805B-2.5P
		2.5x2	1410	4120	56	56									33	FSWW2805B-5.0P
		3.5x1	1040	2880		47									24	FSWW2805B-3.5P
32	5	1.5x2	990	2830		47									26	FSWW3205B-3.0P
		2.5x1	850	2360		43									22	FSWW3205B-2.5P
		2.5x2	1540	4720	58	57	85	12	71	64	6.6	M8x1P			41	FSWW3205B-5.0P
		2.5x3	2180	7080		72									59	FSWW3205B-7.5P
32	10	1.5x2	1130	3300		47									29	FSWW3205B-3.5P
		2.5x1	2260	5620		78									29	FSWW3210F-3.0P
		2.5x2	1930	4680	67	69	103	15	85	78	9	M6x1P			25	FSWW3210F-2.5P
		3.5x1	2580	6550		78									33	FSWW3210F-3.5P

## FSWW

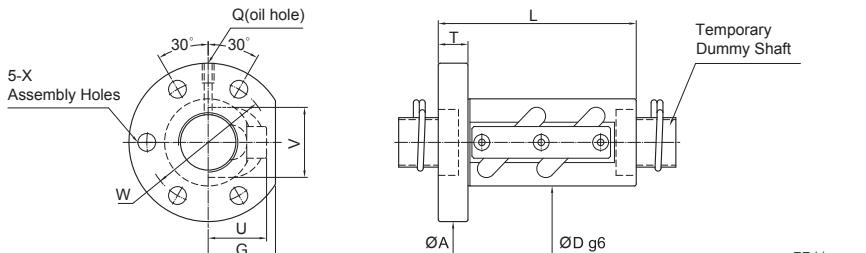


SCREW SIZE		BALL DIA.	EFFECTIVE TURNS circuit × row	BASIC RATE LOAD(kgf)		BALLNUT DIMENSION									
O.D.	LEAD			Dynamic (1×10 <sup>6</sup> REV.) Ca	Static Co	O.D. D	Length L	Flange A	T	W	H	Assembly Hole X	Oil Hole Q	STIFFNESS kgf/μm	Nut Model NO.
36	10	6.35	1.5x2	2170	6480	81							30	FSWW3610F-3.0P	
			2.5x2	3370	10800	70	99	110	17	90	82	11	M6x1P	29	FSWW3610F-5.0P
			3.5x1	2480	7560	81							35	FSWW3610F-3.5P	
40	10	3.175	1.5x2	1180	3560	50							37	FSWW4005B-3.0P	
			2.5x1	1010	2970	48							32	FSWW4005B-2.5P	
			2.5x2	1830	5940	67	60	101	15	83	78	9	M8x1P	60	FSWW4005B-5.0P
			2.5x3	2600	8910	75							87	FSWW4005B-7.5P	
			3.5x1	1350	4160	50							43	FSWW4005B-3.5P	
50	10	6.35	1.5x2	2270	7200	81							39	FSWW4010F-3.0P	
			2.5x1	1940	6000	76	71	116	17	96	88	11	M6x1P	34	FSWW4010F-2.5P
			2.5x2	3520	12000	100	100						59	FSWW4010F-5.0P	
			3.5x1	2590	8400	81							45	FSWW4010F-3.5P	
			3.5x2	4940	21000	126							98	FSWW5010F-7.0P	

## Note:

Stiffness of nut:

Stiffness values listed above are derived from theoretical formula to the elastic deformation between thread grooves and balls while axial load is 30% dynamic load rating.

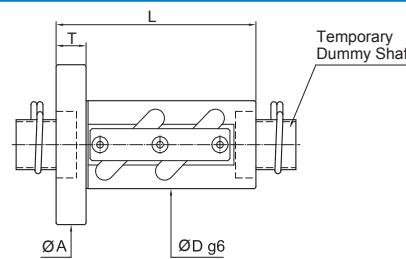
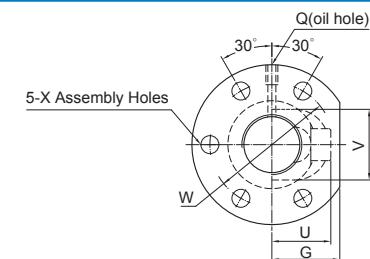


SCREW SIZE		BALL DIA.	EFFECTIVE TURNS circuit × row	BASIC RATE LOAD(kgf)		BALLNUT DIMENSION											
O.D.	LEAD			Dynamic (1×10 <sup>6</sup> REV.) Ca	Static Co	O.D. D	Length L	Flange A	T	W	H	Return tube U	Assembly Hole V	Oil Hole X	STIFFNESS Q kgf/μm	Nut Model NO.	
14	4	3.175	3.5x1	500	1100	25	42	55	10	40	19	21	4.5	M6x1P	15	FSVW1404A-3.5P	
	5		2.5x1	515	990	30	43	50	10	40	22	22	4.5	M6x1P	11	FSVW1405B-2.5P	
	5		1.5x2	540	1260	50							50		15	FSVW1605B-3.0P	
16	5	3.175	2.5x1	550	1140	34	43	54	12	41	24	20	23	5.5	M6x1P	13	FSVW1605B-2.5P
	5		2.5x2	1000	2280	60	60	54	12	41	24	20	23	23	M6x1P	23	FSVW1605B-5.0P
	5		3.5x1	730	1600	50							50		17	FSVW1605B-3.5P	
20	5	3.175	1.5x2	730	1740	50							50		18	FSVW2005B-3.0P	
	5		2.5x1	625	1450	40	43	60	12	50	28	28	27	4.5	M6x1P	15	FSVW2005B-2.5P
	5		2.5x2	1130	2900	60	60	60	12	50	28	28	27	28	M6x1P	28	FSVW2005B-5.0P
	10		3.5x1	830	2030	50							50		20	FSVW2005B-3.5P	
	10		2.5x1	1100	2200	40	60	67	12	53	30	30	30	6.6	M6x1P	16	FSVW2010-2.5P
25	5	3.175	2.5x1	720	1830	42	45	71	12	57	28	28	32	6.6	M6x1P	18	FSVW2505B-2.5P
	5		2.5x2	1120	3710	60	60	71	12	57	28	28	32	37	M6x1P	37	FSVW2505B-5.0P
	10		3.5x1	1480	3340	75								75		23	FSVW2510D-3.0P
30	10	4.762	2.5x1	1270	2780	45	65	72	16	58	34	29	34	6.6	M6x1P	20	FSVW2510D-2.5P
	10		3.5x1	1690	3900	75								75		27	FSVW2510D-3.5P
	10		2.5x1	1720	3590	44	68	79	15	62	34	34	37	9	M6x1P	21	FSVW2510F-2.5P
28	5	3.175	2.5x2	3200	7170	98	60	70	12	56	28	28	34	6.6	M6x1P	40	FSVW2510F-5.0P
	5		1.5x2	910	2470	50								50		21	FSVW2805B-3.0P
	5		2.5x1	780	2060	44	45	70	12	56	28	28	34	18	M6x1P	33	FSVW2805B-2.5P
	5		2.5x2	1410	4120	60	60	70	12	56	28	28	34	24	M6x1P	33	FSVW2805B-5.0P
28	5	3.175	3.5x1	1040	2880	50								50		24	FSVW2805B-3.5P

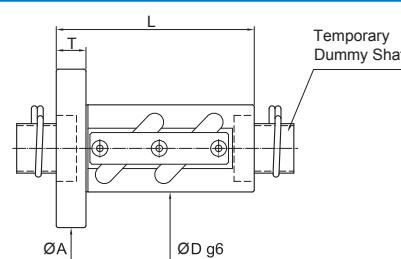
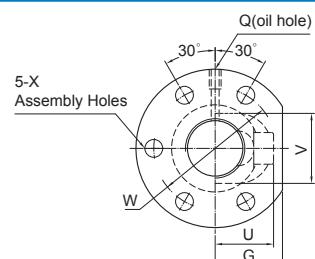
## FSVW

## A255

## FSVW



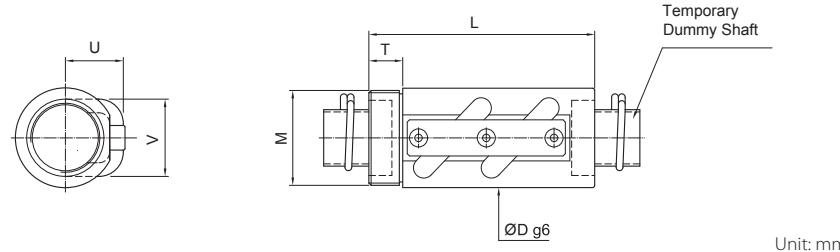
SCREW SIZE	BALL DIA.	EFFECTIVE TURNS circuit x row	BASIC RATE LOAD(kgf)		BALLNUT DIMENSION														
			Dynamic (1x10 <sup>6</sup> REV.) Ca	Static Co	O.D.	Length	Flange	Return tube	Assembly Hole	Oil Hole	STIFFNESS kgf/μm	Nut Model NO.	D	L	A	T	W	H	X
32	5 3.175	1.5x2	990	2830	50	45					26	FSVW3205B-3.0P							
		2.5x1	850	2360	50	60	76	12	63	36	30	38	6.6	M6x1P	41	FSVW3205B-5.0P			
		2.5x2	1540	4720	50	75										59	FSVW3205B-7.5P		
		2.5x3	2180	7080												29	FSVW3205B-3.5P		
		3.5x1	1130	3300		50													
	10 6.35	1.5x2	2260	5620	55	78										29	FSVW3210F-3.0P		
		2.5x1	1930	4680	55	72	97	18	75	39	39	44	11	M6x1P	25	FSVW3210F-2.5P			
		2.5x2	3130	9410	55	101										49	FSVW3210F-5.0P		
		3.5x1	2580	6550		78										33	FSVW3210F-3.5P		
36	10 6.35	1.5x2	2170	6480	60	82	18									30	FSVW3610F-3.0P		
		2.5x1	1860	5400	60	70	105	17	80	42	35	49	11	M6x1P	29	FSVW3610F-2.5P			
		2.5x2	3370	10800	60	98	18									55	FSVW3610F-5.0P		
		3.5x1	2480	7560		82	18									35	FSVW3610F-3.5P		
40	5 3.175	1.5x2	1180	3560	58	55										45	FSVW4005B-3.0P		
		2.5x1	1010	2970	58	50										45	FSVW4005B-2.5P		
		2.5x2	1830	5940	58	65	92	16	72	42	34	46	9	M8x1P	60	FSVW4005B-5.0P			
		2.5x3	2600	8910		80										87	FSVW4005B-7.5P		
		3.5x1	1350	4160		55										43	FSVW4005B-3.5P		
	10 6.35	1.5x2	2270	7200	65	82										39	FSVW4010F-3.0P		
		2.5x1	1940	6000	65	72	106	18	85	44	42	52	11	PT1/8"	34	FSVW4010F-2.5P			
		2.5x2	3520	12000	65	102										59	FSVW4010F-5.0P		
		3.5x1	2590	8400		82										45	FSVW4010F-3.5P		
		3.5x2	4450	16800		123	114	20	90	44	52	14	M6x1P	81	FSVW4010F-7.0P				



單位:mm

## FSVW

## RSVW



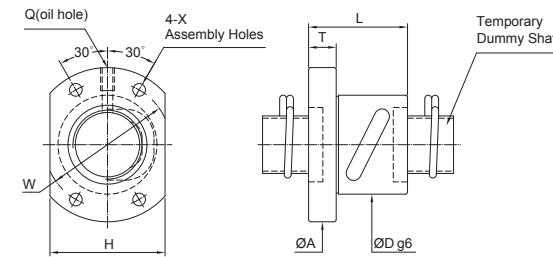
SCREW SIZE	BALL DIA.	EFFECTIVE TURNS circuit × row	BASIC RATE LOAD(kgf)		BALLNUT DIMENSION										
			Dynamic (1×10 <sup>6</sup> REV.) Ca	Static Co	O.D. D	Length L	Flange M	Return tube T	STIFFNESS kgf/μm	Nut Model NO.					
14	4	2.381	3.5×1	500	1100	25	42	M24×1.0P	10 19 21	15	RSVW1404-3.5P				
	5	3.175	2.5×1	515	990	30	43	M26×1.5P	10 22 21	11	RSVW1405-2.5P				
20	5	3.175	2.5×1	625	1450	40	43	M36×1.5P	12 28 27	15	RSVW1605-2.5P				
25	5	3.175	2.5×1	720	1830	42	48	M40×1.5P	15 28 32	18	RSVW2505-2.5P				
			2.5×2	1120	3710		63			37	RSVW2505-5.0P				
	10	6.350	2.5×1	1720	3590	44	68	M42×1.5P	15 34 37	21	RSVW2510-2.5P				
			2.5×2	3200	7170		98			40	RSVW2510-5.0P				
32	10	6.350	2.5×1	1930	4680	55	72	M50×1.5P	18 39 44	25	RSVW3210-2.5P				
			2.5×2	3130	9410		101			49	RSVW3210-5.0P				
40	10	6.350	3.5×2	4450	16800	65	128	M60×2.0P	25 44 52	81	RSVW4010-7.0P				
50	10	6.350	3.5×2	4940	21000	80	143	M75×2.0P	40 52 62	98	RSVW5010-7.0P				

Note:

Stiffness of nut:

Stiffness values listed above are derived from theoretical formula to the elastic deformation between thread grooves and balls while axial load is 30% dynamic load rating.

## FSBW



SCREW SIZE	BALL DIA.	EFFECTIVE TURNS circuit × row	BASIC RATE LOAD(kgf)		BALLNUT DIMENSION										
			Dynamic (1×10 <sup>6</sup> REV.) Ca	Static Co	O.D. D	Length L	A	T	W	H	Assembly Hole X	Oil Hole Q	STIFFNESS kgf/μm	Nut Model NO.	
12	5	2.000	2.5×1	270	350	26	40	47	10	37	30	4.5	M6×1P	8.2	FSBW1205-2.5P
14	4	2.381	3.5×1	500	1100	31	40	50	10	40	37	4.5	M6×1P	15	FSBW1404-3.5P
16	5	3.175	2.5×1	515	990	32	40	50	10	40	38	4.5	M6×1P	11	FSBW1405-2.5P
20	4	2.381	2.5×1	570	1130	34	40	54	10	44	40	4.5	M6×1P	13	FSBW1605-2.5P
20	5	3.175	2.5×1	415	850	40	41	59	10	50	46	4.5	M6×1P	14	FSBW2004-2.5P
25	5	3.175	2.5×1	620	1450	40	40	59	10	50	46	4.5	M6×1P	16	FSBW2005-2.5P
25	4	2.381	2.5×1	450	980	43	41	67	10	55	50	4.5	M6×1P	17	FSBW2504-2.5P
25	5	3.175	2.5×1	720	1830	43	40	67	10	55	50	5.5	M6×1P	18	FSBW2505-2.5P

Note:

Stiffness of nut:

Stiffness values listed above are derived from theoretical formula to the elastic deformation between thread grooves and balls while axial load is 30% dynamic load rating.

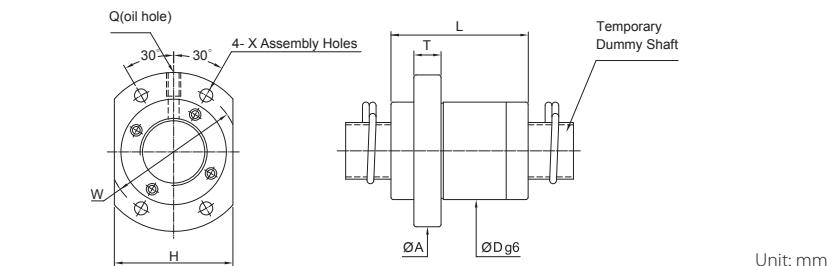
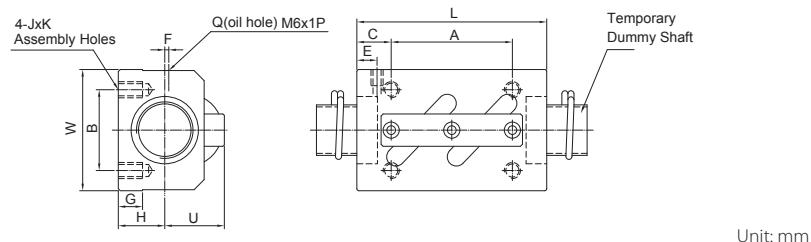
**SSVW**

SCREW SIZE	BALL DIA.	EFFECTIVE TURNS circuit x row	BASIC RATE LOAD(kgf)		BALLNUT DIMENSION												
			Dynamic (1×10 <sup>6</sup> REV.) Ca	Static Co	Length L	Width W	Height H	Assembly Hole A	Position of Oil Hole B	Height from Reference Surface C	JxK E F G U	STIFFNESS kgf/μm	Nut Model NO.				
14	4	2.381	3.5×1	500	1110	35	34	13	22 26 6.5 M4×7	6 2	6 18	15	SSVW1404-3.5P				
	5	3.175	2.5×1	515	990	35	34	13	22 26 6.5 M4×7	6 2	6 18	11	SSVW1405-2.5P				
16	5	3.175	2.5×1	590	1210	35	42	16	22 32 6.5 M5×8	6 2	8 21	13	SSVW1605-2.5P				
	5	3.175	2.5×1	625	1450	35	48	17	22 35 6.5 M6×10	6 3	9.15 22	15	SSVW2005-2.5P				
20	10	4.762	2.5×1	1100	2220	58	48	18	35 35 11.5 M6×10	10 2	9.5 25	16	SSVW2010-2.5P				
	5	3.175	2.5×1	720	1830	35	60	20	22 40 6.5 M8×12	7 5	9.5 25	18	SSVW2505-2.5P				
25	10	6.350	2.5×2	3240	7170	94	60	23	60 40 17 M8×12	10 -	10 30	40	SSVW2510-5.0P				
	6	3.175	2.5×2	1380	4140	67	60	22	40 40 13.5 M8×12	8 5	10 27	39	SSVW2806-5.0P				
32	10	6.350	2.5×1	1930	4680	64	70	26	45 50 9.5 M8×12	10 -	12 36	25	SSVW3210-2.5P				
	2.5×2	3130	9410	94		60	17					49	SSVW3210-5.0P				

## Note:

Stiffness of nut:

Stiffness values listed above are derived from theoretical formula to the elastic deformation between thread grooves and balls while axial load is 30% dynamic load rating.



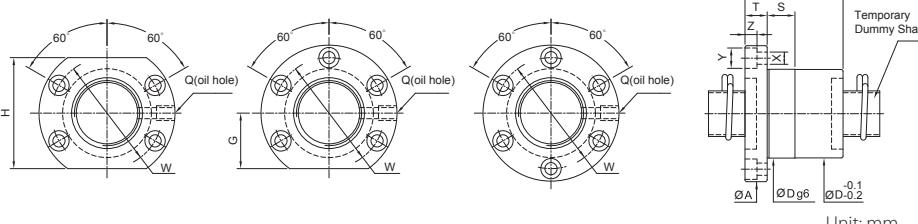
SCREW SIZE	BALL DIA.	EFFECTIVE TURNS circuit X row	BASIC RATE LOAD(kgf)		BALLNUT DIMENSION												
			Dynamic (1×10 <sup>6</sup> REV.) Ca	Static Co	O.D. D	Length L	Flange A	T	W	Assembly Hole H X	Oil Hole Q	STIFFNESS kgf/μm	Nut Model NO.				
15	10	3.175	2.8×2	1000	2570	34	44	57	10	45	40	5.5	M6×1P	26	FSKW1510-5.6P		
16	16	3.175	1.8×1	330	640	32	38	53	10	42	38	4.5	M6×1P	9	FSKW1616-1.8P		
20	20	3.175	1.8×2	780	2280	39	52	62	10	50	46	5.5	M6×1P	21	FSKW2020-3.6P		
25	25	3.969	1.8×2 1.8×4	1230 2230	3570 7140	47	62	74	12	60	56	6.6	M6×1P	27 52	FSKW2525-3.6P FSKW2525-7.2P		
32	32	4.762	1.8×2 1.8×4	1760 3200	5500 11000	58	78	92	15	74	68	9	M6×1P	33 65	FSKW3232-3.6P FSKW3232-7.2P		
40	40	6.350	1.8×2 1.8×4	2870 5220	9170 18340	73	95	114	17	93	84	11	M6×1P	42 81	FSKW4040-3.6P FSKW4040-7.2P		

## Note:

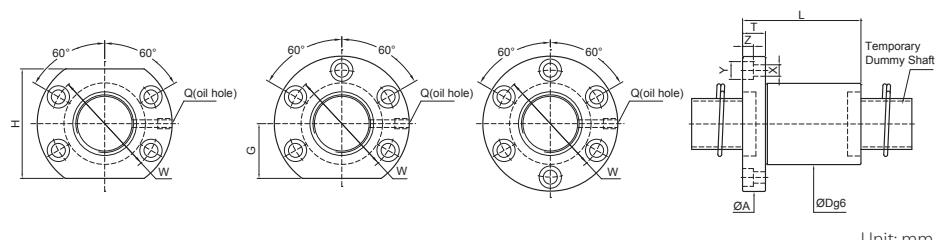
Stiffness of nut:

Stiffness values listed above are derived from theoretical formula to the elastic deformation between thread grooves and balls while axial load is 30% dynamic load rating.

**FSKW**



Unit: mm



Unit: mm

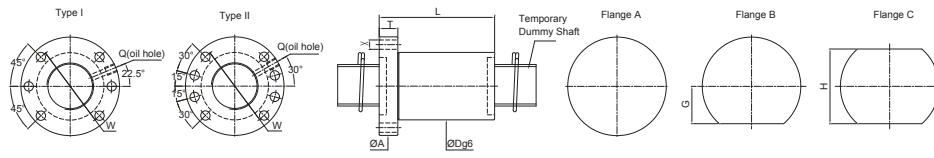
SCREW SIZE	BASIC RATE LOAD(kgf)												BALLNUT DIMENSION									
	O.D.	LEAD	BALL DIA.	EFFECTIVE TURNS	Dynamic (1x10 <sup>6</sup> REV.) Ca	Static Co	O.D. D	Length L	Flange			Assembly Hole			Oil Hole	STIFFNESS Q	kgf/μm	Nut Model NO.				
14	4	2.381	3	310	670	26	42	46	10	36	20	40	4.5	8	4.5	M6x1P	12	FSIW1404A-3.0P				
		4	400	890													18	FSIW1404A-4.0P				
16	4	2.381	3	320	760	28	42	49	10	39	20	40	4.5	8	4.5	M6x1P	13	FSIW1604A-3.0P				
	5	3.175	3	570	1030	30	42	49	10	39	20	40	4.5	8	4.5	M6x1P	17	FSIW1605B-3.0P				
20	4	2.381	4	450	1270	34	44	60	12	48	22	44	5.5	9.5	5.5	M6x1P	19	FSIW2004A-4.0P				
	5	3.175	4	650	1420		47										17	FSIW2005B-3.0P				
25	4	2.381	3	380	1195	40	40	63	12	51	22	44	5.5	9.5	5.5	M8x1P	17	FSIW250A4-3.0P				
	5	3.175	4	730	1820		47										20	FSIW250B-3.0P				
25	5	3.175	4	940	2420	40	53	63.5	12	51	22	44	5.5	9.5	5.5	M8x1P	26	FSIW250B-4.0P				
	5	1140	3030		57												32	FSIW250B-5.0P				
28	3	1215	2660		80												22	FSIW2510D-3.0P				
	10	4.762	4	1550	3540	42	85	68.5	15	55	26	52	6.6	11	6.5	M8x1P	28	FSIW2510D-4.0P				
32	5	1880	4430		91												34	FSIW2510D-5.0P				
	6	3.175	3	770	2180	43	50	68	12	55	26	52	6.6	11	6.5	M8x1P	22	FSIW2806B-3.0P				
32	3	820	2540		47												24	FSIW3205B-3.0P				
	5	3.175	4	1050	3390	48	53	73.5	12	60	30	60	6.6	11	6.5	M8x1P	32	FSIW3205B-4.0P				
36	6	1490	5090		62												46	FSIW3205B-6.0P				
	10	6.35	3	1960	4410	50	80	88	16	70	34	68	9	14	8.5	M8x1P	28	FSIW3210F-3.0P				
36	4	2510	5880	54	90												34	FSIW3210F-4.0P				
	10	6.35	3	2010	5150	58	78	98	18	77	36	72	11	17.5	11	M8x1P	30	FSIW3610F-3.0P				
	4	2570	6870	89	89												39	FSIW3610F-4.0P				

SCREW SIZE	BASIC RATE LOAD(kgf)												BALLNUT DIMENSION									
	O.D.	LEAD	BALL DIA.	EFFECTIVE TURNS	Dynamic (1x10 <sup>6</sup> REV.) Ca	Static Co	O.D. D	Length L	Flange			Assembly Hole			Oil Hole	STIFFNESS Q	kgf/μm	Nut Model NO.				
40	5	3.175		4	1180	4390		56										38	FSIW4005-4.0P			
	6	1670	6590	5	1430	5490	55	61	88.5	16	72	29	58	15	9	14	M8x1P	46	FSIW4005B-5.0P			
40	10	6.35		3	2050	5900		65										55	FSIW4005B-6.0P			
	5	2630	7860	4	2260	7720	64	93	106	18	84	43	86	11	17.5	11	M8x1P	41	FSIW4010F-3.0P			
50	10	6.35		3	2160	7720		83										52	FSIW4010F-4.0P			
	5	3360	12860	4	2770	10290	74	93	116	18	94	42	84	11	17.5	11	M8x1P	39	FSIW5010F-3.0P			
50	6	3920	15440	5	3360	12860	99	114										50	FSIW5010F-4.0P			
				6	3920	15440												62	FSIW5010F-5.0P			
																		73	FSIW5010F-6.0P			

**Note:****Stiffness of nut:**

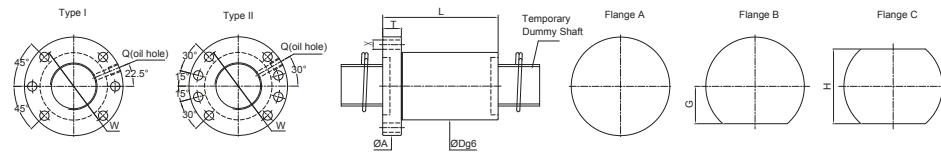
Stiffness values listed above are derived from theoretical formula to the elastic deformation between thread grooves and balls while axial load is 30% dynamic load rating.

## FSDW



Unit: mm

SCREW SIZE				MODIFIED LOAD CAPACITY(kgf)		BALLNUT DIMENSION										Nut Model NO.		
	O.D.	LEAD	BALL DIA.	EFFECTIVE TURNS	Dynamic (1×10 <sup>6</sup> REV.) Cam	Static Coam	O.D.	Length	Flange			Oil Hole Q	Assembly Hole X	STIFFNESS kgf/μm	Nut Model NO.			
12	4	2.381	3	410	990	24	28	44	10	34	16	32	I	M6x1P	4.5	13	FSDW1204A-3.0P	
	4	2.381	3	460	1210	26	28	46	10	36	17	34	I	M6x1P	4.5	14	FSDW1404A-3.0P	
14	4	590	1610	32	32	48												FSDW1404A-4.0P
	5	3.175	3	550	1260	29	32	51	10	39	18.5	37	I	M6x1P	5.5	14	FSDW1405B-3.0P	
15	10	3.175	3	560	1340	29	47	51	10	39	18.5	37	I	M6x1P	5.5	15	FSDW1510B-3.0P	
	5	3.175	3	600	1460	29	35	51	10	39	18.5	37	I	M6x1P	5.5	16	FSDW1605B-3.0P	
16	10	3.175	3	580	1440	29	50	51	10	39	18.5	37	I	M6x1P	5.5	15	FSDW1610B-3.0P	
	16	3.175	2	400	950	29	51	51	10	39	16	38	I	M6x1P	5.5	11	FSDW1616B-2.0P	
	4	2.381	3	520	1660	32	28	53	10	43	21.5	43	I	M6x1P	4.5	18	FSDW2004A-3.0P	
20		5	3.175	3	670	1860	36	35	62	12	49	23	46	I	M6x1P	5.5	19	FSDW2005B-3.0P
	4	870	2480	40														FSDW2005B-4.0P
	10	4.762	3	1320	3390	40	52	62	12	51	24	48	I	M6x1P	6.6	21	FSDW2010D-3.0P	
	20	3.175	2	450	1200	36	56	62	12	49	19	38	I	M6x1P	6.6	13	FSDW2020B-2.0P	
	4	2.381	3	580	2120	37	28	62	12	50	24	48	I	M6x1P	6.6	21	FSDW2504A-3.0P	
		3	740	2350		36												FSDW2505B-3.0P
25		5	3.175	4	960	3190	40	41	62	12	51	24	48	I	M6x1P	6.6	28	FSDW2505B-4.0P
		5	1180	4030		46												FSDW2505B-5.0P
	4.762	4	1920	5700	45	63	65	15	54	25.5	51	I	M6x1P	6.6	32	FSDW2510D-4.0P		
	10	6.35	3	2130	5570	51	58	87	16	72	34.5	69	I	M8x1P	9	27	FSDW2510F-3.0P	
		5	3380	9550	78													FSDW2510F-5.0P
	25	3.969	2	780	2260	40	71	62	12	51	24	48	I	M6x1P	6.6	16	FSDW2525C-2.0P	
28	5	3.175	5	1240	4530	43	48	65	12	54	24	48	I	M8x1P	6.6	38	FSDW2805B-5.0P	
	5	3.175	4	1080	4130	50	41	87	16	72	34.5	69	I	M8x1P	9	34	FSDW3205B-4.0P	
32	10	6.35	3	2410	7020	57	58	87	16	72	34.5	69	I	M8x1P	9	32	FSDW3210F-3.0P	
	5	3820	12030	78														FSDW3210F-5.0P
	32	4.762	2	1100	3420	53	84	87	16	72	34.5	69	I	M8x1P	9	20	FSDW3232D-2.0P	



Unit: mm

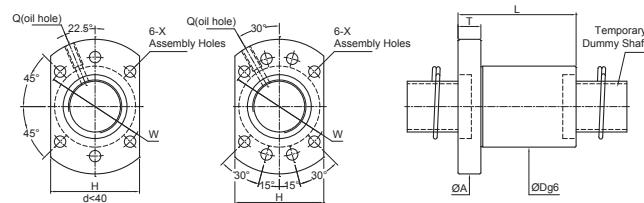
SCREW SIZE				MODIFIED LOAD CAPACITY(kgf)		BALLNUT DIMENSION										Nut Model NO.		
	O.D.	LEAD	BALL DIA.	EFFECTIVE TURNS	Dynamic (1×10 <sup>6</sup> REV.) Cam	Static Coam	O.D.	Length	Flange			Oil Hole Q	Assembly Hole X	STIFFNESS kgf/μm	Nut Model NO.			
36	10	6.35	3	2560	8250	70	58	108	17	90	36	82	I	M6x1P	11	52	FSDW3610F-3.0P	
		5	3970	13750	61	78	91	18	76	34	68	II	M6x1P	9	55	FSDW3610F-5.0P		
	5	3.175	4	1180	5200	60	42	91	18	76	34	68	II	M8x1P	9	40	FSDW4005B-4.0P	
40	10	6.35	5	4290	15290	65	78	95	18	80	36	72	II	M8x1P	9	59	FSDW4010F-5.0P	
	20	6.35	4	3480	11990	65	110	98	18	83	37	74	I	M8x1P	11	48	FSDW4020F-4.0P	
	40	2	1810	5770														FSDW4040F-2.0P
50	10	6.35	5	4780	19360	75	78	118	18	100	46	92	II	M8x1P	11	70	FSDW5010F-5.0P	

## Note:

1.Cam and Coam represent the enhanced dynamic- and static load. Their calculations referred to the standard of ISO-3408-5.

## 2. Stiffness of nut:

Stiffness values listed above are derived from theoretical formula to the elastic deformation between thread grooves and balls while axial load is 30% dynamic load rating.



Unit: mm

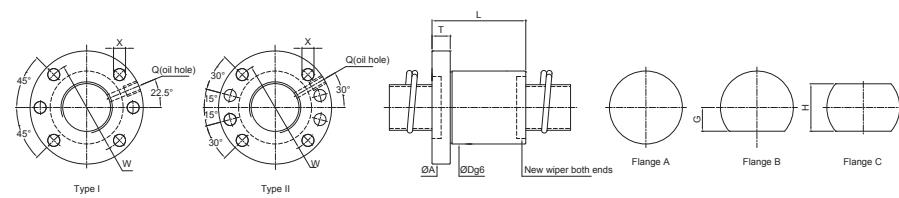
SCREW SIZE	BALL DIA.	EFFECTIVE TURNS	BASIC RATE LOAD(kgf)		BALLNUT DIMENSION												
			Dynamic (1x10 <sup>6</sup> REV.)	Static Cam	O.D.	Length	Flange			Oil Hole	Assembly Hole	STIFFNESS	Nut Model NO.				
O.D.	Lead				D	L	A	T	W	G	H	Q	X	kgf/μm			
16	5	3.175	3	1050	2200	28	42	48	10	38	20	40	M6×1P	5.5	17	FSIN1605B-3.0P	
20	5	3.175	3	1200	2780	36	44	58	12	47	22	44	M6×1P	6.5	24	FSIN2005B-3.0P	
	4	1530	3.720	1530	3720	50	50	50	15	45	30	30		25	25	FSIN2005B-4.0P	
25	5	3.175	3	1320	3540	40	44	62	12	51	24	48	M6×1P	6.5	28	FSIN2505B-3.0P	
	4	1700	4.720	1700	4720	50	50	50	15	45	30	30		37	37	FSIN2505B-4.0P	
30	10	4.762	4	2810	6610	85	62	12	51	24	48	M6×1P	6.5	32	FSIN2510D-4.0P		
	5	3.175	3	1470	4560	47									37	37	FSIN3205B-3.0P
32	5	3.175	4	1900	6090	50	50	80	12	65	31	62	M6×1P	9	50	FSIN3205B-4.0P	
	6	2690	9150	2690	9150	66									69	69	FSIN3205B-6.0P
35	10	6.35	3	3680	8750	50	74	80	12	65	31	62	M6×1P	9	39	FSIN3210F-3.0P	
	4	4720	11670	4720	11670	80	80	93	15	78	35	70	M8×1P	9	50	FSIN3210F-4.0P	
40	5	3.175	4	2090	7670	54									52	52	FSIN4005B-4.0P
	6	2940	11510	2940	11510	66	93	15	78	35	70	M8×1P	9	77	77	FSIN4005B-6.0P	
	10	6.35	3	4140	11130	74	93	15	78	35	70	M8×1P	9	46	46	FSIN4010F-3.0P	
	4	5310	14850	5310	14850	82									60	60	FSIN4010F-4.0P
50	10	6.35	3	4610	14090	78									54	54	FSIN5010F-3.0P
	4	5890	18780	5890	18780	75	88	110	18	93	42.5	85	M8×1P	11	70	70	FSIN5010F-4.0P
		6	8350	28170	106										103	103	FSIN5010F-6.0P

**Note:**

1.Cam and Coam represent the enhanced dynamic- and static load. Their calculations referred to the standard of DIN 69051.

**2. Stiffness of nut:**

Stiffness values listed above are derived from theoretical formula to the elastic deformation between thread grooves and balls while axial load is 30% dynamic load rating.



單位:mm

SCREW SIZE	BALL DIA.	EFFECTIVE TURNS	BASIC RATE LOAD(kgf)		BALLNUT DIMENSION											
			Dynamic (1x10 <sup>6</sup> REV.)	Static Cam	O.D.	Length	Flange			Oil Hole	Assembly Hole	STIFFNESS	Nut Model NO.			
O.D.	Lead				D	L	A	T	W	G	H	Q	X	kgf/μm		
15	5	3	4	1210	1530	28	39	48	10	38	20	40	M6×1P	5.5	22	FSDN1605V-4.0P
16	10	3	3	950	1650	28	47	48	10	38	20	40	M6×1P	5.5	17	FSDN1605V-3.0P
	16	3	3	910	1600	28	64	48	10	38	20	40	M6×1P	5.5	17	FSDN1605V-3.0P
20	5	3.175	4	1570	3270	36	40	58	10	47	22	44	M6×1P	6.6	28	FSDN2005B-4.0P
	20	3.175	4	1460	3120	36	58	58	10	47	22	44	M6×1P	6.6	28	FSDN2020B-4.0P
25	5	3.175	5	2130	3740	40	46	62	10	51	24	48	M6×1P	6.6	41	FSDN2505B-5.0P
	10	3.175	4	1740	4120	40	60	62	10	51	24	48	M6×1P	6.6	33	FSDN2510B-4.0P
30	5	3.175	6	2800	8190	50	53	80	12	65	31	62	M6×1P	9	59	FSDN3205B-6.0P
	10	3.969	4	3240	8480	50	73	80	12	65	31	62	M6×1P	9	52	FSDN3210C-5.0P
32	20	3.969	4	2600	6640	50	101	80	12	65	31	62	M6×1P	9	42	FSDN3220C-4.0P
	32	4	4	2460	6340	50	82	80	12	65	31	62	M6×1P	9	41	FSDN3232C-4.0P
38	10	6.35	5	6500	15610	63	78	93	15	78	35	70	M8×1P	9	64	FSDN3810F-5.0P
	20	6.35	4	5250	12240	63	107	93	15	78	35	70	M8×1P	9	52	FSDN3820F-4.0P
	40	4	4	4940	11770	63	104	93	15	78	35	70	M8×1P	9	51	FSDN3840F-4.0P

**Note:**

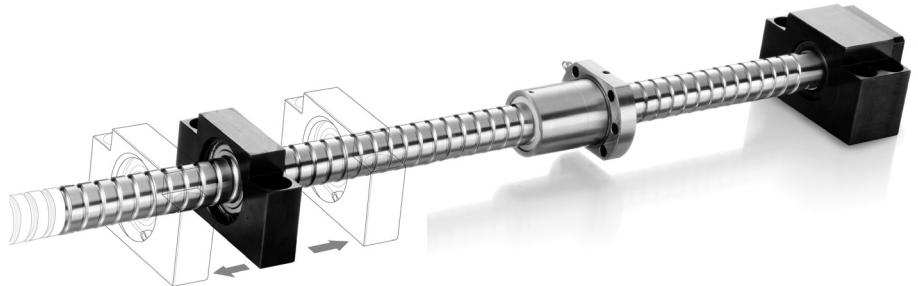
1.Cam and Coam represent the enhanced dynamic- and static load. Their calculations referred to the standard of DIN 69051.

**2. Stiffness of nut:**

Stiffness values listed above are derived from theoretical formula to the elastic deformation between thread grooves and balls while axial load is 30% dynamic load rating.

# 15 FA Series

The new circulation design of **PMI** FA series of precision ballscrews carried out the advantages of High Speed, Low Noise, Efficiency, and Standardization for different kinds of application.



## Features

### Short Delivery

In order to achieve the purpose of standardized stock for short delivery time, the precise outer diameter of screw shaft is used for support bearing seat.

### Flexibility of stroke length

Due to the precise outer diameter of screw shaft is used for support bearing seat, the specific length of shaft can be freely cut from standardized screw shaft. Therefore, the flexible stroke length is allowable for simple support end.

### High accuracy with reasonable price

The accuracy can be as higher as JIS C5 grade and with axial clearance within  $5 \mu\text{m}$ .

### Space saving

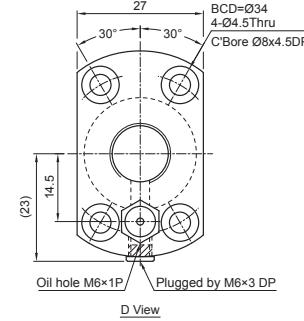
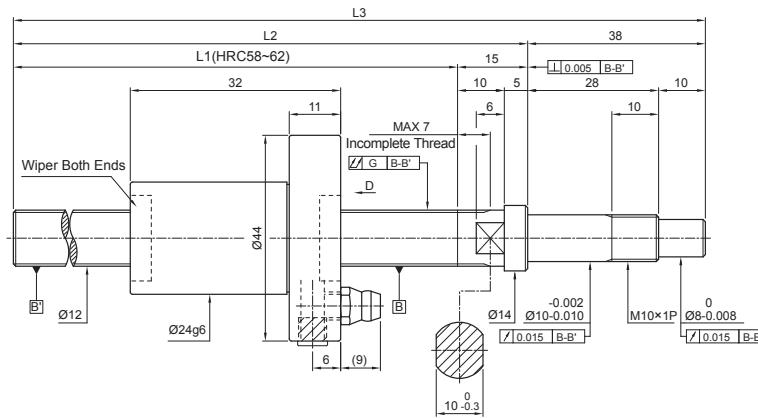
Comparing with conventional ballscrew, the outer diameter of nut is reduced as 20~25% as much, and the nut length is also shorter than usual. Therefore, the mounting space can be saved from engineering design.

### High speed and lower noise

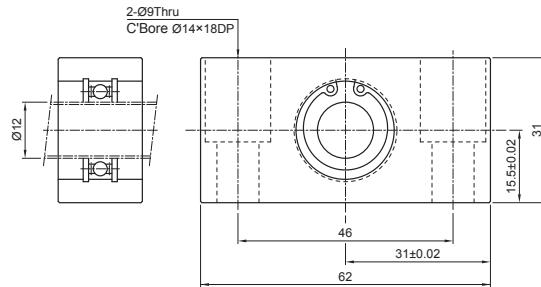
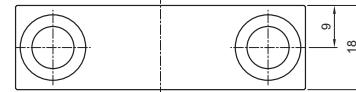
Taking advantage of **PMI** unique technology of high-speed, noise reduction, the rotation speed can be as higher as 5000 rpm. Moreover, due to the design of special circulation system, the vibration and noise(6 db less) are much lower than conventional type of ballscrew.

### Application range

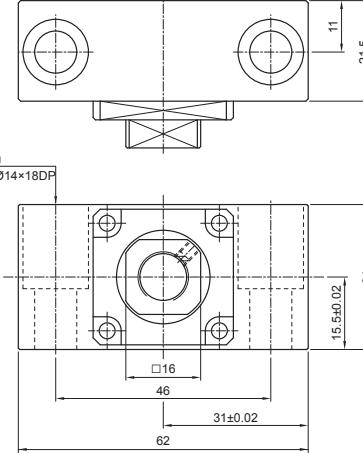
Semiconductor equipments, Measuring devices, Inspection equipments, Medical equipments, Automation, Light load machining, Glue depositing, and other precision motion and positioning applications.

**FA** FA Series Ballscrews  
Screw Dia. Ø12 Lead05


Supported End



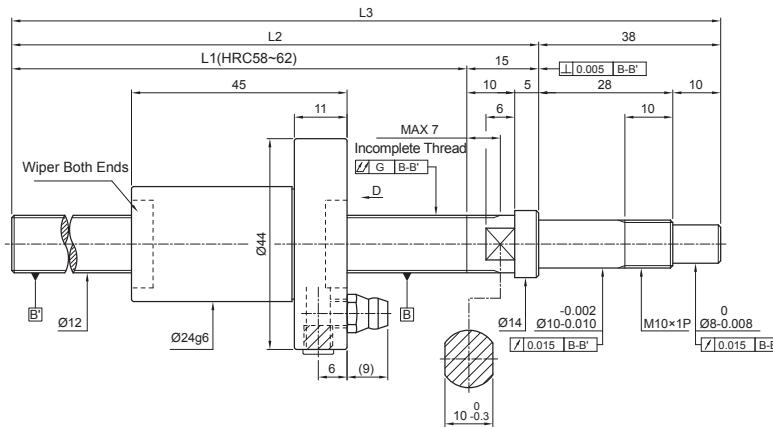
Fixed End



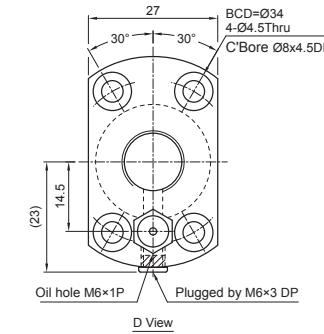
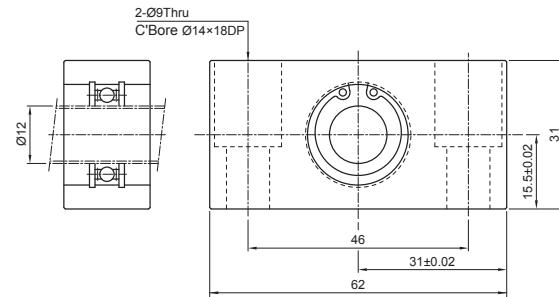
Unit: mm

Model No.	Screw Dia.	Lead	Modified Load Capacity(kgf)		Screw Shaft Length			Accuracy Grade		Axial Play	Lead Accuracy			Tolerances	Fixed End-bearing (kgf)		Supported End-bearing (kgf)	
	d	I	Dynamic Cam	Static Coam	L1	L2	L3				Specified Travel (T)	Accumulated reference lead deviation (E)	Lead Derivation in random 300mm (e300)	Overall Radial Runout	Dynamic Ca	Static Co	Dynamic Ca	Static Co
BL012050400+A000	12	05	610	1190	347	362	400	C5		<0.005	0	0.023	0.018	0.065	546	265	196	106
BL012050600+A000	12	05	610	1190	547	562	600	C5		<0.005	0	0.027	0.018	0.090	546	265	196	106
BL012050900+A000	12	05	610	1190	847	862	900	C5		<0.005	0	0.035	0.018	0.150	546	265	196	106

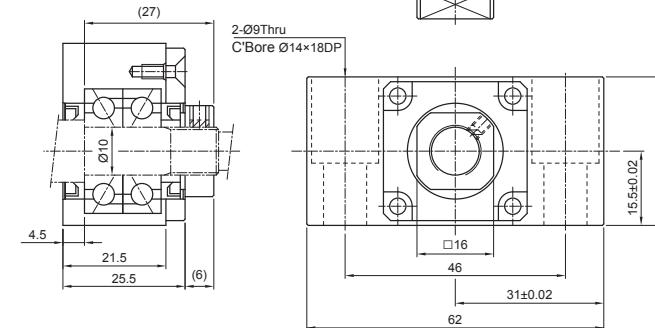
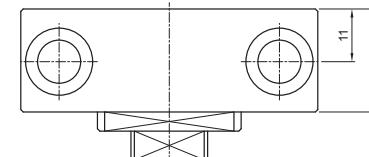
Coam and Cam are the modified static and dynamic load capacities, calculated according to ISO-3408-5



Supported End



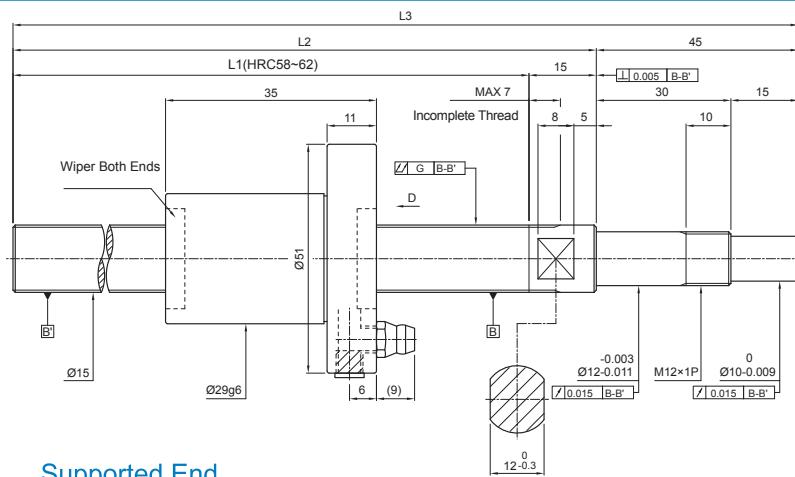
Fixed End



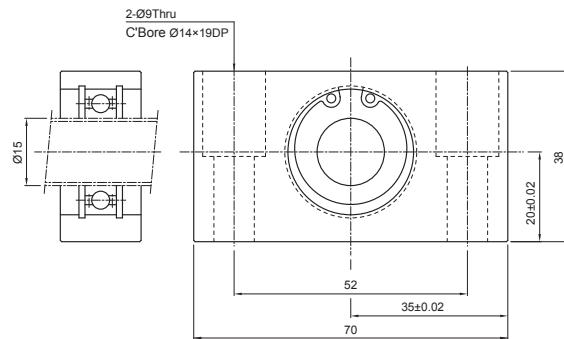
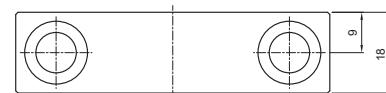
Unit: mm

Model No.	Screw Dia.	Lead	Modified Load Capacity(kgf)		Screw Shaft Length			Accuracy Grade		Axial Play	Lead Accuracy			Tolerances	Fixed End-bearing (kgf)		Supported End-bearing (kgf)	
	d	I	Dynamic Cam	Static Coam	L1	L2	L3				Specified Travel (T)	Accumulated reference lead deviation (E)	Lead Derivation in random 300mm (e300)	Overall Radial Runout	Dynamic Ca	Static Co	Dynamic Ca	Static Co
BL012100400+A000	12	10	590	1160	347	362	400	C5		<0.005	0	0.023	0.018	0.065	546	265	196	106
BL012100600+A000	12	10	590	1160	547	562	600	C5		<0.005	0	0.027	0.018	0.090	546	265	196	106
BL012100900+A000	12	10	590	1160	847	862	900	C5		<0.005	0	0.035	0.018	0.150	546	265	196	106

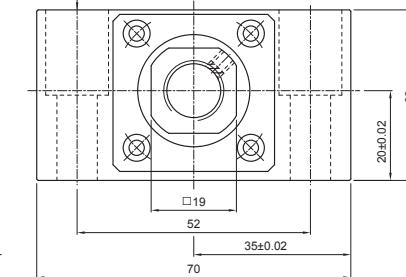
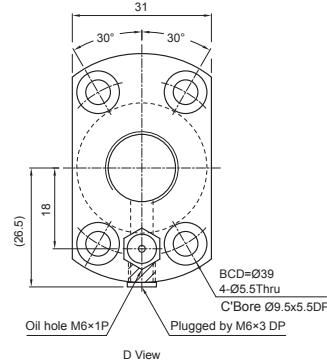
Coam and Cam are the modified static and dynamic load capacities, calculated according to ISO-3408-5

**FA** FA Series Ballscrews  
Screw Dia. Ø15 Lead05


Supported End



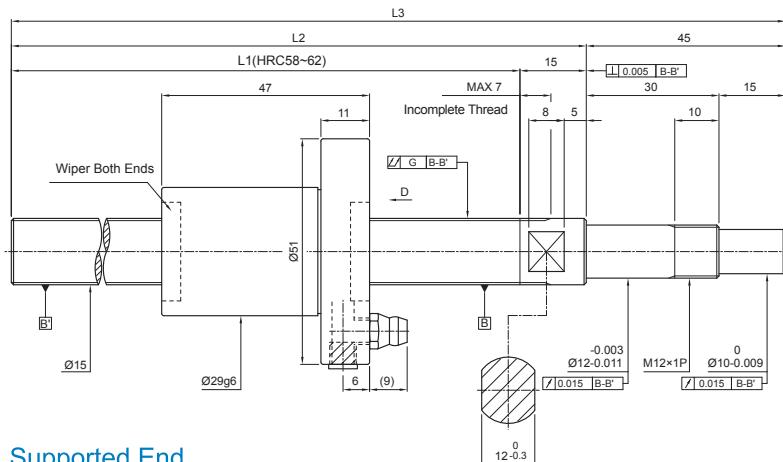
Fixed End



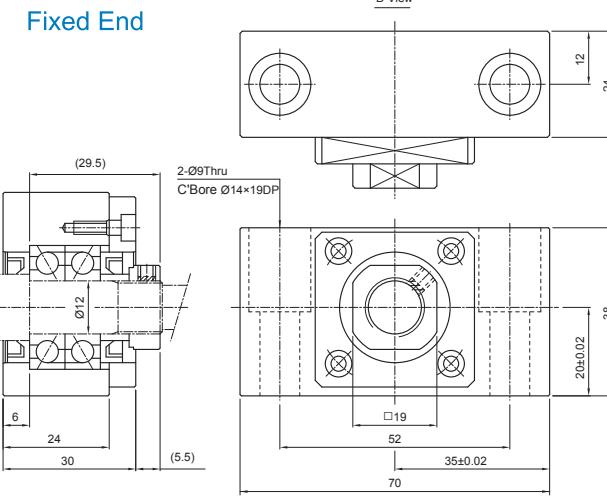
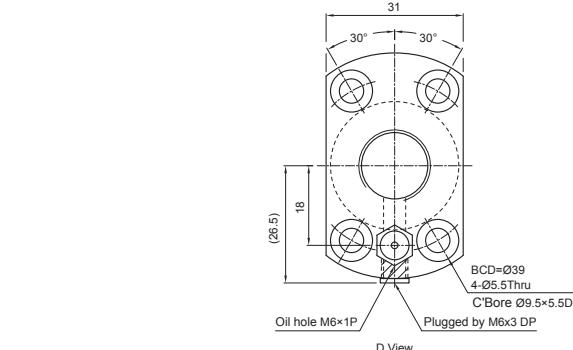
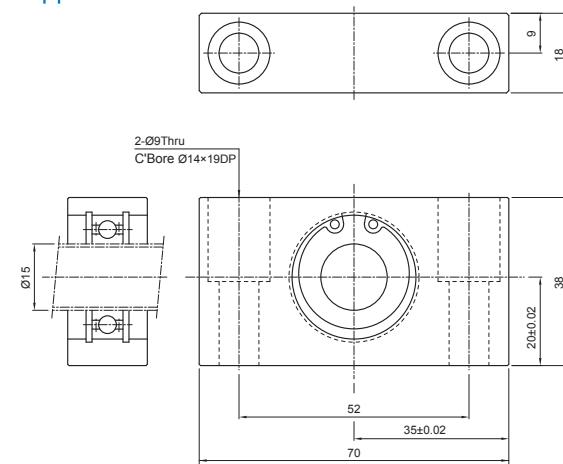
Unit: mm

Model No.	Screw Dia.	Lead	Modified Load Capacity(kgf)		Screw Shaft Length			Accuracy Grade		Axial Play	Lead Accuracy			Tolerances	Fixed End-bearing (kgf)		Supported End-bearing (kgf)	
	d	I	Dynamic Cam	Static Coam	L1	L2	L3				Specified Travel (T)	Accumulated reference lead deviation (E)	Lead Derivation in random 300mm (e300)	Overall Radial Runout	Dynamic Ca	Static Co	Dynamic Ca	Static Co
BL015050500+A000	15	05	850	1640	440	455	500	C5		<0.005	0	0.025	0.018	0.060	592	304	372	204
BL015051000+A000	15	05	850	1640	940	955	1000	C5		<0.005	0	0.040	0.018	0.120	592	304	372	204
BL015051450+A000	15	05	850	1640	1390	1405	1450	C5		<0.005	0	0.054	0.018	0.190	592	304	372	204

Coam and Cam are the modified static and dynamic load capacities, calculated according to ISO-3408-5



Supported End



Unit: mm

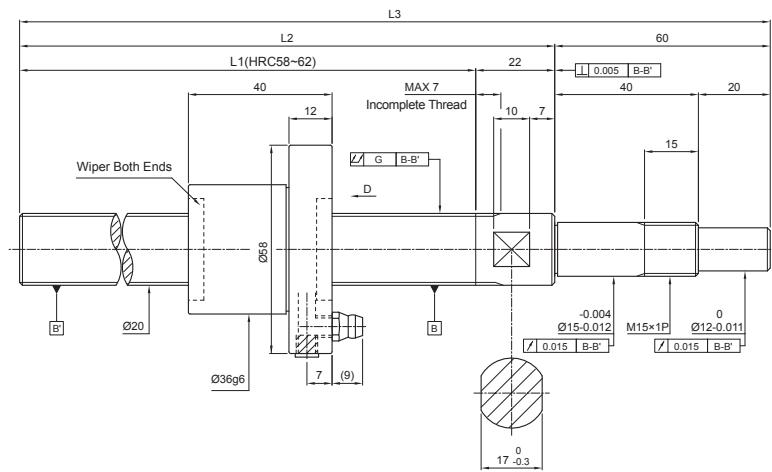
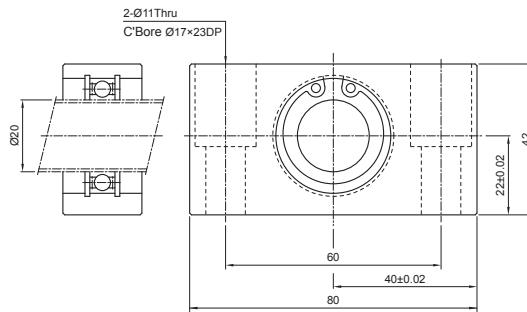
Model No.	Screw Dia.	Lead	Modified Load Capacity(kgf)		Screw Shaft Length			Accuracy Grade		Axial Play	Lead Accuracy			Tolerances	Fixed End-bearing (kgf)		Supported End-bearing (kgf)	
	d	I	Dynamic Cam	Static Coam	L1	L2	L3				Specified Travel (T)	Accumulated reference lead deviation (E)	Lead Derivation in random 300mm (e300)	Overall Radial Runout	Dynamic Ca	Static Co	Dynamic Ca	Static Co
BL015100500+A000	15	10	840	1610	440	455	500	C5		<0.005	0	0.025	0.018	0.060	592	304	372	204
BL015101000+A000	15	10	840	1610	940	955	1000	C5		<0.005	0	0.040	0.018	0.120	592	304	372	204
BL015101450+A000	15	10	840	1610	1390	1405	1450	C5		<0.005	0	0.054	0.018	0.190	592	304	372	204

Coam and Cam are the modified static and dynamic load capacities, calculated according to ISO-3408-5

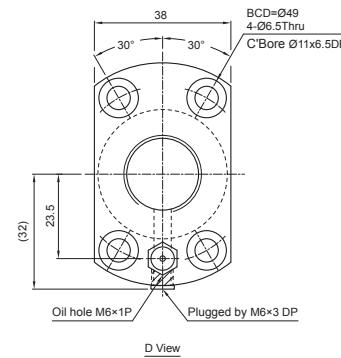
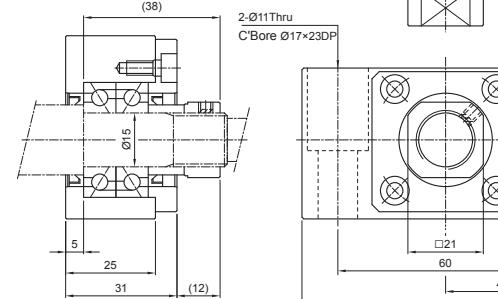
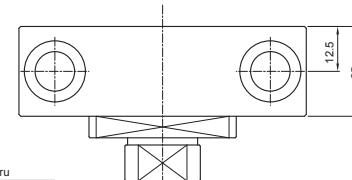
BALLSCREW

Specifications | FA Series

## Supported End



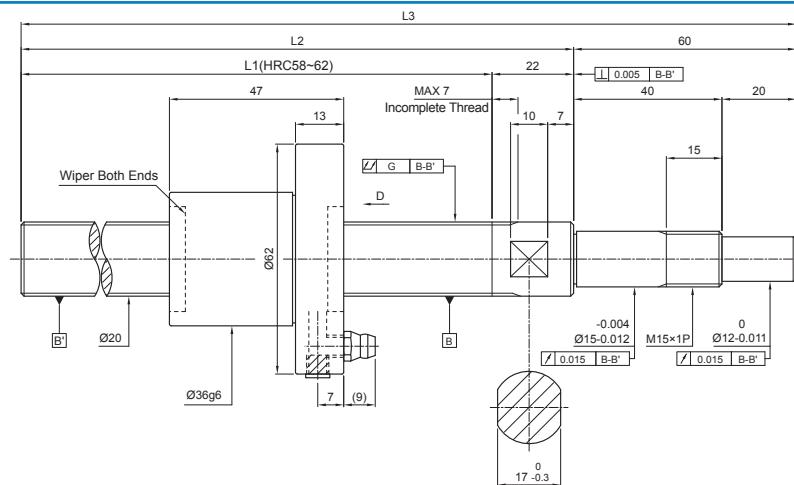
## Fixed End



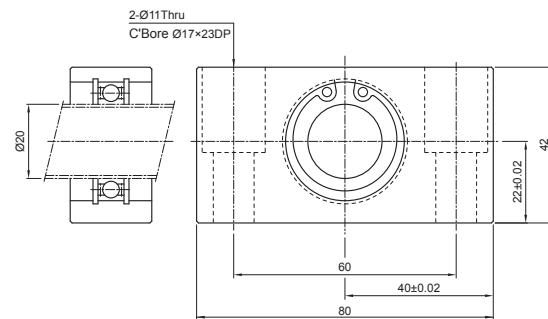
Unit: mm

Model No.	Screw Dia.	Lead	Modified Load Capacity(kgf)		Screw Shaft Length			Accuracy Grade		Axial Play	Lead Accuracy			Tolerances	Fixed End-bearing (kgf)		Supported End-bearing (kgf)	
	d	I	Dynamic Cam	Static Coam	L1	L2	L3				Specified Travel (T)	Accumulated reference lead deviation (E)	Lead Derivation in random 300mm (e300)		Overall Radial Runout	Dynamic Ca	Static Co	Dynamic Ca
BL020050600+A000	20	05	1300	3030	518	540	600	C5		<0.005	0	0.030	0.018	0.075	622	352	408	252
BL020051000+A000	20	05	1300	3030	918	940	1000	C5		<0.005	0	0.040	0.018	0.120	622	352	408	252
BL020051450+A000	20	05	1300	3030	1368	1390	1450	C5		<0.005	0	0.054	0.018	0.190	622	352	408	252

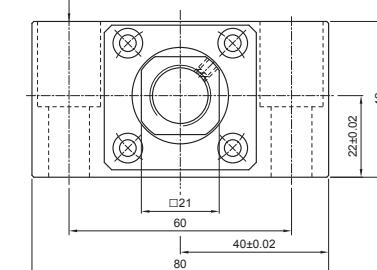
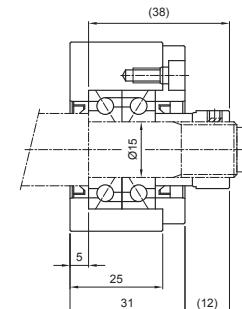
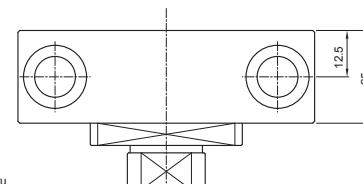
Coam and Cam are the modified static and dynamic load capacities, calculated according to ISO-3408-5.

**FA** FA Series Ballscrews  
Screw Dia. Ø20 Lead10


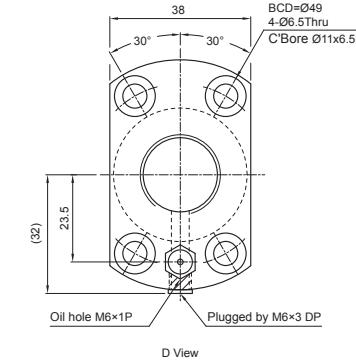
Supported End



Fixed End

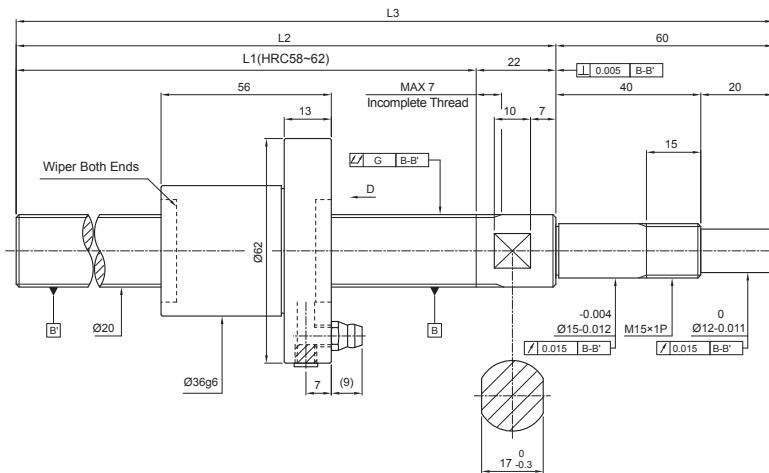


Unit: mm

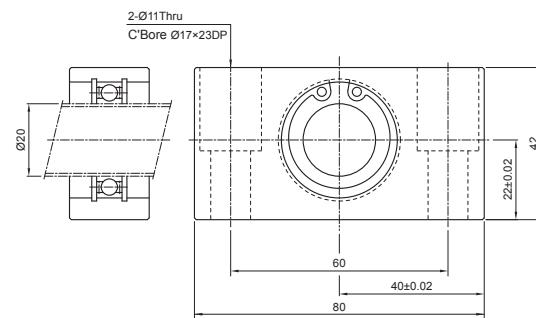
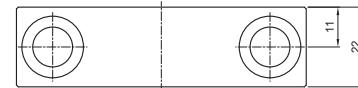


Model No.	Screw Dia.	Lead	Modified Load Capacity(kgf)		Screw Shaft Length			Accuracy Grade		Axial Play	Lead Accuracy			Tolerances		Fixed End-bearing (kgf)		Supported End-bearing (kgf)	
	d	I	Dynamic Cam	Static Coam	L1	L2	L3				Specified Travel (T)	Accumulated reference lead deviation (E)	Lead Derivation in random 300mm (e300)	Overall Radial Runout	Dynamic Ca	Static Co	Dynamic Ca	Static Co	
BL020100600+A000	20	10	990	2220	518	540	600	C5		<0.005	0	0.030	0.018	0.075	622	352	408	252	
BL020101000+A000	20	10	990	2220	918	940	1000	C5		<0.005	0	0.040	0.018	0.120	622	352	408	252	
BL020101450+A000	20	10	990	2220	1368	1390	1450	C5		<0.005	0	0.054	0.018	0.190	622	352	408	252	

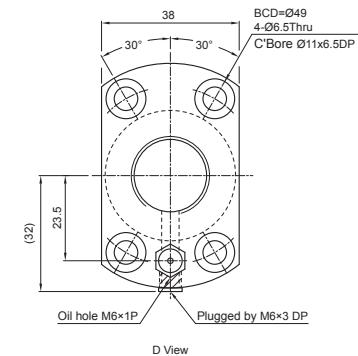
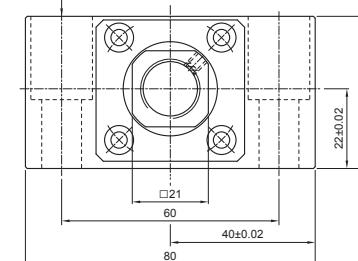
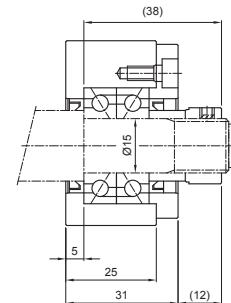
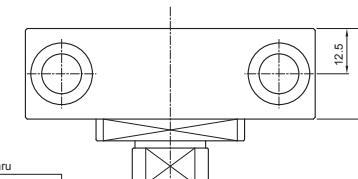
Coam and Cam are the modified static and dynamic load capacities, calculated according to ISO-3408-5



Supported End



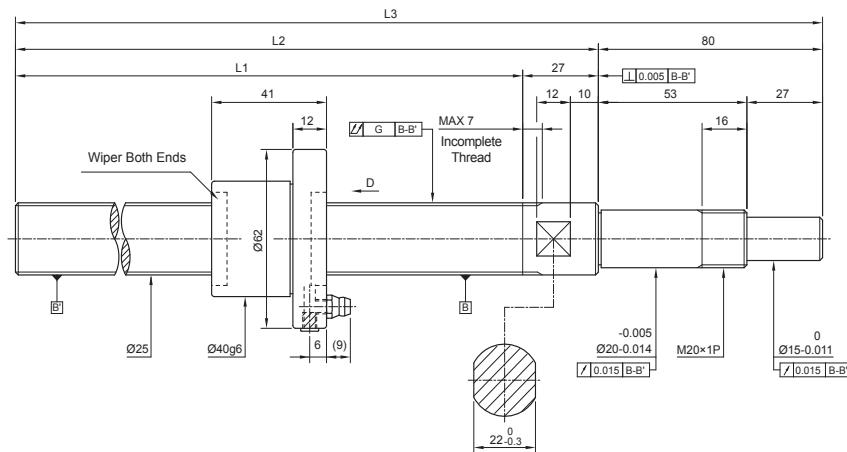
Fixed End



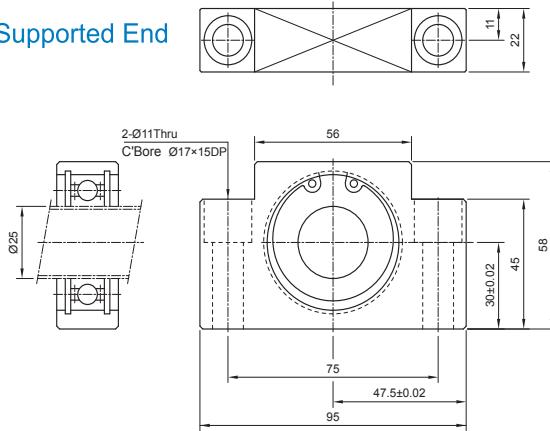
Unit: mm

Model No.	Screw Dia.	Lead	Modified Load Capacity(kgf)		Screw Shaft Length			Accuracy Grade		Axial Play	Lead Accuracy			Tolerances	Fixed End-bearing (kgf)		Supported End-bearing (kgf)	
	d	I	Dynamic Cam	Static Coam	L1	L2	L3				Specified Travel (T)	Accumulated reference lead deviation (E)	Lead Derivation in random 300mm (e300)	Overall Radial Runout	Dynamic Ca	Static Co	Dynamic Ca	Static Co
BL020200600+A000	20	20	670	1450	518	540	600	C5		<0.005	0	0.027	0.018	0.075	622	352	408	252
BL020201000+A000	20	20	670	1450	918	940	1000	C5		<0.005	0	0.040	0.018	0.120	622	352	408	252
BL020201450+A000	20	20	670	1450	1368	1390	1450	C5		<0.005	0	0.054	0.018	0.190	622	352	408	252

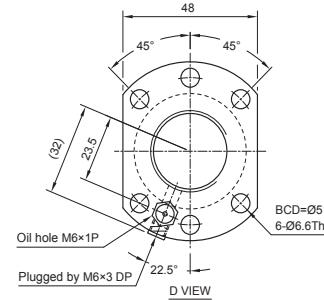
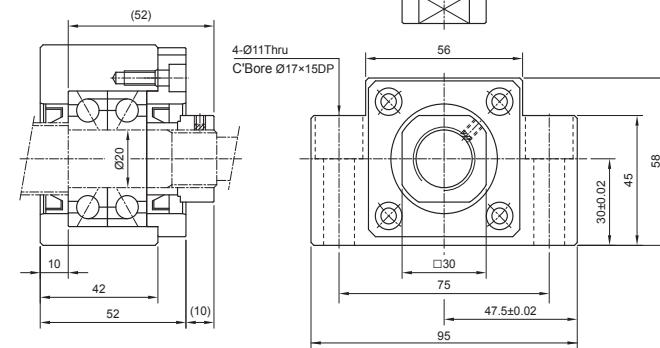
Coam and Cam are the modified static and dynamic load capacities, calculated according to ISO-3408-5

**FA** FA Series Ballscrews  
Screw Dia. Ø25 Lead05


Supported End



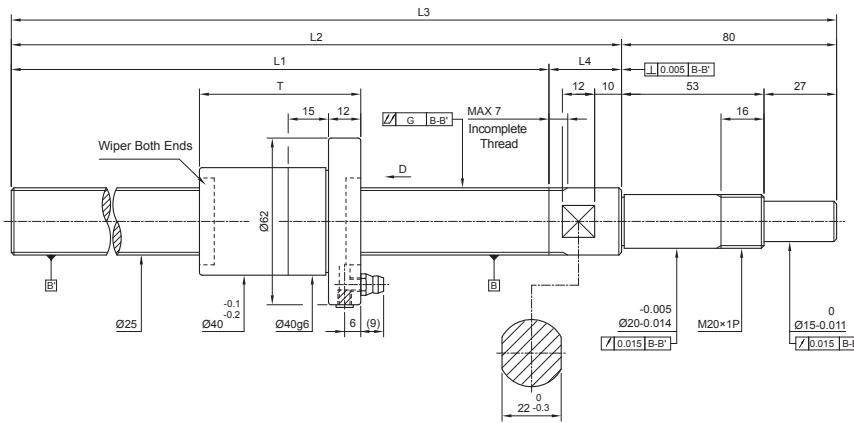
Fixed End



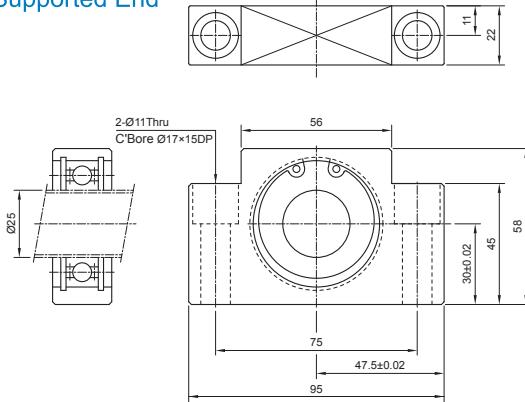
Unit: mm

Model No.	Screw Dia.	Lead	Modified Load Capacity(kgf)		Screw Shaft Length			Accuracy Grade		Axial Play	Lead Accuracy			Tolerances	Fixed End-bearing (kgf)		Supported End-bearing (kgf)	
	d	I	Dynamic Cam	Static Coam	L1	L2	L3				Specified Travel (T)	Accumulated reference lead deviation (E)	Lead Derivation in random 300mm (e300)	Overall Radial Runout	Dynamic Ca	Static Co	Dynamic Ca	Static Co
BL025050600+A000	25	05	1440	3840	493	520	600	C5		<0.005	0	0.027	0.018	0.050	1480	847	1030	597
BL025051000+A000	25	05	1440	3840	893	920	1000	C5		<0.005	0	0.040	0.018	0.085	1480	847	1030	597
BL025051450+A000	25	05	1440	3840	1343	1370	1450	C5		<0.005	0	0.054	0.018	0.130	1480	847	1030	597

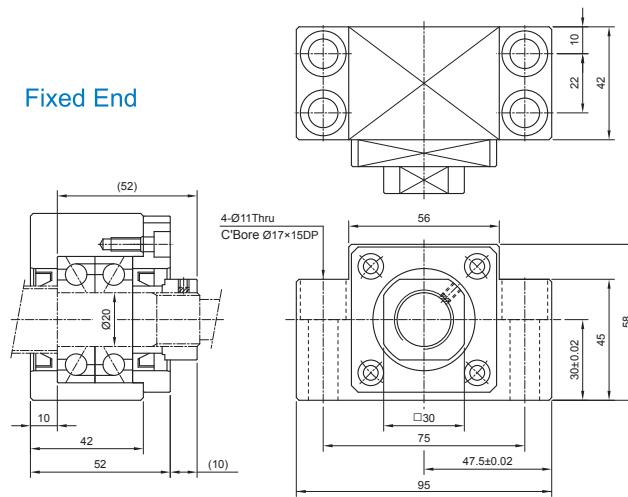
Coam and Cam are the modified static and dynamic load capacities, calculated according to ISO-3408-5

**FA** FA Series Ballscrews  
Screw Dia. Ø25 Lead10, 20, 25


## Supported End



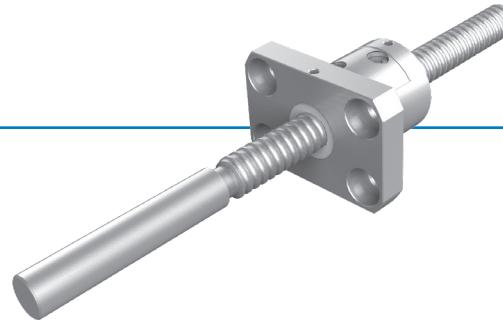
## Fixed End



Unit: mm

Model No.	Screw Dia.	Lead	Modified Load Capacity(kgf)		Screw Shaft Length				Nut	Accuracy Grade		Lead Accuracy			Tolerances	Fixed End-bearing (kgf)		Supported End-bearing (kgf)	
	d	I	Dynamic Cam	Static Coam	L1	L2	L3	L4				Specified Travel (T)	Accumulated reference lead deviation (E)	Lead Derivation in random 300mm (e300)		Overall Radial Runout	Dynamic Ca	Static Co	Dynamic Ca
BL025100600+A000	25	10	1440	3840	493	520	600	27	60	C5	<0.005	0	0.027	0.018	0.050	1480	847	1030	597
BL025101000+A000	25	10	1440	3840	893	920	1000	27	60	C5	<0.005	0	0.040	0.018	0.085	1480	847	1030	597
BL025101450+A000	25	10	1440	3840	1343	1370	1450	27	60	C5	<0.005	0	0.054	0.018	0.130	1480	847	1030	597
BL025200600+A000	25	20	750	1840	494	520	600	26	60	C5	<0.005	0	0.027	0.018	0.050	1480	847	1030	597
BL025201000+A000	25	20	750	1840	894	920	1000	26	60	C5	<0.005	0	0.040	0.018	0.085	1480	847	1030	597
BL025201450+A000	25	20	750	1840	1344	1370	1450	26	60	C5	<0.005	0	0.054	0.018	0.130	1480	847	1030	597
BL025250600+A000	25	25	730	1810	490	520	600	30	71	C5	<0.005	0	0.027	0.018	0.050	1480	847	1030	597
BL025251000+A000	25	25	730	1810	890	920	1000	30	71	C5	<0.005	0	0.040	0.018	0.085	1480	847	1030	597
BL025251450+A000	25	25	730	1810	1340	1370	1450	30	71	C5	<0.005	0	0.054	0.018	0.130	1480	847	1030	597

Coam and Cam are the modified static and dynamic load capacities, calculated according to ISO-3408-5



## 16.1 Product Features

### High Applicability Shaft Ends

Without heat treating processes on the shaft ends, the center holes on both side will be reserved.

The shaft ends could be easily manufactured to favored size.

### Short Delivery

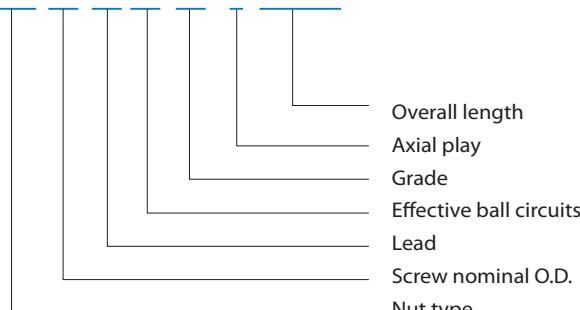
Standardized stock for general specification's thread length and length of blank shaft ends.

### Lower Price

The accuracy can be as good as JIS C5 and C7 grade and with standardized axial clearance for the reason that can be cost down and the price will be cheaper.

### PMI Model No.

PTR 20 10 B1 C7 S -1500



#### Nut type:

PPR: FSMC (Miniature Series)

PTR: FSDC (End Deflector Series)

#### Effective ball circuits:

PPR (Miniature Series)

A1: 1.5x1 circuits / B1: 2.5x1 circuits

PTR (End Deflector Series)

T2: 2 circuits / T3: 3 circuits

Grade	Axial play	Z	T	S	N
	0 (Preload))	0.005 or less	0.010 or less	0.030 or less	
C5	C5Z	C5T	-	-	
C7	-	-	C7S	C7N	

## 16.2 PPR(Miniature Series) - Features

### Space Saving

External circulation system, it don't need to have at least one end with complete thread to the end of Ballscrew for Ballnut assembly to screw shaft. And the special design of ballnut, so the size of ballnut is same as internal circulation system of ballnut, Space saving.

### Circulation

By way of 3D Spline designed pathway for circulation system, and has enhanced the smooth circulation of ball, that can reduce the wearing and increase the life of ballscrew.

## 16.3 PTR(End Deflector Series) - Features

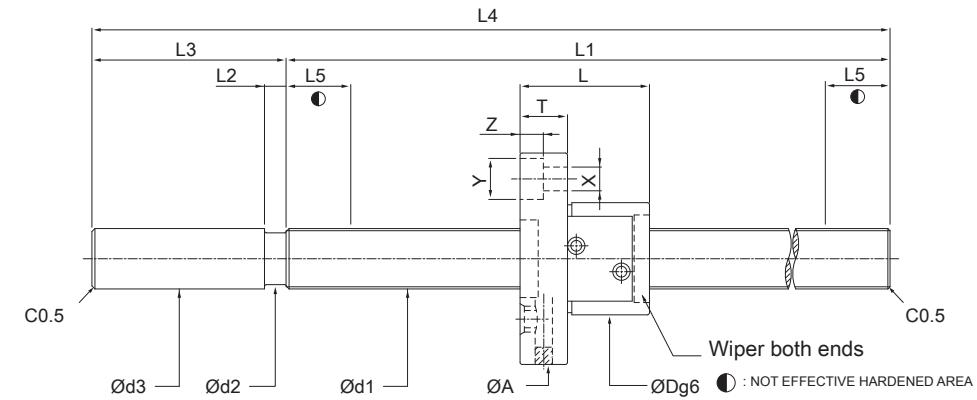
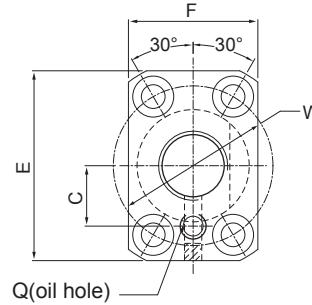
### Space Saving

The ballnut diameter reduces 20%~25% substantially and the length of nut is shorter.

### Low Noise

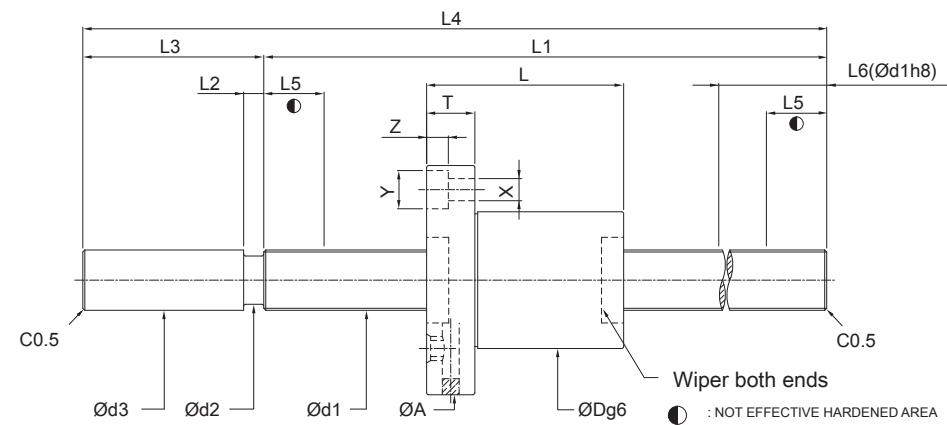
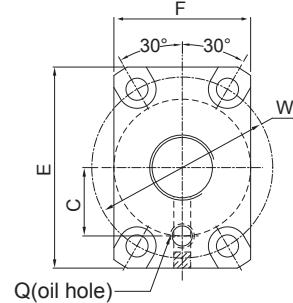
The average and accurate ball circle diameter (BCD) through whole threads make the ballscrews to obtain the stable and consistent drag torque as well as to reduce the noise.

The audio frequency is low and deep due to the designed of plastic circulation system.



Unit:mm

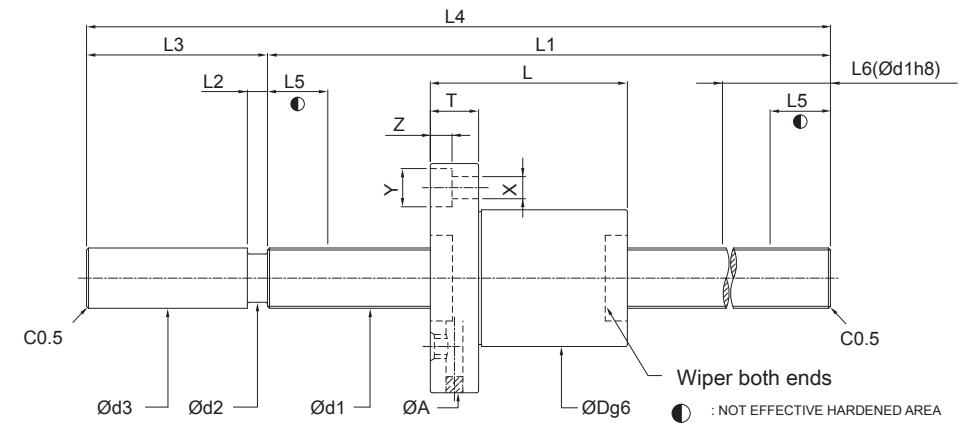
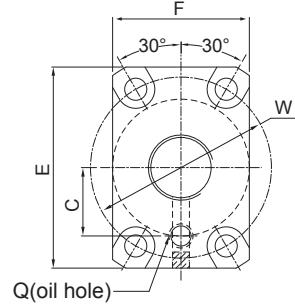
Model No.	SCREW SIZE		EFFECTIVE TURNS	BASIC RATE LOAD(kgf)		SCREW SHAFT LENGTH						SCREW SHAFT LENGTH			NUT		FLANGE					OIL HOLE		BOLT		
	O.D d1	LEAD		Dynamic (1×10 <sup>6</sup> REV.) Ca	Static Co	L1	L2	L3	L4	L5		L6	d2	d3(h8)	Dg6	L	A	T	W	E	F	C	Q	X	Y	Z
PPR0802B1C5T-0220	8	2	2.5×1	190	290	160	3	60	220	10		160	6.5	10	20	25	40	6	30	36	25	-	-	4.5	8	4.4
PPR1202B1C5T-0220	12	2	2.5×1	240	450	160	5	60	220	10		160	10.5	12	25	31	45	10	35	41	28	13	M6	4.5	8	4.4
PPR1202B1C5T-0300						240			300	15		240														



Unit:mm

Model No.	SCREW SIZE		EFFECTIVE TURNS	MODIFIED LOAD CAPACITY(kgf)		SCREW SHAFT LENGTH						SCREW SHAFT LENGTH			NUT		FLANGE					OIL HOLE		BOLT		
	O.D d1	LEAD		Dynamic (1×10 <sup>6</sup> REV.) Ca	Static Co	L1	L2	L3	L4	L5		L6	d2	d3(h8)	Dg6	L	A	T	W	E	F	C	Q	X	Y	Z
PTR1205T3C5T-0300 PTR1205T3C5T-0450	12	5	3	610	1190	240 390	5	60	300 450	10 15		240 390	9.7	12	30	32	50	10	40	45	32	15	M6	4.5	8	4.4
PTR1210T3C5T-0300 PTR1210T3C5T-0450	12	10	3	590	1160	240 390	5	60	300 450	10 15		240 390	9.9	12	30	45	50	10	40	45	32	15	M6	4.5	8	4.4
PTR1220T3C5T-0450 PTR1220T3C5T-0600	12	20	3	390	770	390 540	5	60	450 600	15		390 540	9.9	12	30	54	50	12	40	45	32	15	M6	4.5	8	4.4
PTR1505T3C5T-0300 PTR1505T3C5T-0450 PTR1505T3C5T-0600 PTR1505T3C5T-0750 PTR1505T3C5T-0900	15	5	3	850	1640	240 390 540 690 750 840		300 450	10		240 390 540 690 750 840		12	15	34	35	57	11	45	50	34	17	M6	5.5	9.5	5.4
PTR1510T3C5T-0300 PTR1510T3C5T-0450 PTR1510T3C5T-0600 PTR1510T3C5T-0750 PTR1510T3C5T-0900 PTR1510T3C5T-1100	15	10	3	840	1610	240 390 540 690 750 840 900 1040		300 450	10		240 390 540 690 750 840 900 1040		12	15	34	47	57	11	45	50	34	17	M6	5.5	9.5	5.4
PTR1520T2C5T-0450 PTR1520T2C5T-0600 PTR1520T2C5T-0750 PTR1520T2C5T-0900 PTR1520T2C5T-1000 PTR1520T2C5T-1100 PTR1520T2C5T-1300	15	20	2	560	1050	390 540 690 750 840 940 1040 1240		450 600 750 900	15		390 540 690 750 840 940 1040 1240		12	15	34	58	57	12	45	50	34	17	M6	5.5	9.5	5.4
PTR2005T3C5T-0400 PTR2005T3C5T-0600 PTR2005T3C5T-0800 PTR2005T3C5T-1000	20	5	3	1000	2240	320 520 720 920		400 520 720 920	15		320 520 720 920		17	20	44	35	67	11	55	60	44	22	M6	5.5	9.5	5.4
PTR2010T3C5T-0600 PTR2010T3C5T-0800 PTR2010T3C5T-1000 PTR2010T3C5T-1300 PTR2010T3C5T-1500	20	10	3	1530	3280	515 715 915 1215 1415		600 800 1000 1300 1500	15		515 715 915 1215 1415		16.5	20	46	52	74	13	59	66	46	24	M6	6.6	11	6.5

Coam and Cam are the modified static and dynamic load capacities, calculated according to ISO-3408-5



Unit:mm

Model No.	SCREW SIZE		EFFECTIVE TURNS	MODIFIED LOAD CAPACITY(kgf)		SCREW SHAFT LENGTH						SCREW SHAFT LENGTH			NUT		FLANGE					OIL HOLE		BOLT			
	O.D d1	LEAD		Dynamic (1×10 <sup>6</sup> REV.) Ca	Static Co	L1	L2	L3	L4	L5		L6	d2	d3(h8)	Dg6	L	A	T	W	E	F	C	Q	X	Y	Z	
PTR1205T3C7S-0450	12	5	3	610	1190	390	5	60	450	15		180	9.7	12	30	32	50	10	40	45	32	15	M6	4.5	8	4.4	
PTR1210T3C7S-0600	12	10	3	590	1160	540	5	60	600	15		180	9.9	12	30	45	50	10	40	45	32	15	M6	4.5	8	4.4	
PTR1220T2C7S-0600	12	20	2	390	770	540	5	60	600	15		180	9.7	12	30	54	50	12	40	45	32	15	M6	4.5	8	4.4	
PTR1505T3C7S-0600	15	5	3	850	1640	540	5	60	600	15		230	12	15	34	35	57	11	45	50	34	17	M6	5.5	9.5	5.4	
PTR1510T3C7S-0450						390			450																		
PTR1510T3C7S-0600						540			600																		
PTR1510T3C7S-0750						690			750																		
PTR1510T3C7S-0900						840	5	60	900	15																	
PTR1510T3C7S-1000						940			1000																		
PTR1510T3C7S-1100						1040			1100																		
PTR1510T3C7S-1300						1240			1300																		
PTR1520T2C7S-0600						540			600																		
PTR1520T2C7S-0750						690			750																		
PTR1520T2C7S-0900						840	5	60	900	15																	
PTR1520T2C7S-1000						940			1000																		
PTR1520T2C7S-1100						1040			1100																		
PTR1520T2C7S-1300						1240			1300																		
PTR2005T3C7S-0600	20	5	3	1000	2240	520	5	80	600	15		230	17	20	44	35	67	11	55	60	44	22	M6	5.5	9.5	5.4	
PTR2010T3C7S-0600						515			600																		
PTR2010T3C7S-1000	20	10	3	1530	3280	915	10	85	1000	15		230	16.5	20	46	52	74	13	59	66	46	24	M6	6.6	11	6.5	
PTR2010T3C7S-1500						1415			1500																		

Coam and Cam are the modified static and dynamic load capacities,calculated according to ISO-3408-5

## 17.1 Preface

In recent years, more and more ballscrews are installed in various machines to meet the requirements of higher accuracy and better performance.

Ballscrews become one of the most widely used power transmission components. In CNC machines, ballscrews help improve their positioning accuracy and elongate their service life. Ballscrews are also increasingly used to replace ACME screws in manually operated machines.

A ballscrew is normally preloaded to minimize the backlash of machine movement. Even a high precision ballscrew will not provide good accuracy and long service life if it is not installed properly.

This article discusses primary ballscrew problems and their precautions. Some measuring procedures are also discussed to help users locate the cause of an abnormal backlash.

## 17.2 The Cause and Precautions of Ballscrew Problems

Three major categories of ballscrew problems and their precautions are discussed as follows

### 17.2.1 Unsmooth operation

#### 1. Defects from ballscrew manufacturing:

- (1) The return tube is not attached to the ball nut appropriately.
- (2) The track surface of the ballscrew spindle or the ball nut is too rough.
- (3) The roundness of the ball nut or the screw shaft is out of tolerance.
- (4) The lead or the pitch circle diameter of the ball nut / the shaft is out of tolerance.

#### 2. Over-travel:

Over-travel can damage the return tube and cause it to collapse or even break. When this happens, the steel balls will not circulate smoothly. They may break and damage the groove on the ball nut or the screw shaft under severe circumstances. Over-travel may happen during set-up or as the result of a limit switch failure or a machine collision. To prevent further damage, an over-traveled ballscrew should be checked or repaired by the manufacturer before it goes back to service.

#### 3. Misalignment:

Radial load exists if the center line of the ball nut's housing and the screw shaft's bearing support bracket are not aligned properly. The ballscrew unit may bend if this misalignment is too big. An abnormal wear may still happen even if the misalignment is not significant enough to cause a noticeable bending. The accuracy of a ballscrew unit will deteriorate rapidly if it is misaligned. The higher the preload is set in the nut, the more demanding the

alignment accuracy is required in the ballscrew.

#### 4. Foreign objects enter the ball path:

Machined chips get in the ball track. The chips or dust generated during machining processes may be trapped in the ball track if wiper kits are not used to keep them away from the surface of the ballscrew unit. This may cause unsmooth operation, deteriorate accuracy and reduce service life.

#### 5. Damaged return tube:

The return tube may collapse and cause the same problems as mentioned above if it is hit heavily during installation.

#### 6. The ball nut is not mounted properly on the nut housing:

Eccentric load exists when the mounted ball nut is tilted or misaligned. If this is the case, the motor current may fluctuate during rotation.

#### 7. Ballscrew unit is damaged during transportation

- (1) During installation, avoid nuts separating away from screw, otherwise the balls will get out of the nut, that lead to change of the preload and damage of the circulation system and wiper.
- (2) Due to the low friction coefficient, nuts will fall down because of its self weight during vertical deposition; this kind of damage should be avoided, once happened, it should be inspected by manufacturer preventing further damage.

### 17.2.2 Too much plays

#### 1. No preload or insufficient preload:

The ball nut will rotate and move downward by its self weight when a non-preloaded ballscrew is held vertically with the screw shaft constrained. A significant backlash may exist in a non-preloaded ballscrew unit. Therefore non-preload ballscrews are only used in the machinery, where operation resistance but not positioning accuracy low is the major concerned.

**PMI** can determine the correct amount of preload based on different applications. We can also preset the amount of preload before shipment. Be sure to clearly specify the operation condition of your application when you order a ballscrew unit.

#### 2. Inappropriate bearing selection and installation:

- (1) Angular ball bearings should be used in ballscrew installation. A ball bearing with high pressure angle specially designed for ballscrew installation is even a better choice. A regular deep groove ball bearing will generate a significant amount of axial play when axially loaded. It should not be used in this application.

(2) Two lock nuts and a spring washer should be used in the bearing installation to prevent them from getting loose in operation.

(3) The perpendicularity between the bearing seating face and the thread axis of the bearing locknut on the ballscrew, or the parallelism between the opposite faces of the locknut is out of tolerance causing the bearing to tilt. The thread for bearing lock nut and the seating face of a bearing in the ballscrew journal should be machined in one setting to ensure the perpendicularity. It is even better if they can be ground.

(4) If the bearing is not attached to the screw shaft properly, it would cause axial play under load. This problem may be caused by the bearing journal of the screw shaft being too long or the non-threaded part of the screw shaft being too short. To solve this problem used the collar.

### **3. Parallelism or flatness of the housing surface is out of tolerance:**

In a machine assembly, a shim bar is frequently located between the housing location surface and the machine body for adjustment purpose. The clearance of table movement may vary at different locations if the parallelism or flatness of any matching component is out of tolerance no matter they are ground or scraped.

### **4. The ball nut housing or the bearing housing is not rigid enough:**

The ball-nut-mounted housing or the bearing-mounted housing may deflect under components' weight or machining load if it is not rigid enough.

### **5. The ball nut housing or the bearing housing is not mounted properly:**

- (1) Ball-nut-seated screws become loose due to vibration and lack of a spring washer.
- (2) Ball-nut-seated screws are not seated firmly because the screws are too long or the thread holes on housing are too short.
- (3) Components may become loose due to vibration or lack of locating pin(s). Solid pins instead of spring pins should be used for locating purpose.
- (4) Not enough locking forces for fixing screw because of too short screws

### **6. The motor and the ballscrew spindle are not assembled properly:**

- (1) There will be a relative rotation between the motor shaft and the ballscrew spindle if the connecting coupling is not installed firmly or the coupling itself is not rigid enough.
- (2) Key is loose in the groove. Any inappropriate match among the hub, key, and key seat may cause these components to generate backlash.
- (3) Driving gears are not engaged properly or driving mechanism is not rigid. A timing belt

should be used to prevent slipping if the ballscrew is to be driven by a belt.

### **17.2.3 Fracture**

#### **1. Broken bearing ball:**

Cr-Mo steel is the most commonly used material for bearing balls. It takes about 1,400kg (3,080lb) to 1,600kg (3,520lb) to break a steel ball of 3.175 mm (1/8 in) diameter. The temperature of an under-lubricated or non-lubricated ballscrew raises substantially during operation. This temperature raise could make the bearing balls brittle or break which cause damage to the grooves of the ball nut or the ballscrew spindle consequently.

Therefore, lubricant replenishment should be considered during the design process. If an automatic lubricating system is not available, periodical grease replenishment should be scheduled as part of maintenance program

#### **2. Collapsed or broken return tube:**

Over-travel of the ball nut or an impact on the return tube could cause the return tube to collapse or break. This may block the path of bearing balls and cause them to slide instead of rolling and break eventually.

#### **3. Ballscrew shaft end breaks:**

(1) Inappropriate design: Sharp corners on the ballscrew spindle should be avoided to reduce local stress concentration.

(2) Bend of screw shaft journal: The seating surface of the bearing of the ballscrew and the thread axis of the bearing's lock nut are not perpendicular to each other or the opposite sides of the lock nut are not parallel to each other. This will cause the end of screw shaft to bend and eventually break. The amount of deflection at the end of the ballscrew shaft before and after the bearing's lock nut being tightened should not exceed 0.01 mm (0.0004 in).

(3) Radial force or fluctuating stress: Misalignment in the ballscrew installation creates abnormal fluctuating shear stress and causes the ballscrew to fail prematurely.

(4) It should be avoided, that the dimension of ball screw shaft end too much different designed from ball screw shaft section area.

#### **4. Influence of temperature raise on ball screw**

During the operation of ball screws, the accuracy of machine drive system will influenced by the raise of the temperature, especially for the high speed and high accuracy machines. Following factors affect the temperature raise of ball screws:

(1)Preload (2)Lubrication (3)Preloading torque

#### (1)The Influence of Preload

Increase the rigidity of ball screw nut in order to avoid the lost motion of the machine drive system, that means increase the preload of the nut to a certain standard. Once the nut being preloaded, the friction torque will be increase, making the temperature raised during operation. **PMI** recommended, that the preload force should be 1/3 of the maximal axial load and is not bigger then 10% of the dynamic load, in order to obtain the optimal life time and lower temperature raise effect.

#### (2) The Influence of Pretension

The elongation and deformation of ball screws because of heat will deteriorate the position accuracy. The amount of thermal elongation can be calculated by certain formula and compensated by preloading torque. The target value of the Pretension compensation is the negativ T value on the diagram. Too much Pretension will burn the support bearing. Therefor **PMI** recommended, that the pretention should smaller then the Pretension by 5°C; however when the ball screws diameter is over 50mm, it is not suitable for a preloading torque, that means large Pretension forces will be needed when the diameter is large and will burn down the support bearing. **PMI** recommended, that 5°C of temperature raise should be used as standard to compensate the valueT (about -0.02~0.03mm every 1000mm of ball screw)

#### (3) The Influence of Lubrication

The choice of the lubrication will directly effect the temperature raise of the ball screws. The ball screws of **PMI** should be lubricated by oil or grease. Normaly lubrication oil for bearings will be recommended as ball screw lubrication, and grease from lithium soap will be recommended as lubrication grease. The choice of viscosity of the lubrication should be according to the operation speed, the working temperature, and the situation of load.

Low viscosity lubrication should be choosed during high speed and low load situation; high viscosity lubrication during low speed and high load situation. Normally, viscosity range of lubrication will be recommended at 32~68cSt (ISO VG 32~68)(DIN51519) during 40°C, high speed; viscosity range of lubrication will be recommended over 90cSt(ISO VG 90) during 40°C, low speed. By application of high speed and heavy load, force cooling must be used in order to reduce the temperature, and using hollow ball screw or cooling oil though nut to meet the cooling consequent.

		Standard Housing Diameter Tolerance																				
Diametrical range		e7	e8	e9	f6	f7	f8	g5	g6	h5	h6	h7	h8	h9	js5	js6	js7	k5	k6	m5	m6	n6
-	3	-14 -24	-14 -28	-14 -39	-6 -12	-6 -16	-6 -20	-2 -6	-2 -8	0 -4	0 -6	0 -10	0 -14	0 -25	$\pm 2$	$\pm 3$	$\pm 5$	+4 0	+6 0	+6 +2	+8 +2	+10 +4
3	6	-20 -32	-20 -38	-10 -50	-10 -18	-10 -22	-10 -28	-4 -9	-4 -12	-4 -5	-4 -8	-4 -12	-4 -18	-4 -30	$\pm 2.5$	$\pm 4$	$\pm 6$	+6 +1	+9 +1	+9 +4	+12 +4	+16 +8
6	10	-25 -40	-25 -47	-25 -61	-13 -22	-13 -28	-13 -35	-5 -11	-5 -14	0 -6	0 -9	0 -15	0 -22	0 -36	$\pm 3$	$\pm 4.5$	$\pm 7$	+7 +1	+10 +1	+12 +6	+15 +6	+19 +10
10	14	-32 -50	-32 -59	-16 -75	-16 -27	-16 -34	-16 -43	-6 -14	-6 -17	0 -8	0 -11	0 -18	0 -27	0 -43	$\pm 4$	$\pm 5.5$	$\pm 9$	+9 +1	+12 +1	+15 +7	+18 +7	+23 +12
14	18	-40 -61	-40 -73	-40 -92	-20 -33	-20 -41	-20 -53	-7 -16	-7 -20	0 -9	0 -13	0 -21	0 -33	0 -52	$\pm 4.5$	$\pm 6.5$	$\pm 10$	+11 +2	+15 +2	+17 +8	+21 +8	+28 +15
18	24	-40 -61	-40 -73	-40 -92	-20 -33	-20 -41	-20 -53	-7 -16	-7 -20	0 -9	0 -13	0 -21	0 -33	0 -52	$\pm 4.5$	$\pm 6.5$	$\pm 10$	+11 +2	+15 +2	+17 +8	+21 +8	+28 +15
24	30	-50 -75	-50 -75	-25 -75	-25 -89	-25 -112	-25 -41	-25 -50	-25 -64	-9 -20	-9 -25	-9 -11	-9 -16	-9 -25	$\pm 5.5$	$\pm 8$	$\pm 12$	+13 +2	+18 +2	+20 +9	+25 +9	+33 +17
30	40	-50 -75	-50 -89	-25 -112	-25 -41	-25 -50	-25 -64	-9 -20	-9 -25	0 -11	0 -16	0 -25	0 -39	0 -62	$\pm 5.5$	$\pm 8$	$\pm 12$	+13 +2	+18 +2	+20 +9	+25 +9	+33 +17
40	50	-60 -90	-60 -106	-60 -134	-60 -49	-60 -60	-60 -76	-10 -23	-10 -29	0 -13	0 -19	0 -30	0 -46	0 -74	$\pm 6.5$	$\pm 9.5$	$\pm 15$	+15 +2	+21 +2	+24 +11	+30 +11	+39 +20
50	65	-60 -90	-60 -106	-60 -134	-60 -49	-60 -60	-60 -76	-10 -23	-10 -29	0 -13	0 -19	0 -30	0 -46	0 -74	$\pm 6.5$	$\pm 9.5$	$\pm 15$	+15 +2	+21 +2	+24 +11	+30 +11	+39 +20
65	80	-72 -107	-72 -126	-72 -159	-36 -58	-36 -71	-36 -90	-12 -27	-12 -34	0 -15	0 -22	0 -35	0 -54	0 -87	$\pm 7.5$	$\pm 11$	$\pm 17$	+18 +3	+25 +3	+28 +13	+35 +13	+45 +23
80	100	-72 -107	-72 -126	-72 -159	-36 -58	-36 -71	-36 -90	-12 -27	-12 -34	0 -15	0 -22	0 -35	0 -54	0 -87	$\pm 7.5$	$\pm 11$	$\pm 17$	+18 +3	+25 +3	+28 +17	+35 +17	+45 +31
100	120	-85 -125	-85 -148	-85 -185	-43 -68	-43 -83	-43 -106	-14 -32	-14 -39	0 -18	0 -25	0 -40	0 -63	0 -100	$\pm 9$	$\pm 12.5$	$\pm 20$	+21 +3	+28 +3	+33 +15	+40 +15	+52 +27
120	140																					
140	160																					
160	180																					
180	200																					
200	225	-100 -146	-100 -172	-100 -215	-50 -79	-50 -96	-50 -122	-15 -35	-15 -44	0 -20	0 -29	0 -46	0 -72	0 -115	$\pm 10$	$\pm 14.5$	$\pm 23$	+24 +4	+33 +4	+37 +17	+46 +17	+60 +31
225	250																					

Unit:  $\mu\text{m}$ 

Diametrical range		Standard Spindle Diametion Tolerance																				
		E7	E8	E9	F6	F7	F8	G6	G7	H6	H7	H8	H9	H10	JS6	JS7	K6	K7	M6	M7	N5	N7
-	3	+24 +14	+28 +14	+39 +14	+12 +6	+16 +6	+20 +6	+8 +2	+12 +2	+6 0	+10 0	+14 0	+25 +0	+40 0	$\pm 3$	$\pm 5$	0	0	-2	-2	-4	-4
3	6	+32 +20	+38 +20	+50 +20	+18 +20	+22 +10	+28 +10	+12 +4	+16 +4	+8 0	+12 0	+18 0	+30 0	+48 0	$\pm 4$	$\pm 6$	+2 -6	+3 -9	-1	0	-5	-4
6	10	+40 +25	+47 +25	+61 +25	+22 +13	+28 +13	+35 +13	+14 +5	+20 +5	+9 0	+15 +0	+22 0	+36 0	+58 0	$\pm 4.5$	$\pm 7$	+2 -7	+5 -10	-3	0	-7	-4
10	14	+50 +32	+59 +32	+75 +32	+27 +16	+34 +16	+43 +16	+17 +6	+24 +6	+11 0	+18 0	+27 0	+43 0	+70 0	$\pm 5.5$	$\pm 9$	+2 -9	+6 -12	-4	0	-9	-5
14	18	+52 +32	+60 +32	+77 +32	+30 +16	+38 +16	+46 +16	+20 +6	+28 +6	+13 0	+21 0	+33 0	+52 0	+84 0	$\pm 6.5$	$\pm 10$	+2 -11	+6 -15	-4	-17	-21	-28
18	24	+61 +40	+73 +40	+92 +40	+33 +20	+41 +20	+53 +20	+20 +7	+28 +7	+13 0	+21 0	+33 0	+52 0	+84 0	$\pm 6.5$	$\pm 10$	+2 -11	+6 -15	-4	0	-11	-7
24	30	+61 +40	+73 +40	+92 +40	+33 +20	+41 +20	+53 +20	+20 +7	+28 +7	+13 0	+21 0	+33 0	+52 0	+84 0	$\pm 6.5$	$\pm 10$	+2 -11	+6 -15	-4	-17	-21	-28
30	40	+75 +50	+89 +50	+112 +50	+41 +25	+50 +25	+64 +25	+25 +9	+34 +9	+16 0	+25 0	+39 0	+62 0	+100 0	$\pm 5.5$	$\pm 12$	+3 -13	+7 -18	-4	0	-12	-8
40	50	+75 +60	+89 +60	+112 +60	+41 +30	+50 +30	+64 +30	+25 +10	+34 +10	+16 0	+25 0	+39 0	+62 0	+100 0	$\pm 5.5$	$\pm 12$	+3 -13	+7 -18	-4	0	-12	-8
50	65	+90 +60	+106 +60	+134 +60	+49 +30	+60 +30	+76 +30	+29 +10	+40 +10	+19 0	+30 0	+46 0	+74 0	+120 0	$\pm 9.5$	$\pm 15$	+4 -15	+9 -21	-5	0	-14	-9
65	80	+90 +60	+106 +60	+134 +60	+49 +30	+60 +30	+76 +30	+29 +10	+40 +10	+19 0	+30 0	+46 0	+74 0	+120 0	$\pm 9.5$	$\pm 15$	+4 -15	+9 -21	-5	0	-30	-39
80	100	+107 +72	+126 +72	+159 +72	+58 +72	+71 +36	+91 +36	+34 +12	+47 +12	+22 0	+35 0	+54 0	+87 0	+140 0	$\pm 11$	$\pm 17$	+4 -18	+10 -25	-6	0	-16	-10
100	120	+107 +72	+126 +72	+159 +72	+58 +36	+71 +36	+91 +12	+34 +12	+47 0	+22 0	+35 0	+54 0	+87 0	+140 0	$\pm 11$	$\pm 17$	+4 -18	+10 -25	-6	0	-35	-45
120	140																					
140	160	+125 +85	+148 +85	+185 +85	+68 +85	+83 +85	+106 +43	+39 +43	+54 +14	+25 +14	+40 0	+63 0	+100 0	+160 0	$\pm 12.5$	$\pm 20$	+4 -21	+12 -28	-8	0	-20	-12
160	180																					
180	200																					
200	225	+146 +100	+172 +100	+215 +100	+79 +50	+96 +50	+122 +15	+44 +15	+61 +15	+29 0	+46 0	+72 0	+115 0	+185 0	$\pm 14.5$	$\pm 23$	+5 -24	+13 -33	-8	0	-22	-14
225	250																					